Phase III Drainage Report

for

Pioneer Village

Planning Areas 1-4, 17, and 21

Town of Keenesburg, Weld County, Colorado



SDD Project Number: 1919-001

Drainage Report Prepared for: **Pioneer Community Authority Board** 450 E. 17th Ave., Suite 400 Denver, CO 80203-1254 Contact: Joel Farkas (720) 362-5995

> Initial Submittal: Resubmittal: Resubmittal (If required): For Signatures:

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Table of Contents

Certifications

Section I – General Location and Description

- 1.1 Site Location
- 1.2 Description of Property

Section II – Drainage Basins and Sub-Basins

- 2.1 Major Drainage Basins
- 2.2 Minor Drainage Basins

Section III – Drainage Design Criteria

- 3.1 Regulations
- 3.2 Drainage Studies, Outfall Systems Plans, Site Constraints
- 3.3 Hydrology
- 3.4 Hydraulics
- 3.5 Water Quality Enhancement

Section IV – Stormwater Management Facility Design

- 4.1 Stormwater Conveyance Facilities
- 4.2 Stormwater Storage Facilities
- 4.3 Water Quality Enhancement Best Management Practices
- 4.4 Floodplain Modification
- 4.5 Additional Permitting Requirements
- 4.6 General

Section V - Conclusions

- 5.1 Compliance
- 5.2 Variance
- 5.3 Design Concepts

Appendices

- Appendix A Hydrology
- Appendix B Hydraulics
- Appendix C EDB Pond Details
- Appendix D Reference Material
- Appendix E Drainage Map
- Appendix F Soils Information

Certifications

Engineer Certification

"This report and plan for the Phase III drainage design of Pioneer Village was prepared under my direct supervision in accordance with the provisions of the Town of Keenesburg, the Pioneer Community Authority Board and Weld County. I understand that this jurisdiction does not and will not assume liability for drainage facilities designed by others."

(AFFIX SEAL)

Signature:

Christopher L Perdue, P.E. Registered Professional Engineer State of Colorado No. 50745

Developer/Owner Certification

"______hereby certifies that the drainage facilities for Pioneer Village shall be constructed according to the design presented in this report. I understand that the Town of Keenesburg, the Pioneer Community Authority Board and Weld County does not and will not assume liability for the drainage facilities designed and/or certified by my engineer and that each jurisdiction reviews drainage plans pursuant to Colorado Revised Statutes, Title 30, Article 28; but cannot, on behalf of Pioneer Village, guarantee that final drainage design review will absolve ______ and/or their successors and/or assigns of future liability for improper design."

Name of Developer/Owner

Authorized Representative

Section I – General Location and Description

1.1 Site Location

Pioneer Village is a large and complex development located at the northwest corner of County Roads 22 and 49. The project will encompass all of Sections 5, 7, 8, 9 and the southern half of Section 4 within Township 2 North of Range 64 West. Later phases of Project will the also propose development in portions of Section 12 of 2 North, 65 West and Section 32 of 3 North. 64 West. Sections 7, 8 and 9 along with a portion of



Section 4 was annexed into the Town of Keenesburg in the fall of 2019. The remaining Sections outlined above will be annexed into the Town in the coming months.

A copy of the Annexation Zoning Map has been provided in the appendices for reference.

As of now, the Project is primarily bounded by residential and agricultural uses. Residential uses are typically large lots in this area with an estimated impervious coverage less than 10% of the overall property.

The primary road network serving the property is Weld County Road 49 to the west and Weld County Road 51 to the southwest. Weld County Road 49 is a major arterial highway and was expanded in recent years to include two north and south lanes and an auxiliary lane. The highway currently aligns with a rural section meaning there is no curb and gutter along this segment. All runoff drains to a roadside ditch where culverts collect the runoff and convey it west towards Box Elder Creek. County Road 51 is a gravel road from the intersection with County Road 18 north to the southeast corner of Pioneer Village. From there a narrower improved surface drive makes up County Road 22 at the moment. The small segment of 22 currently supports local oil and gas activity within the subject property. As part of this Project, over time County Roads 22, 24 and 51 will be improved to their master planned sections within the limits of the Project. The timeline of such improvements hinge upon the overall success of the Project and the transportation needs associated with such success.

The description above is an excerpt from the Phase I Report prepared for the portions of Pioneer Village lying within Sections 7, 8 and 9. This Phase III Report is beig

prepared to provide specific detail related to the construction of Planning Areas 1 through 4, 17 and 21. Planning Areas 1 through 4 lie in the northwest corner of Section 7. Planning Areas 17 and 21 lie within the southern portion of Section 8. All of the proposed work will lie within the eastern and middle basins outlined in the Phase I Report.

In addition to the residential planning areas, these plans will also address construction of the Pioneer Village Regional Drainage Way and three large extended detention basins (EDB's).

Due to the overall size of Pioneer Village, our team has drafted this report with a specific focus on Sections 7 through 9. Those sections lie within the first 30-years of master planned permitting and construction. In the case of most master plans of this magnitude, this study will need to be continually revisited to ensure compliance as well as proper long-range planning and revisions as required to address the on-going deviation from the Project's vision as of this draft.

proposed community development project that has been annexed into the Town of Keenesburg. The site is centered around the intersection of Weld County Roads (WCR) 51 and 24, north of WCR 22 and west of WCR 49. This community will lie within Sections 7, 8, 9, and 5 of Township 2 North, Range 64 West and Section 35 of Township 3 North, Range 64 West. The property is located north of the Towns of Hudson and Keenesburg as well as Interstate 76. A Vicinity Map is provided here for reference.

Three primary drainage basins have been identified within the Pioneer Development Area for the first Phase. A natural ridge line runs from the Northwest corner of the NW1/4 of Section 7, East towards the center of Section 7 and North towards WCR 24. The drainage basin located to the west of this ridge line drains West towards Box Elder Creek, a tributary of the South Platte River, while the two basins to the East of this ridge line drain East to a tributary of Box Elder Creek, that runs north to south through Sections 5 and 8 of T3N, R64W. All three basins fall within the larger South Platte River Basin.

1.2 Description of Property

The entire Pioneer Development region spans approximately 3,150 acres zoned for commercial, residential, and industrial development. Currently, this area is comprised of open space and agricultural land with a few well pads and associated gravel access roads. The existing landscape primarily consists of gentle, rolling topography covered in native grasses with surface elevations ranging from approximately 4,800 to 4,950. The only structures currently within the development area are oil and gas infrastructure, some active and some abandoned over the last 10 or so years thereby allowing the current development plan to come to fruition.



In general, Pioneer slopes gradually from south to north with most of Section 7, 8 and half of 9 bearing in a westerly direction. The east half of Section 9 will flow northeast towards the Section corner. Currently, there is a portion of Section 8 encumbered by the 100-year floodplain. The area dissects Section 8 and is listed as Zone "A" meaning no base flood elevation has been determined at this Reference time Map Number 08123C1975E with an effective date of January 20th, 2016.

Our research and site investigation

have confirmed that no existing irrigation canals or ditches lie within the property.

The geotechnical report available to us during the design process did not allude to any significant geological hazards within the property. A summary of the on-site soils is provided in the table below based on NRCS information made publicly available. Additional soil information is available in the custom soils report in the appendices.

As outlined in the previous section, Planning Area's 1 through 4 are located in the northwest corner of the project. An existing ridge bisects Planning Areas 1 through 4 with the eastern most planning areas (3&4) draining northeast and the western planning areas (1&2) draining northwest. Due to this natural divide, SSD has proposed two separate stormwater management facilities to address those planning areas.

Planning area's 17 and 21 naturally drain to the northeast to the existing "un-named" stream listed shown on the above referenced FEMA Firm Panel. The proposed design herein will honor this natural divide with both planning areas sloping gently to the northeast.

In the existing condition, the site is primarily covered in native grasses, with a few, scattered dirt roads providing access to the oil and gas wells on the property (both active and abandoned).

Based on the Custom Soil Resource Report for Pioneer Section 7 included in the Appendices, the portions of Pioneer contained in Section 7 (Planning Areas 1-4 and 17) are primarily composed of the soil types listed below.

Map Unit Symbol	Map Unit Name	% of AOI	Hydrologic Soil Group
44	Olney Loamy Sand, 1 to 3% slopes	0.2	В
49	Osgood Sand, 0 to 3% slopes	14.4	А
70	Valent Sand, 3 to 9% slopes	76.7	A
72	Vona Loamy Sand, 0 to 3% slopes	8.6	A

Based on the Custom Soil Resource Report for Pioneer Section 8 included in the Appendices, the soils in this section are primarily composed of the soil types listed in the table below.

Map Unit Symbol	Map Unit Name	% of AOI	Hydrologic Soil Group
35	Loup-Boel Loamy Sands, 0 to 3% slopes	11.6	A/D
44	Olney Loamy Sand, 1 to 3% slopes	3.4	В
49	Osgood Sand, 0 to 3% slopes	26.0	A
70	Valent Sand, 3 to 9% slopes	53.0	A
72	Vona Loamy Sand, 0 to 3% slopes	5.5	A
85	Water	0.6	

However, the portion of Section 8 utilized for the construction of Planning Area 21 only contains soil types 44, 49, 70 and 72 as shown on page 9 of the Custom Soil Resource Report for Pioneer Section 8.

The predominant soil type for each of these Sections is Hydrologic Group Type "A".

There is an existing drainage ditch running South to North on the East side of WCR 49 that contains two culverts. The first culvert allows the ditch to flow under WCR 22, in the Southwest corner of the development area, and a second culver that allows the ditch to flow under WCR 24, in the Northwest corner of the development area.

Our field visits and results of previous a Geotechnical Engineering Study suggest that no major geological features lie within the basin.

The proposed development consists of six residential planning areas, including approximately 1,273 units. The development will include all necessary infrastructure, including wet and dry utilities, parking facilities, connections to existing roadways, storm drainage, and drainage control facilities. Three extended detention basins (EDB) will be located within the development area. One EDB will be located in the northeast corner of Section 7, in the southeast corner of the intersection of WCR 49 and WCR 24. A second will be located north, center of Section 7, just south of WCR 24. The third pond will be located slightly southwest of the center of Section 8, just north of Planning

Area 21 and east of the tributary running through the property. See the exhibit on the following page for delineation of each of these basins, labeled by their associated detention pond.

Section II – Drainage Basins and Sub-Basins

2.1 Major Drainage Basins

There are three major drainage basins identified within the development area for Development Phase 1 of Pioneer.

The first major basin identified is Basin Pond A. This delineation includes 66.46 acres in the NW1/4 and SW1/4 of Section 7 with an impervious land cover condition of 48.87%. This basin will contain all drainage associated with Planning Areas 1 and 2 of this development, a portion of Collector D, a portion of Local road G, and a portion of WCR 24. Pond A's proposed location is in the NW1/4 of the NW1/4 of Section 7, in the southeast corner of the intersection of WCRs 49 and 22.

The second major basin identified is Basin Pond B. The delineation of Pond B includes 51.64 acres in the NE1/4 and SE1/4 of the NW1/4 of Section 7 with an impervious land cover condition of 58%. Basin Pond B will collect drainage from Planning Areas 3 and 4, a portion of Collector A, a portion of Collector D, a portion of WCR 24, and Collector B. Pond B's proposed location is in the NW1/4 of the NE1/4 of Section 7.

The final major basin in Basin Pond C. Basin Pond C contains 144.88 acres that lies within the SE1/4 of Section 7 and the SW ¼ of Section 8. The land cover condition for Basin Pond C is 49% imperviousness. Pond C will collect runoff from Planning Areas 17 and 21, Collector XX, a portion of Collector A, and the portions of WCR 22 included in the initial phase. The proposed location for pond C is in the NE1/4 of the SE1/4 of Section 8

All construction on this site will provide water quality treatment and peak runoff reduction in accordance with Mile High Flood District (MHFD) requirements.

2.2 Minor Drainage Basins

Specifically, this report will focus on the minor drainage basins associated with the proper design of "on-site" and adjacent stormwater management collection, conveyance, and treatment infrastructure. As shown in the attached construction plans, there are four (4) closed conduit systems which will be addressed.

On-Site Conduit Systems:

 A system consisting of 17 Type "R" Inlets which will collect runoff generated within Planning Areas 1 and 2, as well as all runoff West of the centerline of Local Road G and North of the centerline of Collector A. This conduit system will drain to Pond A, located in the NW1/4 of the NW1/4 corner of Section 7, and will ultimately outfall to an existing Culvert located on the Northeast side of the intersection of WCRs 49 and 24.

- 2. A system consisting of 18 Type "R' Inlets and 2 Type "C" drop inlets which will collect runoff from Planning Areas 3 and 4, as well as all runoff East of the centerline of Local Road G and West of Collector B. This conduit system will drain to Pond B, located in the NE 1/4 of Section 7 and will outfall to a ditch draining east toward the tributary of Box Elder Creek.
- 3. A system consisting of 31 Type "R" Inlets which will collect runoff from all of Planning Area 17, all of the drainage in Planning Area 21 East of Local Road 21-4, and the Northern half of Planning Area 21 that falls West of Local Road 21-4. This system will also collect drainage from Collector XX East of WCR 51, and drainage from the portions of the East side of Collector A that fall South of Collector XX. This system will drain to Pond C, located slightly southwest of the center of Section 8, just north of Planning Area 21 and east of the tributary running through the property.
- 4. And a system consisting of 16 Type "R" Inlets which will collect runoff from the portions of Planning Area 21 that fall east of Local Road 21-7, the Southern half of Planning Area 21 that falls west of Local Road 21-7, and runoff from WCR 22. This conduit system will also drain to Pond C.

Off-site Systems Tributary to the On-Site Systems

1. While no there are no independent, off-site conduit systems, a portion of the conduit system draining to Pond A is located off-site, to the west of Planning Areas 1 and 2. This portion of the system runs south to north parallel to WCR 49.

A detailed summary of each basin can be found on the following page.

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C₅	C 100	Q₅	Q 100
CI 1.00	Type "R" Inlet on the Northern half of Collector D, west of Local Road G	1.00	2.77	A	55.0	Typical Single-Family Residential Development	0.40	0.54	2.59	8.10
CI 1.01	Type "R" Inlet on the Northwest side of Local Road 1A	1.01	1.00	A	55.0	Typical Single-Family Residential Development	0.40	0.54	1.16	3.60
CI 1.02	Type "R" Inlet on the Northeast side of Local Road A	1.02	2.90	A	55.0	Typical Single-Family Residential Development	0.40	0.54	3.36	10.50
CI 1.03	Type "R" Inlet on the West side of Local Road 1A at the intersection of Local Roads 1A and 1B	1.03	3.26	A	55.0	Typical Single-Family Residential Development	0.40	0.54	3.12	9.76
CI 1.04	Type "R" Inlet on the South side of Local Road 1B at the intersection of Local Roads 1A and 1B	1.04	4.96	A	55.0	Typical Single-Family Residential Development	0.40	0.54	4.66	14.59
CI 1.05	Type "R" Inlet on the North side of Local Road 1B at the intersection of Local Roads 1A and 1B	1.05	2.29	A	55.00	Typical Single-Family Residential Development	0.40	0.54	2.41	7.53
CI 1.06	Type "R' Inlet on the South side of Country Road 24 that lies west of Local Road G	1.06	0.83	A	54.00	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.39	0.53	0.99	3.13
CI 1.07	Type "R" Inlet located on Northwest side of Local Road G	1.07	0.31	A	81.4	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.66	0.74	0.79	2.08

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C₅	C ₁₀₀	Q₅	Q 100
CI 1.08	Type "R" Inlet located on Northeast side of Local Road G	1.08	0.74	A	80.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.65	0.73	1.60	4.23
Pond A Direct	Direct runoff contributing to Pond A		9.68	A	2.0	Open Space	0.01	0.13	0.10	5.17
CI 2.00	Type "R" Inlet on the Southern half of Collector D, west of Local Road G	2.00	6.40	A	55.0	Typical Single-Family Residential Development	0.40	0.54	4.83	15.12
CI 2.01	Type "R" Inlet on the Northwest corner of Local Road 2A	2.01	3.85	A	55.0	Typical Single-Family Residential Development	0.40	0.54	3.82	11.96
CI 2.02	Type "R" Inlet on the Northeast corner of Local Road 2A	2.02	2.90	A	55.0	Typical Single-Family Residential Development	0.40	0.54	2.98	9.32
CI 2.03	Type "R" Inlet on the Western side of the Northern half of Local Road G	2.03	5.26	A	55.0	Typical Single-Family Residential Development	0.40	0.54	4.36	13.63
CI 2.04	Type "R' Inlet on the Southwest corner of the Intersection of Local Road G and Local Road 2B	2.04	2.52	A	55.0	Typical Single-Family Residential Development	0.40	0.54	2.91	9.09
CI 2.05	Type "R' Inlet on the Southwest corner of the Intersection of Local Road G and Local Road 2C	2.05	5.66	А	55.0	Typical Single-Family Residential Development	0.40	0.54	5.37	16.79
CI 2.06	Type "R' Inlet on the Southeast corner of the Intersection of Local Road G and Local Road 2C	2.06	6.37	A	55.0	Typical Single-Family Residential Development	0.40	0.54	5.50	17.23

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C₅	C100	Q5	Q100
CI 2.07	Type "R" Inlet on the Northwest corner of Local Road 2B	2.07	1.57	А	55.0	Typical Single-Family Residential Development	0.40	0.54	1.80	5.64
CI 3.00	Type "R" Inlet on the Northern half of Collector D, east of Local Road G		1.29	A	85.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84	3.38	7.96
CI 3.01	Type "R" Inlet on the Southern half of Collector D, east of Local Road G		3.94	A	55.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.51	0.60	5.91	13.94
CI 3.02	Type "R" Inlet on the Eastern half of the most Eastern side of Local 3A, north of Tract A		2.40	А	55.0	Typical Single-Family Residential Development	0.51	0.60	3.74	8.78
CI 3.03	Type "R" Inlet on the Western half of the most Eastern side of Local Road 3A, north of the intersection with Local Road 3B		1.71	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.87	6.77
CI 3.04	Type "R" Inlet on the Eastern half of the most Eastern side of Local 3A, south of Tract A		3.45	A	55.0	Typical Single-Family Residential Development	0.51	0.60	5.17	12.00
CI 3.05	Type "R" Inlet on the Northern half of the East side of Local Road 3B		1.38	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.40	5.63

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C ₅	C 100	Q5	Q 100
CI 3.06	Type "R" Inlet on the Southern half of the East side of Local Road 3B		1.64	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.24	7.47
CI 3.07	Type "R" Inlet on the Western half of the most Eastern side of Local Road 3A, south of the intersection with Local Road 3B		1.71	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.77	6.56
CI 3.08	Type "R" Inlet on the Northwest corner of the intersection of Collector B and Local Road E		0.38	A	85.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84	1.22	2.89
CI 3.08A	Type "R" Inlet on the Northeast corner of the intersection of Collector B and Local Road E		0.28	A	85.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84	0.90	2.13
CI 3.09	Type "R" Inlet on the Northern half of the East side of Local Road E		2.28	A	55.0	Typical Single-Family Residential Development	0.51	0.60	4.24	9.70
CI 4.00	Type "R" Inlet on the Southern half of the East side of Local Road E		4.63	A	55.0	Typical Single-Family Residential Development	0.51	0.60	6.66	15.27
CI 4.01	Type "R" Inlet on the West side of Collector B in the Southwest corner of the intersection of Collector B and Local Road E		2.48	A	55.0	Typical Single-Family Residential Development	0.51	0.60	4.16	9.66

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C5	C 100	Q ₅	Q 100
CI 4.01A	Type "R" Inlet on the East side of Collector B in the Southeast corner of the intersection of Collector B and Local Road E		1.30	A	85.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84	3.51	8.24
DI 4.02	Type "C" Inlet on the North side of Local Road 4B in the Northeast corner of Planning Area 4		4.35	A	55.0	Typical Single-Family Residential Development	0.51	0.60	10.17	23.47
DI 4.03	Type "C" Inlet on the South side of Local Road 4B in the Northeast corner of Planning Area 4		1.50	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.51	8.09
CI 4.04	Type "R" Inlet on the West side of Local Road 4A in the Southwest corner of the intersection of Local Road 4A and Local Road E		3.17	A	55.0	Typical Single-Family Residential Development	0.51	0.60	7.41	17.10
CI 4.05	Type "R" Inlet on the South side of Local Road 4B, east of the intersection with Local Road 4A and directly North of Tract D		2.06	A	55.0	Typical Single-Family Residential Development	0.51	0.60	4.82	11.11
CI 4.06	Type "R" Inlet on the South side of Local Road 4B, east of the intersection with Local Road 4A and directly North Planning Area 4, Block 5, Lot 1		0.90	A	55.0	Typical Single-Family Residential Development	0.51	0.60	1.51	3.51

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C₅	C ₁₀₀	Q₅	Q100
CI 4.07	Type "R" Inlet on the West side of Local Road 4A, in the Southwest corner of the intersection of Local Road 4A and Local Road 4B		2.36	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.68	8.49
Future Flow WCR 24	Future flow attributed to the continued development of Weld Country Road 24		4.39	A	85.00	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84		
Pond B Direct	Direct runoff contributing to Pond B		0.49	A	17.00	Combination of Open Space and Sidewalk	0.16	0.29		
CI 17A.01	Type "R" Inlet on the North half of Collector XX, on the Northwest corner of the intersection of Collector XX and Country Road 51		2.44	A	85.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84	8.04	18.55
CI 17A.02	Type "R" Inlet on the South half of Collector XX, on the Southwest corner of the intersection of Collector XX and Country Road 51		7.85	A	51.0	Combination of Asphalt Roadway, Sidewalk, some Open Space, and Tree Lawn	0.47	0.56	9.30	21.26
CI 17A.03	Type "R" Inlet on the South half of Collector XX, just East of the intersection of Collector XX and Local Road 17-6		1.27	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.44	5.71

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C ₅	C ₁₀₀	Q₅	Q 100
CI 17A.04	Type "R" Inlet on the South half of Collector XX, just West of the intersection of Collector XX and Local Road 17-6		4.06	A	85.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.79	0.84	8.92	20.58
CI 17A.05	Type "R" Inlet centered on the South half of Local 17 Loop Road at the intersection of Local 17 Loop Road and Local Road 17-6		4.64	A	55.0	Typical Single-Family Residential Development	0.51	0.60	8.35	19.75
CI 17A.06	Type "R" Inlet on the East side of Local Road 17-1, on the Southeast corner of the intersection of Local Road 17-1 and Collector XX		5.66	A	55.0	Typical Single-Family Residential Development	0.51	0.60	10.52	24.09
CI 17A.07	Type "R" Inlet on the North side of Local 17 Loop Road, directly West of the Intersection of Local 17 Loop Road and Local Road 17-1		6.38	A	35.0	Single-Family Residential and Open Space	0.33	0.44	6.46	15.16
CI 17A.08	Type "R" Inlet on the West side of Local Road 17-1, on the Southwest corner of the intersection of Local Road 17-1 and Local 17 Loop Road		1.33	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.39	5.58
CI 17A.09	Type "R" Inlet on the East side of Local Road 17-1, on the Southeast corner of the intersection of Local Road 17-1 and Local 17 Loop Road		1.58	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.13	7.39
CI 17A.10	Type "R" Inlet on the East side of Local Road 17-3, on the Southeast corner of the intersection of Local Road 17-3 and Local 17 Loop Road		4.33	A	55.0	Typical Single-Family Residential Development	0.51	0.60	7.01	16.35

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C5	C100	Q₅	Q 100
CI 17A.11	Type "R" Inlet on the West side of Local Road 17-3, on the Southwest corner of the intersection of Local Road 17-3 and Local 17 Loop Road		3.38	A	46.0	Single-Family Residential and Open Space	0.43	0.52	5.67	13.12
CI 17A.12	Type "R" Inlet on the West side of Local Road 17-5, on the Southwest corner of the intersection of Local Road 17-5 and Local 17 Loop Road		4.05	A	55.0	Typical Single-Family Residential Development	0.51	0.60	7.28	17.24
CI 17A.13	Type "R" Inlet on the South half of Local 17 Loop Road, to the east of the intersection of Local 17 Loop Road and Local Road 17-5		2.34	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.79	8.98
CI 17A.14	Type "R" Inlet on the East side of Local Road 17-6, on the Southeast corner of the intersection of Local Road 17-6 and Collector XX		6.34	A	39.0	Single-Family Residential and Open Space	0.36	0.47	5.66	13.10
Pond C Direct	Direct runoff contributing to Pond B		3.74	А	7.00	Combination of Open Space with some Asphalt and Sidewalk	0.06	0.21		
CI 21A.01 (NW)	Type "R" Inlet on the North half of Collector XX, on the Northwest corner of the intersection of Collector XX and the Gravel Access Road located West of Pond C		2.07	A	85.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84	4.72	11.19
CI 21A.01 (NE)	Type "R" Inlet on the North half of Collector XX, on the Northeast corner of the intersection of Collector XX and the Gravel Access Road located West of Pond C		1.68	A	85.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.79	0.84	4.12	9.51

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C ₅	C100	Q ₅	Q 100
CI 21A.01 (S)	Type "R" Inlet on the South half of Collector XX, on the southwest corner of the intersection of Collector XX and the Gravel Access Road located West of Pond C		5.65	A	51.0	Combination of Asphalt Roadway, Sidewalk, and Tree Lawn	0.47	0.56	8.29	19.14
CI 21A.02	Type "R" Inlet on the South half of Collector XX, on the southwest corner of the intersection of Collector XX and Local Road 21-4		9.63	A	42.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.39	0.50	9.59	23.02
CI 21A.02A	Type "R" Inlet on the East side of Local Road 21-4, on the southeast corner of the intersection of Collector XX and Local Road 21-4		0.25	A	100.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.93	0.96	0.94	2.17
CI 21A.03	Type "R" Inlet on the North half of Local 21 Loop Road, on the Northwest corner of the intersection of Local 21 Loop Road and Local 21-4		2.79	A	55.0	Typical Single-Family Residential Development	0.51	0.60	4.18	9.53
CI 21A.04	Type "R" Inlet on the South half of Local 21 Loop Road, on the Southwest corner of the intersection of Local 21 Loop Road and Local 21-4		2.55	A	55.0	Typical Single-Family Residential Development	0.51	0.60	4.28	9.78
CI 21A.05	Type "R" Inlet on the South half of Local 21 Loop Road, on the Southeast corner of the intersection of Local 21 Loop Road and Local 21-4		3.49	A	55.0	Typical Single-Family Residential Development	0.51	0.60	6.07	14.02

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C ₅	C100	Q ₅	Q 100
CI 21A.06	Type "R" Inlet on the North half of Local 21 Loop Road, on the Northeast corner of the intersection of Local 21 Loop Road and Local 21-4		1.19	A	55.0	Typical Single-Family Residential Development	0.51	0.60	1.93	4.57
CI 21A.07	Type "R" Inlet on the Northeast side of Local Road 21-3, on the Southeast corner of the intersection of Local Road 21-3 and Local 21 Loop Road		1.97	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.31	7.68
CI 21A.08	Type "R" Inlet on the Northwest side of Local Road 21-3, on the Southwest corner of the intersection of Local Road 21-3 and Local 21 Loop Road		2.33	A	55.0	Typical Single-Family Residential Development	0.51	0.60	4.05	9.36
CI 21A.09	Type "R" Inlet on the Northeast side of Local Road 21-2, on the Southeast corner of the intersection of Local Road 21-2 and Local 21 Loop Road		1.95	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.04	7.25
CI 21A.10	Type "R" Inlet on the Northwest side of Local Road 21-2, on the Southwest corner of the intersection of Local Road 21-2 and Local 21 Loop Road		6.10	A	38.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.36	0.46	6.23	14.45
CI 21A.11	Type "R" Inlet on the Northeast side of Local Road 21-1, on the Southeast corner of the intersection of Local Road 21-1 and Local 21 Loop Road		1.92	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.11	7.37

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C ₅	C100	Q5	Q 100
CI 21A.12	Type "R" Inlet on the Northwest side of Local Road 21-1, on the Southwest corner of the intersection of Local Road 21-1 and Local 21 Loop Road		4.27	A	55.0	Typical Single-Family Residential Development	0.51	0.60	6.40	14.59
CI 21A.13	Type "R" Inlet on the Northeast side of Local Road 21-5, on the Southeast corner of the intersection of Local Road 21-5 and Local 21 Loop Road		2.17	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.77	8.72
CI 21A.14	Type "R" Inlet on the Northeast side of Local Road 21-6, on the Southeast corner of the intersection of Local Road 21-6 and Local 21 Loop Road		1.46	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.45	5.78
CI 21B.01	Type "R" Inlet on the North half of Tract N, just east of center		3.12	A	55.0	Typical Single-Family Residential Development	0.51	0.60	5.61	5.61
CI 21B.02	Type "R" Inlet on the South half of Tract N, just east of center		4.75	A	23.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.21	0.34	2.89	2.89
CI 21B.03	Type "R" Inlet on the East side of Local 21 Loop Road, on the Southeast corner of the intersection of Local Road 21-9, and Tract N		2.84	A	42.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.39	0.50	3.52	3.52

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C ₅	C 100	Q5	Q 100
CI 21B.04	Type "R" Inlet on the West side of Local 21 Loop Road, on the Southwest corner of the intersection of Local 21 Loop Road, Local Road 21-9, and Tract N		2.14	A	55.0	Typical Single-Family Residential Development	0.51	0.60	3.59	12.91
CI 21B.05	Type "R" Inlet on the Southwest side of Local Road 21-8, just North of the intersection of Local 21 Loop Road and Local Road 21-8		0.95	A	55.0	Typical Single-Family Residential Development	0.51	0.60	1.71	6.91
CI 21B.06	Type "R" Inlet on the Southeast side of Local Road 21-8, just North of the intersection of Local 21 Loop Road and Local Road 21-8		0.24	A	55.0	Typical Single-Family Residential Development	0.51	0.60	0.56	8.30
CI 21B.07	Type "R" Inlet on the South side of Local 21 Loop Road, Southwest of the intersection of Local 21 Loop Road and Local Road 21-8		1.03	A	43.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.40	0.50	1.45	8.47
CI 21B.08	Type "R" Inlet on the North side of Local 21 Loop Road, Northwest of the intersection of Local 21 Loop Road and Local Road 21-8		1.63	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.64	6.06
CI 21B.09	Type "R" Inlet on the West side of Local Road 21-7, on the Southwest corner of the intersection of Local Road 2107 and Local 21 Loop Road		5.50	A	34.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.32	0.43	4.27	9.97

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C ₅	C100	Q₅	Q 100
CI 21B.10	Type "R" Inlet on the West side of Local Road 21-7, on the Northwest corner of the intersection of Local Road 2107 and Local 21 Loop Road		1.61	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.70	6.18
CI 21B.11	Type "R" Inlet on the Southeast side of Local Road 21-6, on the Northeast corner of the intersection of Local Road 21-6 and Local 21 Loop Road		0.98	A	55.0	Typical Single-Family Residential Development	0.51	0.60	1.70	3.94
CI 21B.12	Type "R" Inlet on the Southwest side of Local Road 21-6, on the Northwest corner of the intersection of Local Road 21-6 and Local 21 Loop Road		1.08	A	55.0	Typical Single-Family Residential Development	0.51	0.60	1.88	4.34
CI 21B.13	Type "R" Inlet on the Southeast side of Local Road 21-5, on the Northeast corner of the intersection of Local Road 21-5 and Local 21 Loop Road		0.78	A	55.0	Typical Single-Family Residential Development	0.51	0.60	1.36	3.23
CI 21B.14	Type "R" Inlet on the Southwest side of Local Road 21-5, on the Northwest corner of the intersection of Local Road 21-5 and Local 21 Loop Road		0.98	A	55.0	Typical Single-Family Residential Development	0.51	0.60	1.70	4.05
CI 21B.15	Type "R" Inlet on the Northwest side of Local Road 21-8, on the Southwest corner of the intersection of Local Road 21-8 and Local 21 Loop Road		1.46	A	55.0	Typical Single-Family Residential Development	0.51	0.60	2.63	6.04

Sub Basin	Basin Description	DP	Area (acres)	HSG	IMP %	Land Cover	C5	C ₁₀₀	Q₅	Q 100
CI 21B.16	Type "R" Inlet on the South half of Local 21 Loop Road, Southeast of the intersection of Local Road 21-5 and Local 21 Loop Road		4.93	A	29.0	Combination of Asphalt Roadway, Sidewalk, Single- Family Residential, and Tree Lawn	0.27	0.39	5.40	12.54

Section III – Drainage Design Criteria

3.1 Regulations

All storm drainage infrastructure proposed for construction in connection with this Project have been designed using the following criteria as required by local jurisdictions.

- Weld County Engineering and Construction Guidelines
- Urban Drainage and Flood Control District's Technical Criteria Manual
 Volumes One, Two and Three
- Urban Drainage Technical Bulletin T-5
- Urban Drainage Technical Bulletin T-12

3.2 Drainage Studies, Outfall Systems Plans, Site Constraints

To our knowledge, no prior drainage studies have been conducted in this area prior to this project. In addition to this Phase III Drainage Report, a Phase I report, including a Master Drainage study has also been completed for this development.

As mentioned in Section 2.1, due to the limited existing infrastructure in the project area, the principal constraint for this system is the existing topography and tributary running North/South across the center of the property. Drainage from Planning Areas One and Two of the development naturally drain Westward, while the remaining Planning Areas naturally drain eastward towards a tributary of Box Elder Creek.

Planning Areas 17 and 21 will drain Northeast to an Extended Detention Basin (EDB) that will slowly release flow into the tributary of Box Elder Creek. Drainage from Planning Areas 1 and 2 will flow to an EDB located in the NW1/4 of Section 7; this EDB shall outfall to an existing culvert located underneath WCR 24, on the eastern side of the intersection of WCRs 49 and 24. Drainage from Planning Areas 3 and 4 will flow to an EDB located in the NE1/4 of Section 7, just south of WCR 22. This EDB shall outfall to a ditch that spans west/east along the southern border of WCR 24 until ultimately out falling into the tributary.

3.3 Hydrology

Hydrology for the Project was determined using two methodologies.

All storm sewer collection and conveyance infrastructure were sized based upon the minor and major storm event. The Weld County Engineering and Construction Guidelines define the "major" storm event as a 100-year storm event. The "minor" storm definition for this report shall be a 5-year storm event. The Rational Method was used for determining peak discharge rates required to size on-site collection system infrastructure. Runoff Coefficients were determined for each on-site basin per values provided in UDFCD's Table 6-3 and 6-4. To calculate peak flows, UDFCD's "UD-Rational Spreadsheet" was used. The rainfall depths utilized are provided below:

	5-year, 1-hour	100-year, 1-hour
Depth (P1) Inches	1.14	2.66

These values were obtained from the National Oceanic and Atmospheric Administrations (NOAA) Rainfall data base.

The stormwater management facility was designed in accordance with volume and release rate criteria outlined by MHFD.

3.4 Hydraulics

All on-site storm sewers are proposed to be constructed using a combination of Corrugated High-Density Polyethylene (HDPE) pipe, Pre-cast Box Culverts, or Class III Reinforced Concrete Pipe (RCP) and are sized to convey runoff generated during the 100-year event. On-site curb inlets have been sized using UDFCD's UD-Inlet Software. A modeling software called Stormwater Studio was utilized to evaluate the capacity and velocity of the conveyance network and determine the hydraulic grade lines during the minor and major event.

Given the overall size of the site and the proposed land cover conditions, the primary design constraint used to size the collection system was pipe capacity. The systems were evaluated to ensure that all proposed pipes and box culverts remained a size that could be prefabricated, and that the Hydraulic Grade Line (HGL) for the major-storm event was not above the ground surface. The primary design goal was to maintain HGL elevations at a minimum of 9-inchs below the top of structure, this was achieved at the vast majority of structures in the proposed network¹. Note that Chapter 7 of the MHFD Manual does not establish the minimum distance from the top of structure to HGL. Our team utilizes 9-inches since it is a median between the two widely accepted industry standards of one (1) foot and the other being the HGL contained within the structure.

It should also be pointed out that our team made some minor assumptions that attribute to a conservative design which are provided below:

- Due to the size of the basin(s), the intensity reduction based upon the time of concentration was not reduced beyond that of the actual basin. Therefore, basin flows on the perimeter of the development will be higher in our analysis than actual flows if the time of concentration were further reduced as flows from the upstream basin traverse downstream basins to the overall outfall. *Our analysis suggests that no major inefficiencies are created by doing this since the minimum pipe size of 15-inches is oversized as is.*
- In order to design the Storm Drain Network and the Detention Pond, both the rational method and CUHP are required. Mixing the two methodologies often generates unfavorable results so SSD's typical procedure is to size the closed conduits, inlets, culverts, etc. using the rational method and then all pond infrastructure is designed using CUHP working within the UD-Detention Spreadsheet. As our design is presented later this this report, we will highlight the methodologies uses to size each element.

¹ Our team utilized 9 inches as a reference based on the Type R inlet dimension from the top of structure to invert of throat opening being 9 inches.

3.5 Water Quality Enhancement

Permanent water quality enhancement has been provided in accordance with the UDFCD's Drainage Criteria. Based on the existing topography of the site and the required 100-year detention volume, the post-construction Best Management Practice selected for this site is an EDB. The pond has been sized to provide the required Water Quality Capture Volume (WQCV) and release it over a period of 40-hours per the guidelines in Volume 3 of the Urban Drainage's Manual and Technical Bulletin T-5. A detailed description of the proposed EDB is provided in Section IV on the following pages.

Section IV – Stormwater Management Facility Design

4.1 Stormwater Conveyance Facilities

The design concept used for this site was simple: grade the site to the extent possible to honor the natural drainage divides. As outlined previously, the site has a natural ridgeline (highpoint) that runs north/south through the middle of Section 7. Everything to the west of this ridgeline drains westward towards Weld Country Road 49, while everything located to the east of this ridgeline drains east towards a tributary of Box Elder Creek that runs north/south through the Center of Section 8. To honor these existing drainage paths to the greatest extent possible, this design proposes the construction of three separate EBDs: Pond A, Pond B, and Pond C. Pond A's proposed location is in the northeast corner of Section 7, in the southeast corner of the intersection of WCR 49 and WCR 24. Pond B's proposed location is in the north, center of Section 7, just south of WCR 24. Pond C's Proposed location is slightly southwest of the center of Section 8, just north of Planning Area 21 and east of the tributary running through the property.

Street capacities were also evaluated based upon Weld County's design criteria for major and minor storm events:

- 1. Major Storm: Drainage system must be able to convey the fully developed flow from a 1-hour, 100-year event without significant damage to the system
- 2. Minor Storm: Road overtopping not to exceed 6-inches in the 10-year event and 18 inches in the 100 year event

All on-site inlets were proposed and analyzed in accordance with Chapter 7 of the MHFD's manual. The key criteria utilized were spread width and ponding depth.

Results of the street capacity analysis is provided in the UD-Inlet Spreadsheets in the appendices. Our assumptions for allowable spread for each road classification are provided below for the minor and major storms.

Street Classification	Event	Spread	Allowable Depth	Reasoning
Local Residential	Minor Major	17' 27'	6.4" ² 6.4"	Flow may pond to the street crown Flow may pond to the right of way
Residential Collector	Minor Major	17' 33.5'	8.4" ³ 8.4"	One, 12' drive isle remains Flow may pond to the right of way, with one 12' drive isle remaining
Minor Arterial	Minor Major	22' 35.5'	8.88" ⁴ 8.88"	Two, 12' drive isles remain Flow may pond to right of way, with two 12' drive isles remaining

All Type "C" and Type "R" Inlets were analyzed for capture capacity using UDFCD's UD-Inlet Software and CDOT derived nomographs. Curb inlet calculations and drop inlet computations are provided in the appendices for reference.

² Based on the street section for a local residential, the maximum depth when ponding to the right of way is 0.53' or 6.4inches. This is derived using a 4-inch curb height and a tree lawn width of 10-feet at 2.0%. During the minor storm event, the street capacity was analyzed by restricting the depth of flow to the crown elevation(s). During the major event, the crown was allowed to overtop and reach the full 6.4" depth.

³ Based on the street section for a local collector, the maximum depth when ponding to the right of way is 0.7' or 8.4inches. This is derived using a 6-inch curb height and a tree lawn width of 10-feet at 2.0%. During the minor storm event, the street capacity was analyzed by restricting the depth of flow to the crown elevation(s). During the major event, the crown was allowed to overtop and reach the full 8.4" depth.

⁴ Based on the street section for a minor arterial, the maximum depth when ponding to the right of way is 0.74' or 8.88inches. This is derived using a 6-inch curb height and a tree lawn width of 12-feet at 2.0%. During the minor storm event, the street capacity was analyzed by restricting the depth of flow to the crown elevation(s). During the major event, the crown was allowed to overtop and reach the full 8.88" depth.

Each of these system components proposed were designed to adequately convey a 100-year storm event while containing HGL elevations 9" below surface level. The design proposed for this site is consistent with local requirements having well documented maintenance protocols and therefore no concern is warranted with respect to atypical operation and maintenance procedures.

4.2 Stormwater Storage Facilities

There are three EBD stormwater management facilities proposed for construction as part of this project, identified as Pond A, Pond B, and Pond C. Pond A's proposed location is in the NW1/4 of Section 7, in the southeast corner of the intersection of WCR 49 and WCR 24. Pond B's proposed location is in the NE 1/4 Section 7, just south of WCR 24. Pond C's Proposed location is slightly southwest of the center of Section 8, just north of Planning Area 21 and east of the tributary running through the property. UDFCD's UD-Detention Spreadsheet was utilized to size the detention facilities, outlet structures, and emergency overflow. The table below depicts the proposed stage for each event and the associated inflow/outflow, based on the final routing for each Pond and associated conduit system(s).

Pond	Condition	Drainage Area (ac)	% IMP	5-Year Peak (cfs)	100-Year Peak (cfs)
Α	Inflow	66.46	47.9	16.5	81.9
A	Outflow	00.40	47.9	0.6	24.2
В	Inflow	51.6	58.0	25.1	96.5
В	Outflow			0.7	31.2
с	Inflow	144.6	49.0	48.9	203.4
C	Outflow			1.7	50.1

	Event	Туре	Stage (ft)	Corresponding Elevation
Pond A	Top of Micropool	n/a	0.00	4878.23'
	WQCV	Top of Volume	2.82	4881.05'
	EURV	Top of Volume	4.71	4882.94'
	100-Year	Top of Volume	6.36	4884.59'

Pond B	Top of Micropool	n/a	0.00	4872.12'
	WQCV EURV		2.71	4874.83'
			4.71	4876.83'
	100-Year	Top of Volume	6.36	4878.48'
Pond C	Top of Micropool	n/a	0.00	4862.21'
	WQCV	Top of Volume	3.02	4865.23'
	EURV	Top of Volume	5.49	4867.70'
	100-Year		7.65	4869.86'

Based on the information above, the proposed facilities are adequately sized to capture, detain and release the required storm events.

The required Initial Surcharge Volume (ISV) has been provided in the outlet structure and trickle channel. Given the Water Quality Capture volume, no additional infrastructure is required to keep the ISV over a hardened surface as recommended by UDFCD.

Pond	WQCV (CF)	ISV (0.3% of WQCV)	Volume Provided (CF)
А	48,395 CF	145.2 CF	213
В	43,037 CF	129.1 CF	219
С	107,026 CF	321.1 CF	344

The UD-Detention Spreadsheet was also utilized to size the emergency spillway for each EDB. Those details can be found in the spreadsheets in the appendices as well as Plan Sheets C7.00 to C7.05 of the Construction Drawings attached hereto.

All outfall pipe sizes were also pulled from the UD-Detention spreadsheet. SSD did confirm the pipe size and slope proposed in the CD's were adequate to convey the flow; however, most normal capacity calculations do not account for the outlet being surcharged by the pond.

An energy dissipation structure will be installed where each conduit system enters the corresponding pond. The dissipation structures will each have a headwall or "seal" immediately upstream of the trickle channel with a notch sized to release 2% of the peak un-detained 100-year event. The required notches sizes and subsequent release rates are provided in the table below:

Impact Stilling Basin (ISB) #	Pond	100-year UD Flow (CFS)	ISB Release Rate (2% of UD Flow)	Notch Depth (D) x Width (W) Required ³
1	А	81.9	1.64 CFS	30" (D) x 4-1/4" (W)
2	В	96.5	1.93 CFS	30" (D) x 4-5/8" (W)
3	С	150.5 ⁶	3.01 CFS	30" (D) x 6-1/8" (W)
4	С	52.9 ⁶	1.1 CFS	30" (D) x 3-5/16" (W)

Each energy dissipation structure will have the minimum forebay volume integrated into the structure. Per UDFCD Table EDB-4, the minimum forebay volume shall be 3% of the WQCV for drainage areas with greater than 20 impervious acres.

Pond	WQCV (CF)	Required Forebay Volume (CF) (3% of WQCV)	Volume Provided (CF) ⁴
A	48,395	1,452	1,595
В	43,037	1,291	1,557
С	107,026	3,211	4,035

A low flow or "trickle" channel is provided from the inflow point to the outlet structure for each of the three ponds. The trickle channels were all designed to have adequate capacity to convey 1% of the 100-year un-detained event.

³ Depth was set based upon providing required forebay volume

⁶ The Forebays for Pond C were sized based off the acreage draining to each structure. ISB 3 was sized based off 74% of the peak inflow rate contributing to Pond C, while ISB 4 was sized based off 26% of the peak inflow rate contributing to Pond C.

Trickle from ISB #	100-year UD Flow (CFS)	Required Trickle Capacity (2% of UD Flow)	Dimension of Channel	Capacity Provided (CFS)
1	81.9	1.64 CFS	2' wide x 6" deep	3.88
2	96.5	1.93 CFS	2' wide x 6" deep	3.01
3	150.5 ⁶	3.01 CFS	3' wide x 6" deep	4.88
4	52.9 ⁶	1.06 CFS	3' wide x 6" deep	4.88

Please note that like the outlet structure piping and emergency overflow, the notch and the trickle channel were evaluated based on the CUHP Calculations performed within the UD-Detention Spreadsheet. In our opinion, this alternative mitigates mixing methodologies *(i.e. CUHP vs Rationale)* and yields the best results.

Maintenance access has been provided to the invert of each pond via an 20-foot wide drive.

4.3 Water Quality Enhancement Best Management Practices

The proposed EBDs were designed in accordance with MHFD requirements with respect to water quality treatment. A Water Quality Control Plate will be provided within the outlet structure for each pond that will slowly release flow as described below:

Pond	Water Quality Capture Volume (acre-ft)	Time for Release (hrs)
A	1.111	40
В	0.988	40
С	2.457	40

The facilities have also been designed to ensure that the proposed release rates are equal to or less than 90% of the pre-development peak flow rate as determined by UD-Detention.

The previous section outlined the implementation of a sediment forebay at each concentrated pond inflow point which will release 2% of the 100-year un-detained event.

A separate operation and maintenance plan will be prepared for the facility per MHFD standards are part of the facility as-built process. As such, detailed operation and maintenance information will be provided therein. For purposes of this report, the facility's operation and maintenance plan will be consistent with other facilities of this nature. Maintenance information is available from the Mile High Flood Control District should the facility specific operation and maintenance manual be misplaced.

4.4 Floodplain Modification

As mentioned previously, a portion of Section 8 is inundated by the 100-year floodplain which is being amended via construction drawings contained in this package. That design was completed as part of the Pioneer Village Phase I Drainage Study which is attached hereto as a supplement.

4.5 Additional Permitting Requirements

Based on background information available and existing site features, no additional permits aside from the local jurisdiction's required applications typical for this type of project.

4.6 General

At the back of this report, maps and supporting calculations have been provided which support the design concepts and conclusions outlined in this report. A summary of the Appendices is provided on the following page:

Appendix	Title	Included Material
Appendix A	Hydrology	 UDFCD Table 6-3 and 6-4 Impervious Percentage Calcs UDFCD's UD Rationale
Appendix B	Hydraulics	 Stormwater Studio Outputs Inlet Carry Over Calculations Inlet Spreadsheets
Appendix C	EDB Pond Details	 UDFCD UD-Detention Workbook Trickle Channel Section Forebay Notch Sizing
Appendix D	Reference Material	 FIRM Map Index – Weld County Un- incorporated
Appendix E	Drainage Maps	Post Development Drainage Map
Appendix F	Soils Information	Web Soil Survey Report

Section V – Conclusions

5.1 Compliance with Standards

As demonstrated throughout this report and concluded in Paragraph 5.3 below, the Stormwater Management Plan proposed for the subject property is considered adequate based upon the analysis completed. Our drainage design was particularly focused on the storm drain collection and conveyance system and compliance with water quality and runoff reduction requirements outlined in the Weld County Standards and Specifications as well as Volumes One through Three of UDFCD's Stormwater Criteria.

5.2 Variances

Based on the current design, no variances to the criteria outlined by Weld County or MHFD have been made.

5.3 Drainage Concept

As shown the in previous sections and the appendices herein, the overall effectiveness of the post construction stormwater management plan outlined herein is considered adequate for the proposed development.

Based on the land cover conditions within the basin, the storm drain collection and conveyance systems are adequate to capture runoff during the minor and major event without generating excessive ponding within the Right of Way. The hydraulic grade line calculations demonstrate that all pipes will operate under normal flow conditions during the minor event. While many pipes will surcharge during a 100-year storm event, the HGLs for each pipe were designed to remain 9" below surface level. The only exception to this is CI 2.00, in which the HGL exceed 9" below surface level but remains below surface level.

As shown in the UD-Inlet Spreadsheet, the proposed roadways and allowable spreading parameters provide adequate street capacity to mitigate hydroplaning issues and provide the necessary travel lanes during the major event.

The stormwater management facility is also adequately sized to provide water quality treatment for both proposed and anticipated future impervious surfaces tributary to the EDBs. The facilities will reduce runoff volumes below pre-developed levels to mitigate any potential impacts of this development on downstream neighbors and existing drainage infrastructure.

Section VI – References

- 1. Weld County Standards and Specifications, July 2017
- Urban Storm Drainage Criteria Manual, Urban Drainage and Flood Control District, Volume 1 revised March 2017, Volume 2 revised September 2017, Volume 3 Revised November 2010
- 3. Urban Drainage Technical Memo T-5, Extended Detention Basins
- 4. Urban Drainage Technical Memo T-12, Outlet Structure



Land Use or	Percentage Imperviousness (%)		
Surface Characteristics			
Business:			
Downtown Areas	95		
Suburban Areas	75		
Residential lots (lot area only):			
Single-family			
2.5 acres or larger	12		
0.75 – 2.5 acres	20		
0.25 – 0.75 acres	30		
0.25 acres or less	45		
Apartments	75		
Industrial:			
Light areas	80		
Heavy areas	90		
Parks, cemeteries	10		
Playgrounds	25		
Schools	55		
Railroad yard areas	50		
Undeveloped Areas:			
Historic flow analysis	2		
Greenbelts, agricultural	2		
Off-site flow analysis (when land use not defined)	45		
Streets:			
Paved	100		
Gravel (packed)	40		
Drive and walks	90		
Roofs	90		
Lawns, sandy soil	2		
Lawns, clayey soil	2		

Table 6-3. Recommended percentage imperviousness values

NRCS		Storm Return Period					
Soil Group	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year
Α	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =	C _A =
	$0.84i^{1.302}$	$0.86i^{1.276}$	$0.87i^{1.232}$	$0.88i^{1.124}$	0.85 <i>i</i> +0.025	0.78 <i>i</i> +0.110	0.65 <i>i</i> +0.254
В	C _B =	C _B =	C _B =	$C_B =$	C _B =	C _B =	$C_B =$
	$0.84i^{1.169}$	$0.86i^{1.088}$	0.81 <i>i</i> +0.057	0.63 <i>i</i> +0.249	0.56 <i>i</i> +0.328	0.47 <i>i</i> +0.426	0.37 <i>i</i> +0.536
C/D	C _{C/D} =	C _{C/D} =	C _{C/D} =	$C_{C/D} =$	C _{C/D} =	C _{C/D} =	$C_{C/D} =$
	$0.83i^{1.122}$	0.82 <i>i</i> +0.035	0.74 <i>i</i> +0.132	0.56 <i>i</i> +0.319	0.49 <i>i</i> +0.393	0.41 <i>i</i> +0.484	0.32 <i>i</i> +0.588

Table 6-4. Runoff coefficient equations based on NRCS soil group and storm return period

Where:

- i = % imperviousness (expressed as a decimal)
- C_A = Runoff coefficient for Natural Resources Conservation Service (NRCS) HSG A soils
- C_B = Runoff coefficient for NRCS HSG B soils
- $C_{C/D}$ = Runoff coefficient for NRCS HSG C and D soils.

The values for various catchment imperviousness and storm return periods are presented graphically in Figures 6-1 through 6-3, and are tabulated in Table 6-5. These coefficients were developed for the Denver region to work in conjunction with the time of concentration recommendations in Section 2.4. Use of these coefficients and this procedure outside of the semi-arid climate found in the Denver region may not be valid. The UD-Rational Excel workbook performs all the needed calculations to find the runoff coefficient given the soil type and imperviousness and the reader may want to take advantage of this macro-enabled Excel workbook that is available for download from the UDFCD's website www.udfcd.org.

See Examples 7.1 and 7.2 that illustrate the Rational Method.



Overall Inputs	
Land Use	% Impervious
Open Space/Lawn	0.02
Hardscape/Pavement	1
Roof	0.9
Residential	0.55
Packed Gravel	0.4

					Pond A	A Percent Imp	ervious Calc	ulations						
Subbasin	Total Area (ac)	NRCS Hydrologic Soil Group	Open Space/	Lawn	Hardscape/	Pavement	R	oof	Resi	dential	Packee	d Gravel	% Check	Composite Imperviousness
			Area (ac)	Imp (ac)	Area (ac)	Imp (ac)	Area (ac)	Imp (ac)	Area (ac)	Imp (ac)	Area (ac)	Imp (ac)		
CI2.06	6.37	A	0.00	0.00	0.00	0.00	0.00	0.00	6.37	3.50	0.00	0	100.00%	55%
CI2.05	7.16	A	0.00	0.00	0.00	0.00	0.00	0.00	7.16	3.94	0.00	0	100.00%	55%
CI2.07	1.57	A	0.00	0.00	0.00	0.00	0.00	0.00	1.57	0.86	0.00	0	100.00%	55%
CI2.04	2.52	A	0.00	0.00	0.00	0.00	0.00	0.00	2.52	1.39	0.00	0	100.00%	55%
CI2.03	5.24	A	0.00	0.00	0.00	0.00	0.00	0.00	5.24	2.88	0.00	0	100.00%	55%
CI2.02	2.90	A	0.00	0.00	0.00	0.00	0.00	0.00	2.90	1.60	0.00	0	100.00%	55%
CI2.01	3.85	A	0.00	0.00	0.00	0.00	0.00	0.00	3.85	2.12	0.00	0	100.00%	55%
CI2.00	6.44	A	0.00	0.00	0.00	0.00	0.00	0.00	6.44	3.54	0.00	0	100.00%	55%
CI1.00	3.09	A	0.00	0.00	0.00	0.00	0.00	0.00	3.09	1.70	0.00	0	100.00%	55%
CI1.04	4.97	A	0.00	0.00	0.00	0.00	0.00	0.00	4.97	2.73	0.00	0	100.00%	55%
CI1.03	3.25	A	0.00	0.00	0.00	0.00	0.00	0.00	3.25	1.79	0.00	0	100.00%	55%
CI1.05	2.26	A	0.00	0.00	0.00	0.00	0.00	0.00	2.26	1.24	0.00	0	100.00%	55%
CI1.02	4.21	A	0.00	0.00	0.00	0.00	0.00	0.00	4.21	2.32	0.00	0	100.00%	55%
CI1.01	1.01	A	0.00	0.00	0.00	0.00	0.00	0.00	1.01	0.56	0.00	0	100.00%	55%
CI1.07	0.36	A	0.06	0.00	0.30	0.30	0.00	0.00	0.00	0.00	0.00	0	100.00%	84%
CI1.08	0.84	A	0.15	0.00	0.69	0.69	0.00	0.00	0.00	0.00	0.00	0	100.00%	82%
CI1.06	0.70	A	0.26	0.01	0.44	0.44	0.00	0.00	0.00	0.00	0.00	0	100.00%	64%
Pond (Direct)	9.68	A	9.68	0.19	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0	100.00%	2%
Total Site	66.42	A	10.15	0.20	1.43	1.43	0.00	0.00	54.84	30.16	0.00	0	100.00%	48%
CI10.1	1.00	A	0.26	0.01	0.74	0.74	0.00	0.00	0.00	0.00	0.00	0	100.00%	75%

1																Calcula	ation of P	eak Runc	off using R	ational M	lethod																
	er: TJH ny: SSD te: 3/24/2	021			Version 2.			2017 Duired user	ripput		t _i =	0.395(1.1 - C ₅)		Computed	$t_c = t_i + t_t$			t _{minimum} = t _{minimum} =	5 (urban) 10 (non-urban)							2-vr	Atlas 14 Rainfall D 5-yr 10-y 1.14 1.41	r 25-v	r 50-vr	100-vr	500-vr	n depths obta	ined from	the NOAA	website (click	this link)	
Proje	ct: Pionee	er Village			Cells of th	his color a	are for opt	tional over	ride value	es ed on override:	B t _t	$= \frac{L_t}{60K\sqrt{S_t}} = \frac{L}{60K}$	r <u>t</u> IV _t	Regional t	_c = (26 – 17i)	$+\frac{L_t}{60(14i+9)}$	$\sqrt{S_t}$	Selected t _c =	= max{t _{minimum}	, min(Comput	ed t _c , Regional	t _c)}				а	b c 10.00 0.78		$hr) = \frac{a * l}{(b + t)}$		3.65			Q(cf	(s) = CIA]	
						Rur	noff Coeff	ficient, C				Overla	and (Initial) Flo	w Time				Channe	elized (Travel) F	low Time			Tim	e of Concentr	ation		Rain	fall Intens	ity, I (in/hr)					Peak F	low, Q (cfs)		
Subcatchm Name	ent Area (ac)			es 2-yr	5-yr	10-yr	25-у	r 50-y	r 100	0-yr 500-yr	Overland Flow Lengt L _i (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Overland Flow Slope Si (ft/ft)	Overland Flow Time t _i (min)	Channelized Flow Length Lt (ft)	U/S Elevation (ft) (Optional)	D/S Elevation (ft) (Optional)	Channelized Flow Slope St (ft/ft)	NRCS Conveyance Factor K	Channelized Flow Velocity Vt (ft/sec)	Channelized Flow Time t _t (min)	Computed t _c (min)	Regional t _c (min)	Selected t _c (min)	2-yr	5-yr 10-y	r 25-y	r 50-yr	100-yr	500-yr	2-yr	5-yr	10-yr 2	25-yr 50-	yr 100-yr	r 500-yr
CI 1.04	4.96	5 A	55.0	0.39	0.40	0.42	0.45	5 0.49	9 0.:	54 0.61	88.50			0.014	10.62	1065.00			0.013	20	2.28	7.78	18.40	25.97	18.40	1.77	2.34 2.90	3.80	4.58	5.46	7.87	3.38	4.66	6.00	8.51 11.	24 14.59	23.75
CI 1.03	3.26	5 A	55.0							54 0.61	97.80			0.033	8.41	1252.70			0.012	20	2.23	9.37	17.78	27.88	17.78	1.80	2.38 2.95	i 3.87	4.66	5.56	8.00	2.26	3.12	4.01	5.69 7.5	1 9.76	15.88
CI 2.05	2.29	ə A	55.0							54 0.61				0.031	8.62	926.50			0.017	20	2.57	6.01	14.63	23.85	14.63	1.98	2.62 3.24	4.25	5.12	6.11	8.80	1.74	2.41	3.10	4.39 5.8	0 7.53	12.27
CI 1.02	2.90	A C	55.0	0.39	0.40	0.42	0.45	5 0.49	9 0.	54 0.61	60.00			0.080	4.92	905.00			0.012	20	2.19	6.88	11.80	24.89	11.80	2.17	2.88 3.56	4.68	5.64	6.72	9.68	2.43	3.36	4.32	6.12 8.0	9 10.50	17.09
CI 1.01	1.00	A C	55.0	0.39	0.40	0.42	0.45	5 0.49	9 0.1	54 0.61	19.80			0.038	3.62	1035.80			0.011	20	2.10	8.23	11.85	26.51	11.85	2.17	2.88 3.56	4.67	5.63	6.71	9.67	0.84	1.16	1.49	2.11 2.1	8 3.61	5.88
CI 2.02	2.90	A C	55.0							54 0.61	94.50			0.021	9.60	1049.50			0.023	20	3.03	5.77	15.36	23.56	15.36		2.56 3.16										
CI 2.01	3.85	5 A	55.0							54 0.61	93.60			0.025	9.02	1300.00			0.021	20	2.90	7.48	16.49	25.60	16.49		2.47 3.06										
CI 2.03	5.26	5 A	55.0							54 0.61	93.80			0.021	9.53	1892.60			0.013	20	2.28	13.83	23.36	33.22			2.06 2.55										
CI 2.04	2.52	2 A	55.0							54 0.61	30.40			0.019	5.63	1091.62			0.021	20	2.90	6.28	11.90	24.17			2.87 3.55										
CI 2.05	5.66		55.0							54 0.61	91.70			0.023	9.17	1353.07			0.016	20	2.53	8.91	18.09	27.33	21.61		2.36 2.92										
CI 2.06	6.37		55.0							54 0.61	98.60			0.018	9,71	1545.26			0.013	20	2.28	11.29	21.61	30.18	21.61		1.88 2.33										
CI 2.00	6.40	_	55.0							54 0.61	112.00			0.026	6.33	2466.80			0.013	20	2.31	17.82	12.01	38.00			2.86 3.54		0.00								
CI 2.07	1.57	_	55.0							54 0.61	30.00			0.013	10.31	1003.50			0.022	20	2.95	5.68	18.63	23.45			2.33 2.88										
CI 1.00	2.71	_	55.0							53 0.60	96.60			0.018	5.61	1300.98			0.017	20	2.61	8.32	10.29	26.61			3.05 3.77										
Ci 1.06	0.83		54.0							74 0.78	10.00			0.009	2.83	633.00			0.013	20	2.25	4.68	4.69	22.47			3.87 4.78										
CI 1.07	0.31		81.4							73 0.77	28.00			0.036	2.68	365.70			0.027	20	3.29	1.85	8.06	13.99			3.34 4.13										
CI 1.08	0.74	_	80.0							13 0.27	17.00			0.020	32.35	912.50			0.020	20	2.83	5.38	34.45	17.72			1.82 2.25										
Pond A Dire	ct 9.68	5 A	2.0	0.01	5.01	5.01	0.01	. 0.0			491.00			0.025	52.00	327.00			0.030	15	2.60	2.10		29.05	23.00			-	0.01							<u> </u>	

Pre-Development C Value Calculations Pioneer Village Keenesburg, COLORADO

Global Parameters	1
Land Use	% Imp.
Open Space/Landscaping	2
Hardscaping	100
Residential Lots	55

			F	Pond B Percer	nt Impervi	ous Calculatio	ns				
		Land Use Area p	er Sub-Bas	in						0.000	fficient ²
Subbasin	Total Area	Hardsca	nina	Ope		Residentia	allats		Composite		mcient
Cubbuoin	(acres)			Space/Lanc		reordonic		% Check	Imperviousness	5-year	100-yea
		Area (acres)	%	Area (acres)	%	Area (acres)	%				
CI 3.00	1.29	1.10	85.0%	0.19	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
CI 3.01	3.94	0.00	0.0%	0.00	0.0%	3.94	100.0%	100.00%	55%	0.51	0.60
CI 3.02	2.40	0.00	0.0%	0.00	0.0%	2.40	100.0%	100.00%	55%	0.51	0.60
CI 3.03	1.71	0.00	0.0%	0.00	0.0%	1.71	100.0%	100.00%	55%	0.51	0.60
CI 3.04	3.45	0.00	0.0%	0.00	0.0%	3.45	100.0%	100.00%	55%	0.51	0.60
CI 3.05	1.38	0.00	0.0%	0.00	0.0%	1.38	100.0%	100.00%	55%	0.51	0.60
CI 3.06	1.64	0.00	0.0%	0.00	0.0%	1.64	100.0%	100.00%	55%	0.51	0.60
CI 3.07	1.71	0.00	0.0%	0.00	0.0%	1.71	100.0%	100.00%	55%	0.51	0.60
CI 3.08	0.38	0.32	85.0%	0.06	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
CI 3.08A	0.28	0.24	85.0%	0.04	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
CI 3.09	2.28	0.00	0.0%	0.00	0.0%	2.28	100.0%	100.00%	55%	0.51	0.60
CI 4.00	4.63	0.00	0.0%	0.00	0.0%	4.63	100.0%	100.00%	55%	0.51	0.60
CI 4.01	2.48	0.00	0.0%	0.00	0.0%	2.48	100.0%	100.00%	55%	0.51	0.60
CI 4.01A	1.30	1.11	85.0%	0.20	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
CI 4.04	3.17	0.00	0.0%	0.00	0.0%	3.17	100.0%	100.00%	55%	0.51	0.60
CI 4.05	2.06	0.00	0.0%	0.00	0.0%	2.06	100.0%	100.00%	55%	0.51	0.60
CI 4.06	0.90	0.00	0.0%	0.00	0.0%	0.90	100.0%	100.00%	55%	0.51	0.60
CI 4.07	2.36	0.00	0.0%	0.00	0.0%	2.36	100.0%	100.00%	55%	0.51	0.60
DI 4.02	4.35	0.00	0.0%	0.00	0.0%	4.35	100.0%	100.00%	55%	0.51	0.60
DI 4.03	1.50	0.00	0.0%	0.00	0.0%	1.50	100.0%	100.00%	55%	0.51	0.60
											<u> </u>
uture CR 24	5.16	4.39	85.0%	0.77	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
Pond (Direct)	3.27	0.49	15.0%	2.78	85.0%	0.00	0.0%	100.00%	17%	0.16	0.29
	5.21	0.43	13.070	2.10	00.070	0.00	0.070	100.00 /0	1770	0.10	0.23
OTAL SITE	51.64	7.64	14.8%	4.04	7.8%	39.96	77.4%	100.00%	58%	0.53	0.62

¹From Table 6-3 in UDFCD Volume 1

²From Table 6-4 in UDFCD Volume 1

STANDARD FORM SF-2

TIME OF CONCENTRATION - POST DEV

Development: . Calculated By:

Pioneer Village ~ Keenesburg, CO TH

Date: 3/14/2021

						Ti	me of Cond	centration,	T _c			Minimum	Tc in Urbar	n Areas	Einel T		
	Subbas	sin Data		Initial/	Overland T	ime (t _i)		Tr	ravel Time	(t _t)			T _c Check		Final T _c	Ren	arks
Sub-Basin	Area	C5	imperviousness	Length (300' max)	Slope	ţ,	Length	Slope	Velocity	t _t	t ₆ =ti,+t _i	Comp T_c	Total Length	$T_{\rm c}$ (urban) Min			
	acres			ft	%	min.	ft	%	fps	min	min	Tc	min	min	min		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16		
CI 3.00	1.29	0.79	0.85	17	2.0%	1.8	1200	1.5%	2.4	8.2	10.0	10.0	1217	9.6	9.6		
CI 3.01	3.94	0.51	0.55	20	2.0%	3.8	1750	1.5%	2.4	11.9	15.7	15.7	1770	18.0	15.7		
CI 3.02	2.40	0.51	0.55	110	2.0%	9.0	940	1.8%	2.7	5.8	14.8	14.8	1050	14.7	14.7		
CI 3.03	1.71	0.51	0.55	93	2.6%	7.6	745	1.8%	2.7	4.6	12.2	12.2	838	13.2	12.2		
CI 3.04	3.45	0.51	0.55	22	1.9%	4.1	1365	0.8%	1.7	13.1	17.2	17.2	1387	16.4	16.4		
CI 3.05	1.38	0.51	0.55	95	2.9%	7.4	700	1.9%	2.8	4.2	11.6	11.6	795	12.8	11.6		
CI 3.06	1.64	0.51	0.55	17	2.0%	3.5	850	1.9%	2.8	5.1	8.7	8.7	867	13.8	8.7		
CI 3.07	1.71	0.51	0.55	20	2.0%	3.8	980	0.8%	1.7	9.4	13.3	13.3	1000	14.4	13.3		
CI 3.08	0.38	0.79	0.85	21	2.0%	2.0	313	0.8%	1.7	3.0	5.1	5.1	334	6.4	5.1		
CI 3.08A	0.28	0.79	0.85	21	2.0%	2.0	313	0.8%	1.7	3.0	5.1	5.1	334	6.4	5.1		
CI 3.09	2.28	0.51	0.55	23	2.0%	4.1	1030	2.0%	2.8	6.1	10.2	10.2	1053	14.7	10.2		
CI 4.00	4.63	0.51	0.55	21	2.0%	3.9	2150	1.6%	2.6	14.0	17.9	17.9	2171	19.9	17.9		
CI 4.01	2.48	0.51	0.55	21	2.0%	3.9	1575	2.3%	3.0	8.7	12.6	12.6	1596	17.2	12.6		
CI 4.01A	1.30	0.79	0.85	44	3.4%	2.5	1365	2.3%	3.0	7.5	10.0	10.0	1409	9.1	9.1		
DI 4.02	4.35	0.51	0.55	75	9.0%	4.5	1095	2.3%	3.0	6.1	10.5	10.5	1170	12.3	10.5		
DI 4.03	1.50	0.51	0.55	15	2.0%	3.3	578	2.2%	3.0	3.3	6.6	6.6	593	12.5	6.6		
CI 4.04	3.17	0.51	0.55	79	8.5%	4.7	1252	1.8%	2.7	7.8	12.5	12.5	1331	12.8	12.5		
CI 4.05	2.06	0.51	0.55	27	3.5%	3.7	705	3.2%	3.6	3.3	7.0	7.0	732	12.3	7.0		
CI 4.06	0.90	0.51	0.55	26	1.2%	5.2	547	3.7%	3.8	2.4	7.5	7.5	573	13.2	7.5		
CI 4.07	2.36	0.51	0.55	17	2.0%	3.5	925	2.3%	3.0	5.1	8.6	8.6	942	14.2	8.6		
CI 21B.15	1.46	0.51	0.55	109	2.7%	8.1	248	0.5%	1.4	2.9	11.0	11.0	357	11.2	11.0		
CI 21B.14	0.98	0.51	0.55	118	2.7%	8.4	233	0.5%	1.4	2.7	11.2	11.2	351	11.2	11.2		
CI 21B.13	0.78	0.51	0.55	118	2.7%	8.4	233	0.5%	1.4	2.7	11.2	11.2	351	11.2	11.2		
CI 21B.12	1.08	0.51	0.55	108	1.4%	10.0	297	0.9%	1.9	2.6	12.7	12.7	405	12.0	12.0		
CI 21B.11	0.98	0.51	0.55	108	1.4%	10.0	297	0.9%	1.9	2.6	12.7	12.7	405	12.0	12.0		
CI 21B.10	1.61	0.51	0.55	110	1.5%	10.0	477	0.8%	1.8	4.4	14.4	14.4	587	13.0	13.0		
CI 21B.09	10.43	0.30	0.32	300	0.9%	26.4	1632	0.6%	1.5	18.2	44.6	44.6	1932	30.5	30.5		
CI 21B.08	1.63	0.51	0.55	111	1.4%	10.2	686	0.7%	1.7	6.8	16.9	16.9	797	14.2	14.2		
CI 21B.07	1.03	0.40	0.43	46	1.4%	7.8	459	0.8%	1.7	4.4	12.2	12.2	505	14.7	12.2		
CI 21B.06	0.24	0.51	0.55	15	2.3%	3.2	180	1.3%	2.3	1.3	4.5	4.5	195	10.6	5.0	5 minutes	minimum
CI 21B.05	0.95	0.51	0.55	109	2.7%	8.1	310	0.9%	1.9	2.7	10.8	10.8	419	11.4	10.8		
CI 21B.04	2.14	0.51	0.55	110	3.5%	7.5	580	0.5%	1.4	7.1	14.5	14.5	690	12.2	12.2		
CI 21B.03	2.84	0.39	0.42	173	2.3%	12.9	697	0.5%	1.3	8.7	21.5	21.5	870	16.0	16.0		
CI 21B.02	4.75	0.21	0.23	46	1.4%	9.9	1668	0.5%	1.3	20.7	30.6	30.6	1714	28.4	28.4		
CI 21B.01	3.12	0.51	0.55	90	1.0%	10.2	807	0.8	17.7	0.8	11.0	11.0	897	15.7	11.0		
Notes:																	

Notes:

1. Flows calculated using the rational method, based on the methods provided in chapter 4 section 4 (rainfall), and Chapter 5 Section 2 (runoff) of the USDCM by UDFCD (2008). 2. $T_1 = 0.395(1.1-C_{10})(L)^{0.5}/S^{0.33}$

3. V=KSw^0.5

Pre-Development C Value Calculations Pioneer Village Keenesburg, COLORADO

Global Parameters	1
Land Use	% Imp.
Open Space/Landscaping	2
Hardscaping	100
Residential Lots	55

				Pond C In	npervious	Calculations					
		Land Use Area	per Sub-Bas	sin						0.0	fficient ²
Subbasin	Total Area (acres)	Hardsca	ping	Ope Space/Lan		Residentia	al Lots	% Check	Composite Imperviousness	5-vear	100-yea
	(00100)	Area (acres)	%	Area (acres)	%	Area (acres)	%	in chicola	Imperviousness	J-year	100-yea
CI 21B.16	4.93	0.00	0.0%	2.39	48.5%	2.54	51.5%	100.00%	29%	0.27	0.39
CI 21B.15	1.46	0.00	0.0%	0.00	0.0%	1.46	100.0%	100.00%	55%	0.51	0.60
CI 21B.14	0.98	0.00	0.0%	0.00	0.0%	0.98	100.0%	100.00%	55%	0.51	0.60
CI 21B.13	0.78	0.00	0.0%	0.00	0.0%	0.78	100.0%	100.00%	55%	0.51	0.60
CI 21B.12	1.08	0.00	0.0%	0.00	0.0%	1.08	100.0%	100.00%	55%	0.51	0.60
CI 21B.11	0.98	0.00	0.0%	0.00	0.0%	0.98	100.0%	100.00%	55%	0.51	0.60
CI 21B.10	1.61	0.00	0.0%	0.00	0.0%	1.61	100.0%	100.00%	55%	0.51	0.60
CI 21B.09	5.50	0.00	0.0%	2.15	39.1%	3.35	60.9%	100.00%	34%	0.32	0.43
CI 21B.08	1.63	0.00	0.0%	0.00	0.0%	1.63	100.0%	100.00%	55%	0.51	0.60
CI 21B.07	1.03	0.00	0.0%	0.23	22.3%	0.80	77.7%	100.00%	43%	0.40	0.50
CI 21B.06	0.24	0.00	0.0%	0.00	0.0%	0.24	100.0%	100.00%	55%	0.51	0.60
CI 21B.05	0.95	0.00	0.0%	0.00	0.0%	0.95	100.0%	100.00%	55%	0.51	0.60
CI 21B.04	2.14	0.00	0.0%	0.00	0.0%	2.14	100.0%	100.00%	55%	0.51	0.60
CI 21B.03	2.84	0.00	0.0%	0.69	24.3%	2.15	75.7%	100.00%	42%	0.39	0.50
CI 21B.02	4.75	0.00	0.0%	2.89	60.8%	1.86	39.2%	100.00%	23%	0.21	0.34
CI 21B.01	3.12	0.00	0.0%	0.00	0.0%	3.12	100.0%	100.00%	55%	0.51	0.60
CI 21A.14	1.46	0.00	0.0%	0.00	0.0%	1.46	100.0%	100.00%	55%	0.51	0.60
CI 21A.13	2.17	0.00	0.0%	0.00	0.0%	2.17	100.0%	100.00%	55%	0.51	0.60
CI 21A.11	1.92	0.00	0.0%	0.00	0.0%	1.92	100.0%	100.00%	55%	0.51	0.60
CI 21A.12	4.27	0.00	0.0%	0.00	0.0%	4.27	100.0%	100.00%	55%	0.51	0.60
CI 21A.10	6.10	0.00	0.0%	1.92	31.5%	4.18	68.5%	100.00%	38%	0.36	0.46
CI 21A.09	1.95	0.00	0.0%	0.00	0.0%	1.95	100.0%	100.00%	55%	0.51	0.60
CI 21A.08	2.33	0.00	0.0%	0.00	0.0%	2.33	100.0%	100.00%	55%	0.51	0.60
CI 21A.07	1.97	0.00	0.0%	0.00	0.0%	1.97	100.0%	100.00%	55%	0.51	0.60
CI 21A.06	1.19	0.00	0.0%	0.00	0.0%	1.19	100.0%	100.00%	55%	0.51	0.60
CI 21A.05	3.49	0.00	0.0%	0.00	0.0%	3.49	100.0%	100.00%	55%	0.51	0.60
CI 21A.04	2.55	0.00	0.0%	0.00	0.0%	2.55	100.0%	100.00%	55%	0.51	0.60
CI 21A.03	2.79	0.00	0.0%	0.00	0.0%	2.79	100.0%	100.00%	55%	0.51	0.60
CI 21A.02A	0.25	0.25	100.0%	0.00	0.0%	0.00	0.0%	100.00%	100%	0.93	0.96
CI 21A.02	9.63	2.36	24.5%	4.28	44.4%	2.99	31.0%	100.00%	42%	0.39	0.50
CI 21A.01(S)	5.65	1.59	28.1%	1.81	32.0%	2.25	39.8%	100.00%	51%	0.47	0.56
CI 21A.01(NE)	1.68	1.43	85.0%	0.25	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
CI 21A.01(NW)	2.07	1.76	85.0%	0.31	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
CI 17A.14	6.34	0.00	0.0%	1.92	30.3%	4.42	69.7%	100.00%	39%	0.36	0.47
CI 17A.13	2.34	0.00	0.0%	0.00	0.0%	2.34	100.0%	100.00%	55%	0.51	0.60
CI 17A.12	4.05	0.00	0.0%	0.00	0.0%	4.05	100.0%	100.00%	55%	0.51	0.60
CI 17A.11	3.38	0.00	0.0%	0.59	17.5%	2.79	82.5%	100.00%	46%	0.43	0.52
CI 17A.10	4.33	0.00	0.0%	0.00	0.0%	4.33	100.0%	100.00%	55%	0.51	0.60
CI 17A.09	1.58	0.00	0.0%	0.00	0.0%	1.58	100.0%	100.00%	55%	0.51	0.60
CI 17A.08	1.33	0.00	0.0%	0.00	0.0%	1.33	100.0%	100.00%	55%	0.51	0.60
CI 17A.07	6.38	0.00	0.0%	2.37	37.1%	4.01	62.9%	100.00%	35%	0.33	0.44
CI 17A.06	5.66	0.00	0.0%	0.00	0.0%	5.66	100.0%	100.00%	55%	0.51	0.60
CI 17A.05	4.64	0.00	0.0%	0.00	0.0%	4.64	100.0%	100.00%	55%	0.51	0.60
CI 17A.04	4.06	3.45	85.0%	0.61	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
CI 17A.03	1.27	0.00	0.0%	0.00	0.0%	1.27	100.0%	100.00%	55%	0.51	0.60
CI 17A.02	7.85	2.88	36.7%	3.09	39.4%	1.88	23.9%	100.00%	51%	0.47	0.56
CI 17A.01	2.44	2.07	85.0%	0.37	15.0%	0.00	0.0%	100.00%	85%	0.79	0.84
ond C (Direct)	3.74	0.19	5.0%	3.55	95.0%	0.00	0.0%	100.00%	7%	0.06	0.21
	144.88	15.98	11.0%	29.42	20.3%	99.48	68.7%	100.00%	49%	0.46	0.55
TOTAL SITE											

¹From Table 6-3 in UDFCD Volume 1

²From Table 6-4 in UDFCD Volume 1

STANDARD FORM SF-2 TIME OF CONCENTRATION - POST DEV

Development: Calculated By:

Pioneer Village ~ Keenesburg, CO TH

Date: 3/14/2021

	Subbasir	Data				Ti	me of Con	centration,	T _c			Minimum	Tc in Urban	Areas	Final T.	Remarks	
	Subbasir	Data		Initial/	Overland T	ime (t _i)		Tr	avel Time	(t _t)			T _c Check		rinai i _c	Remarks	
Sub-Basin	Area	C5	imperviousness	Length (300' max)	Slope	ťi	Length	Slope	Velocity	tı	t₀=t₁+tţ	$CompT_{c}$	Total Length	T _c (urban) Min			
	acres			ft	%	min.	ft	%	fps	min	min	Tc	min	min	min		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16		
CI 21B.16	4.93	0.27	0.29	10	2.0%	3.8	935	0.8%	1.7	8.9	12.7	12.7	945	19.5	12.7		
CI 21B.15	1.46	0.51	0.55	109	2.7%	8.1	248	0.5%	1.4	2.9	11.0	11.0	357	11.2	11.0		
CI 21B.14	0.98	0.51	0.55	118	2.7%	8.4	233	0.5%	1.4	2.7	11.2	11.2	351	11.2	11.2		
CI 21B.13	0.78	0.51	0.55	118	2.7%	8.4	233	0.5%	1.4	2.7	11.2	11.2	351	11.2	11.2		
CI 21B.12	1.08	0.51	0.55	108	1.4%	10.0	297	0.9%	1.9	2.6	12.7	12.7	405	12.0	12.0		
CI 21B.11	0.98	0.51	0.55	108	1.4%	10.0	297	0.9%	1.9	2.6	12.7	12.7	405	12.0	12.0		
CI 21B.10	1.61	0.51	0.55	110	1.5%	10.0	477	0.8%	1.8	4.4	14.4	14.4	587	13.0	13.0		
CI 21B.09	5.50	0.32	0.34	300	0.9%	25.7	1632	0.6%	1.5	18.2	43.9	43.9	1932	29.6	29.6		
CI 21B.08	1.63	0.51	0.55	111	1.4%	10.2	686	0.7%	1.7	6.8	16.9	16.9	797	14.2	14.2		
CI 21B.07	1.03	0.40	0.43	46	1.4%	7.8	459	0.8%	1.7	4.4	12.2	12.2	505	14.7	12.2		
CI 21B.06	0.24	0.51	0.55	15	2.3%	3.2	180	1.3%	2.3	1.3	4.5	4.5	195	10.6	5.0	5 minutes minin	num
CI 21B.05	0.95	0.51	0.55	109	2.7%	8.1	310	0.9%	1.9	2.7	10.8	10.8	419	11.4	10.8		
CI 21B.04	2.14	0.51	0.55	110	3.5%	7.5	580	0.5%	1.4	7.1	14.5	14.5	690	12.2	12.2		
CI 21B.03	2.84	0.39	0.42	173	2.3%	12.9	697	0.5%	1.3	8.7	21.5	21.5	870	16.0	16.0		
CI 21B.02	4.75	0.21	0.23	46	1.4%	9.9	1668	0.5%	1.3	20.7	30.6	30.6	1714	28.4	28.4		
CI 21B.01	3.12	0.51	0.55	90	1.0%	10.2	807	0.8	17.7	0.8	11.0	11.0	897	15.7	11.0		
CI 21A.14	1.46	0.51	0.55	105	1.0%	11.1	284	0.8%	1.8	2.7	13.7	13.7	389	12.3	12.3		
CI 21A.13	2.17	0.51	0.55	105	1.0%	11.1	347	1.3%	2.3	2.5	13.6	13.6	348	12.0	12.0		
CI 21A.12	4.27	0.51	0.55	60	1.6%	7.2	1256	1.1%	2.1	10.0	17.2	17.2	1316	16.7	16.7		
CI 21A.11	1.92	0.51	0.55	24	2.0%	4.2	1096	1.0%	2.0	9.1	13.3	13.3	1097	14.9	13.3		
CI 21A.10	6.10	0.36	0.38	300	1.8%	19.6	1188	0.8%	1.7	11.4	31.0	31.0	1488	21.1	21.1		
CI 21A.09	1.95	0.51	0.55	24	2.3%	4.0	1171	0.9%	1.9	10.4	14.4	14.4	1171	14.9	14.4		
CI 21A.08	2.33	0.51	0.55	24	2.3%	4.0	880	0.9%	1.8	8.0	12.0	12.0	904	13.7	12.0		
CI 21A.07	1.97	0.51	0.55	83	1.8%	8.1	610	0.8%	1.7	5.9	14.0	14.0	610	12.8	12.8		
CI 21A.06	1.19	0.51	0.55	60	2.2%	6.4	740	0.8%	1.7	7.1	13.5	13.5	800	13.3	13.3		
Ci 21A.05	3.49	0.51	0.55	25	1.5%	4.7	705	0.7%	1.7	7.0	11.7	11.7	730	13.7	11.7		
CI 21A.04	2.55	0.51	0.55	24	2.0%	4.2	926	0.8%	1.7	8.9	13.1	13.1	926	14.1	13.1		
CI 21A.03	2.79	0.51	0.55	60	1.6%	7.2	1256	1.1%	2.1	10.0	17.2	17.2	1316	16.7	16.7	_	
CI 21A.02A	0.25	0.93	1.00	23	2.0%	1.2	15	2.0%	2.8	0.1	1.3	1.3	38	3.1	5.0	5 minutes minin	num
CI 21A.02	9.63	0.39	0.42	144	2.2%	11.9	2380	0.9%	1.9	20.6	32.5	32.5	2381	23.7	23.7		
CI 21A.01(S)	5.65	0.47	0.51	20	1.6%	4.4	890	0.4%	1.2	12.4	16.8	16.8	910	15.4	15.4		

CI 21A.01(NE)	1.68	0.79	0.85	27	2.0%	2.3	1870	0.4%	1.2	26.0	28.3	28.3	1871	12.0	12.0	
CI 21A.01(NW)	2.07	0.79	0.85	106	2.1%	4.6	2175	0.4%	1.2	30.2	34.8	34.8	2281	13.4	13.4	
CI 17A.14	6.34	0.36	0.39	47	1.0%	9.3	2153	1.0%	2.0	17.8	27.0	27.0	2200	29.3	27.0	
CI 17A.13	2.34	0.51	0.55	24	2.0%	4.2	1096	1.0%	2.0	9.1	13.3	13.3	1096	14.9	13.3	
CI 17A.12	4.05	0.51	0.55	24	2.0%	4.2	925	1.5%	2.4	6.3	10.5	10.5	949	14.2	10.5	
CI 17A.11	3.38	0.43	0.46	13	2.0%	3.5	953	1.9%	2.7	5.8	9.4	9.4	966	16.1	9.4	
CI 17A.10	4.33	0.51	0.55	251	2.6%	12.4	734	1.7%	2.6	4.7	17.1	17.1	985	13.8	13.8	
CI 17A.09	1.58	0.51	0.55	19	2.2%	3.6	797	2.1%	2.9	4.6	8.2	8.2	816	13.4	8.2	
CI 17A.08	1.33	0.51	0.55	98	2.4%	8.0	525	2.4%	3.1	2.8	10.8	10.8	623	12.4	10.8	
CI 17A.07	6.38	0.33	0.35	165	3.0%	12.6	1177	1.3%	2.3	8.7	21.3	21.3	1342	19.0	19.0	
CI 17A.06	5.66	0.51	0.55	19	2.2%	3.6	1062	1.8%	2.7	6.6	10.2	10.2	1081	14.6	10.2	
CI 17A.05	4.64	0.51	0.55	24	3.6%	3.4	1052	1.6%	2.5	6.9	10.3	10.3	1076	13.5	10.3	
CI 17A.04	4.06	0.79	0.85	26	1.9%	2.3	2670	1.1%	2.0	21.7	24.0	24.0	2696	15.2	15.2	
CI 17A.03	1.27	0.51	0.55	15	2.0%	3.3	805	1.5%	2.4	5.6	8.9	8.9	820	13.6	8.9	
CI 17A.02	7.85	0.47	0.51	25	2.0%	4.6	2611	1.2%	2.1	20.3	24.9	24.9	2636	23.3	23.3	
CI 17A.01	2.44	0.79	0.85	24	2.6%	2.0	2680	1.1	21.0	2.1	4.1	4.1	2704	13.9	5.0	
0.00	#N/A	#N/A	#N/A	-	-	-	1668		-	-	-	-	-	-	5.0	5 minutes minimum
PR20	#N/A	#N/A	#N/A	150	3.2%	#N/A	1668	0.5%	1.4	19.7	#N/A	#N/A	1818	#N/A	#N/A	
PR21	#N/A	#N/A	#N/A	54	5.6%	#N/A	1668	5.0%	4.5	6.2	#N/A	#N/A	1722	#N/A	#N/A	
PR22	#N/A	#N/A	#N/A	97	6.5%	#N/A	1668	3.6%	3.8	7.3	#N/A	#N/A	1765	#N/A	#N/A	
		•		•	•							•				•

Notes:

1. Flows calculated using the rational method, based on the methods provided in chapter 4 section 4 (rainfall), and Chapter 5 Section 2 (runoff) of the USDCM by UDFCD (2008). 2. $T_i = 0.395(1.1-C_{10})(L)^{0.5}/S^{0.33}$

3. V=KSw^0.5

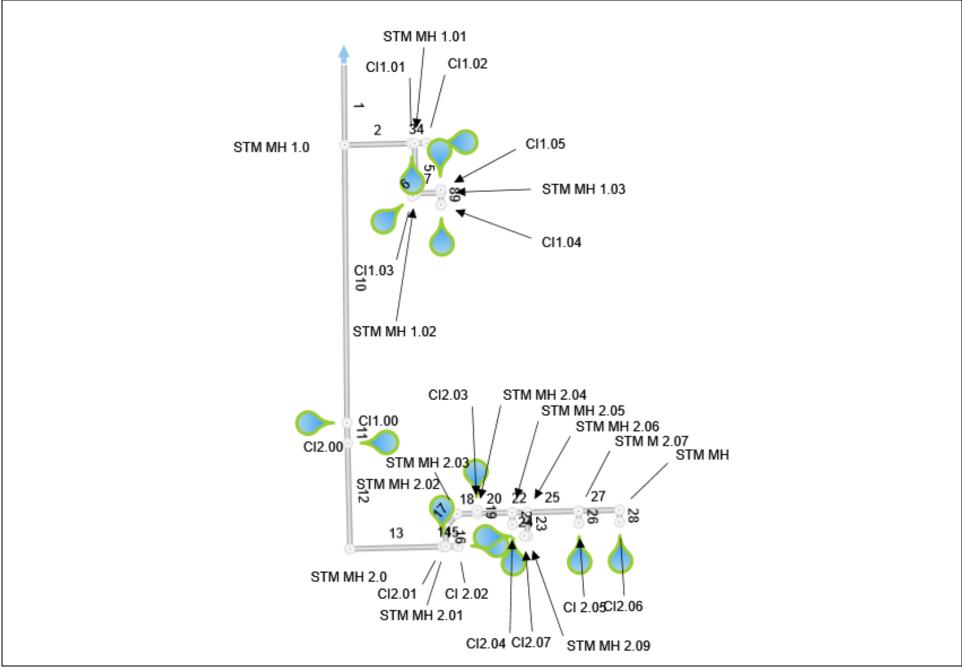
Pioneer Village Phase 1 Town of Keenesburg

				Off	site Impervio	us Calculations	for Culverts ar	nd Inlets Alor	ng WCR 49						
		Total	NRCS	Open Spa	ce/Lawn	Hardscape/	Pavement	Ro	oof	Resid	ential	Packed	l Gravel		Percent
Structure	Design Points	Area (ac)	Hydrologic	Area (ac)	Imp (ac)	Area (ac)	Imp (ac)	Area (ac)	Imp (ac)	Area (ac)	Imp (ac)	Area (ac)	Imp (ac)	% Check	Impervious
EX CULV 1	EX CULV 1	5.46	A	4.5692	0.091384	0.8908	0.8908							100.00%	17.99%
P CULV 1	P CULV 1	7.73	A	6.145	0.1229	1.585	1.585							100.00%	22.09%
CI A.00	P CULV 2	0.93	A	0.648	0.01296	0.282	0.282							100.00%	31.72%
Ci A.01	P CULV 3	0.64	A	0.373	0.00746	0.267	0.267							100.00%	42.88%

	SSD 4/8/2021 Pioneer	Village			Cells of this Cells of this Cells of this Cells of this	color are color are color are	for requir for option for calcul	red user-inp nal override lated result	values	n overrides	t _i = -	$\frac{1.395(1.1 - C_5)}{S_1^{0.33}} = \frac{L_t}{60K\sqrt{S_t}} = \frac{L}{60}$	t. Vt		$c = t_i + t_t$ = (26 - 17i) -	$+\frac{L_t}{60(14i+9)}$	1/St		0 (non-urban) max{t _{minimum}		ed t _e , Regional	t _c)}	Rainfall Inter	hour rainfall d	epth, P1 (in) = Coefficients =	2-yr 0.86	5-yr 1.14 b 10.00	10-yr 25- 1.41 1.8 c I(in 0.786	yr = 5i 5 = 2i /hr) = -i	alldown list OR e 50-yr 100-yr 2.23 2.66 a * P1 (b + tc) ^c 0			obtained fro	Q	Q(cfs) = CIA	A	<u>nk)</u>	
Subcatchmen Name	Area (ac)	NRCS Hydrologic Soil Group	Percent Imperviousnes	2-vr	5-vr	Runoff	f Coeffici 25-vr		100-vr	500-vr	Overland Flow Length	U/S	D/S Elevation	V Time Overland Flow Slope		Channelized Flow Length	U/S Elevation	D/S	Channelized Flow Slope	NRCS	Channelized Flow	Channelized Flow Time	Computed	e of Concentr Regional	Selected	2-vr		Rainfall Inten			r 500-v	r 2-yr	5-yr		ak Flow, Q (o 25-yr		100-yr	500-vr
		Soll Group	5	0.09		0.11			0.25	0.37	L _i (ft)	(ft) (Optional)	(ft) (Optional)	S _i (ft/ft)	t _i (min) 26.55	L, (ft)	(ft) (Optional)	(ff) (Optional)	S _t (ft/ft)	Factor K	Velocity V _t (ft/sec)	t, (min)	t _c (min) 33.33	t _c (min)	t _e (min) 31.77	130	-	2.14 2.8		3.38 4.03		-	-	1.23	-			11.73
EX CULV 1	5.46	A	18.0	0.00	0.10						300.00			0.017		708.95			0.014	15	1.74	6.78		31.77		1.00							0.51					
P CULV 1	7.73	A	22.1	0.12	0.13	0.14	0.16	0.21	0.28	0.40	300.00			0.038	19.62	1022.00			0.017	15	1.93	8.81	28.43	33.18	28.43	1.39	1.85	2.28 3.0	0 3	3.61 4.31	6.20	1.27	1.79	2.40	3.75	5.96	9.39	19.01
CI A.00	0.93	A	31.7	0.19	0.20	0.21	0.24	0.30	0.36	0.46	17.30			0.023	5.14	318.50			0.039	20	3.94	1.35	6.49	22.61	6.49	2.71	3.59	4.44 5.8	3 7	7.02 8.38	12.06	3 0.47	0.66	0.88	1.32	1.93	2.78	5.14
CI A.01	0.64	A	42.9	0.28	0.29	0.31	0.34	0.39	0.44	0.53	49.30			0.019	8.26	274.50			0.039	20	3.94	1.16	9.42	20.26	9.42	2.38	3.16	3.90 5.1	2 6	6.17 7.37	10.61	1 0.43	0.59	0.77	1.12	1.55	2.09	3.60
																-													-	=	+	-				\rightarrow		

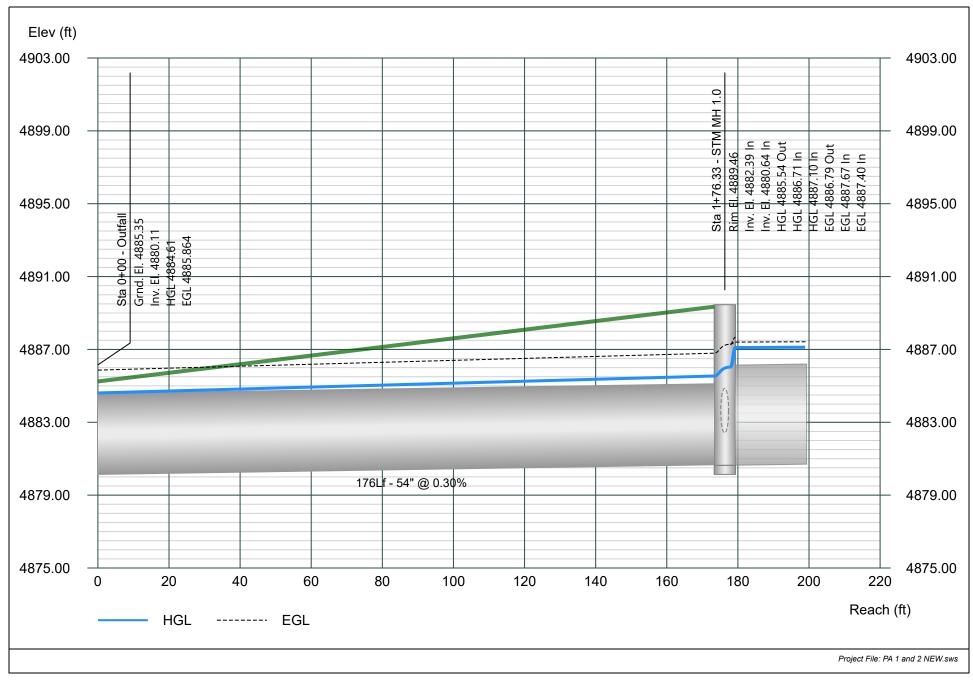
Plan View

Stormwater Studio 2021 v 3.0.0.24



Line 1 - Pipe - (110) (1) (Storm Sewer PAs 1 and 2)

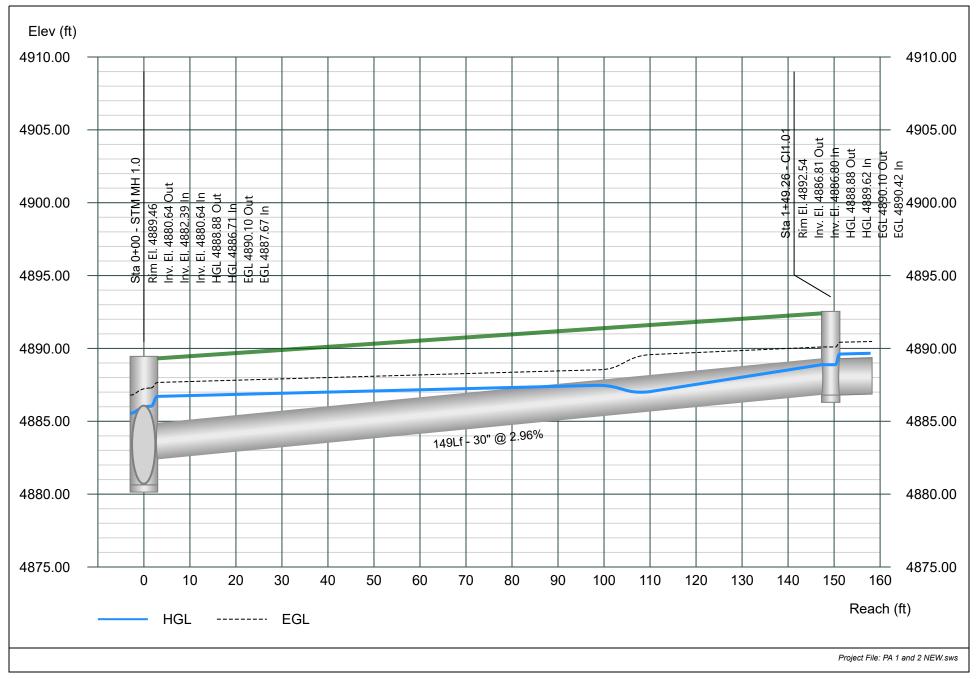
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 2 - Pipe - (362) (Storm Sewer PAs 1 and 2)

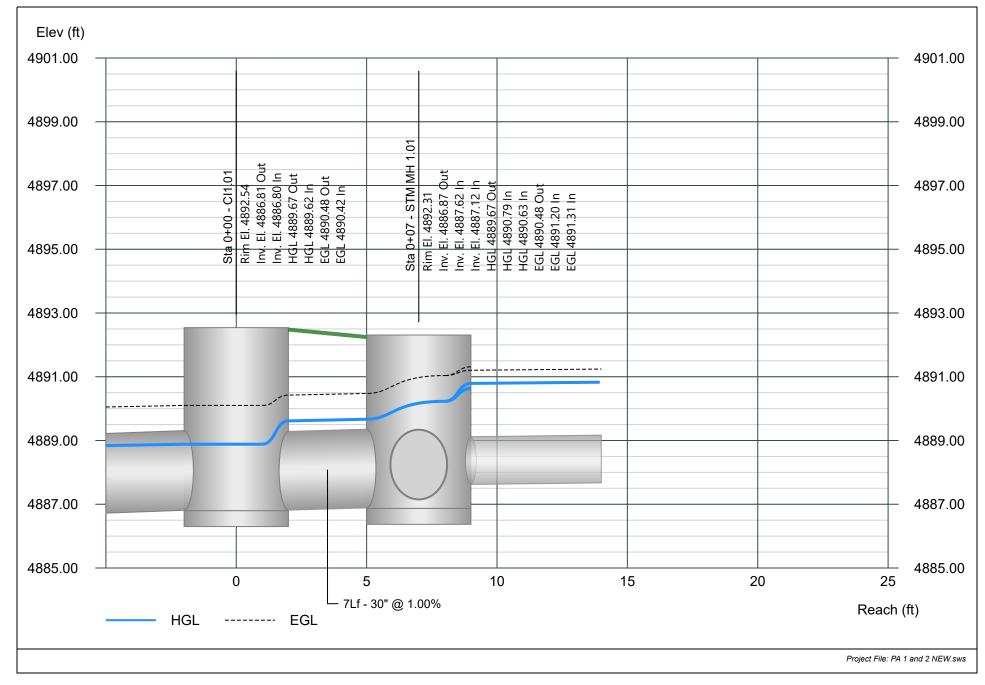
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 3 - Pipe - (361) (Storm Sewer PAs 1 and 2)

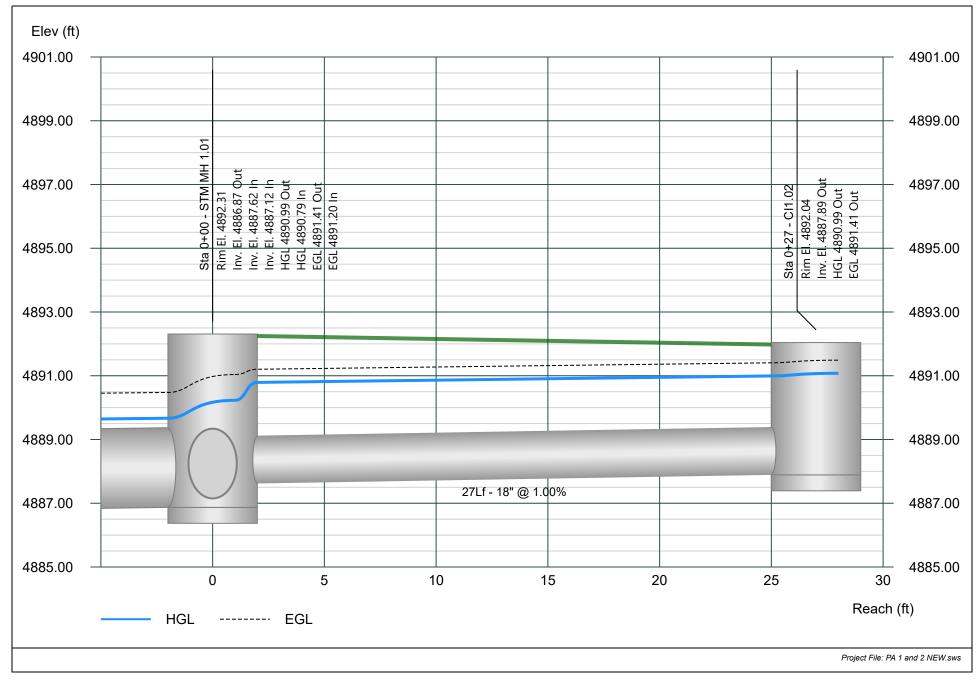
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 4 - Pipe - (364) (Storm Sewer PAs 1 and 2)

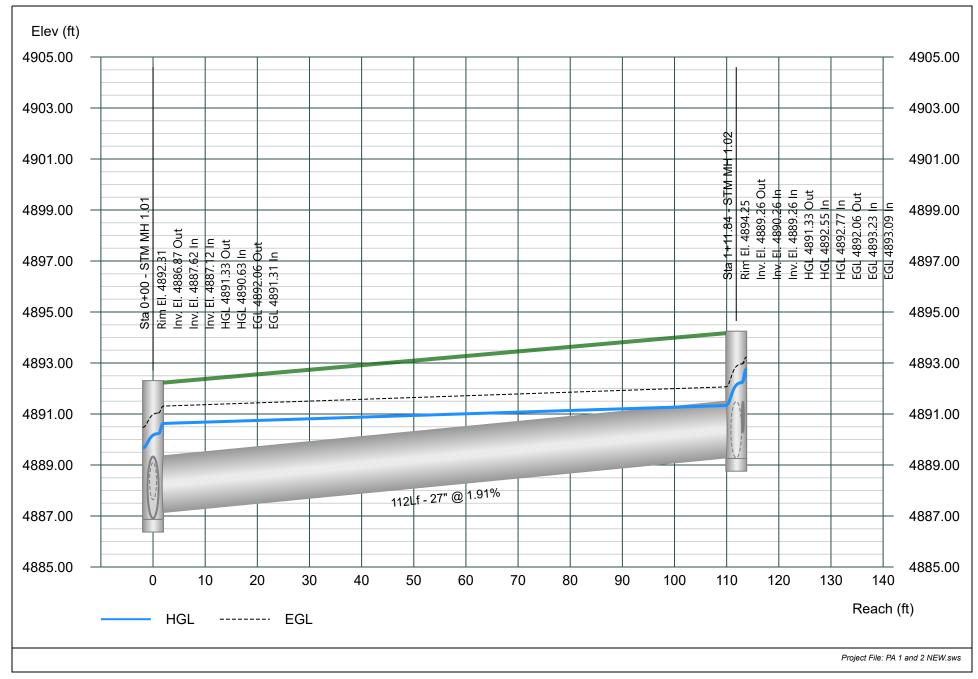
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 5 - Pipe - (360) (Storm Sewer PAs 1 and 2)

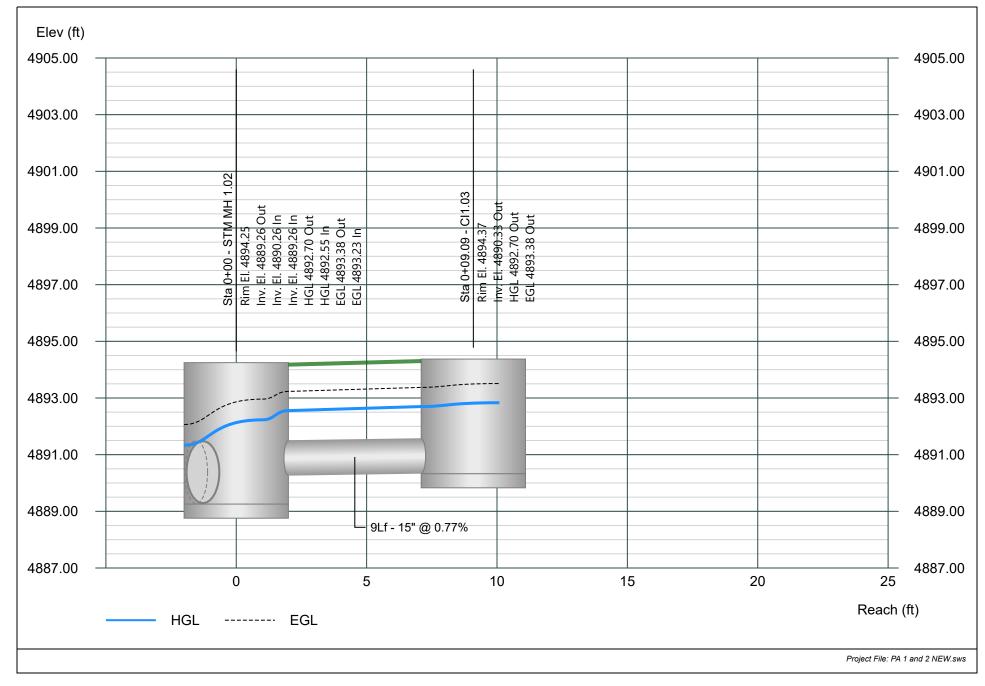
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 6 - Pipe - (363) (Storm Sewer PAs 1 and 2)

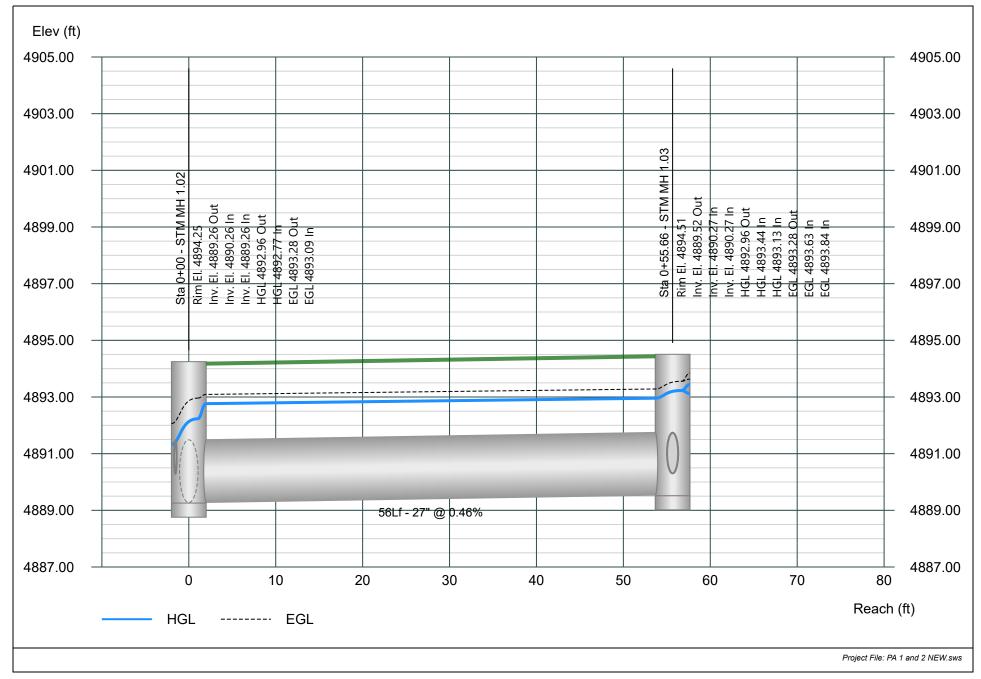
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 7 - Pipe - (359) (Storm Sewer PAs 1 and 2)

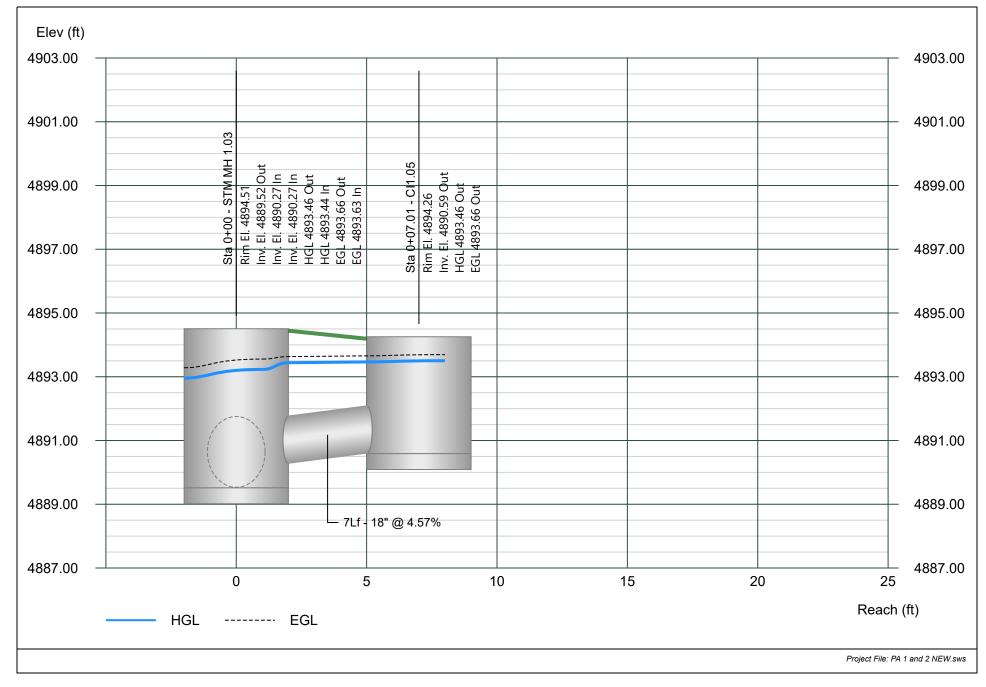
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 8 - Pipe - (578) (Storm Sewer PAs 1 and 2)

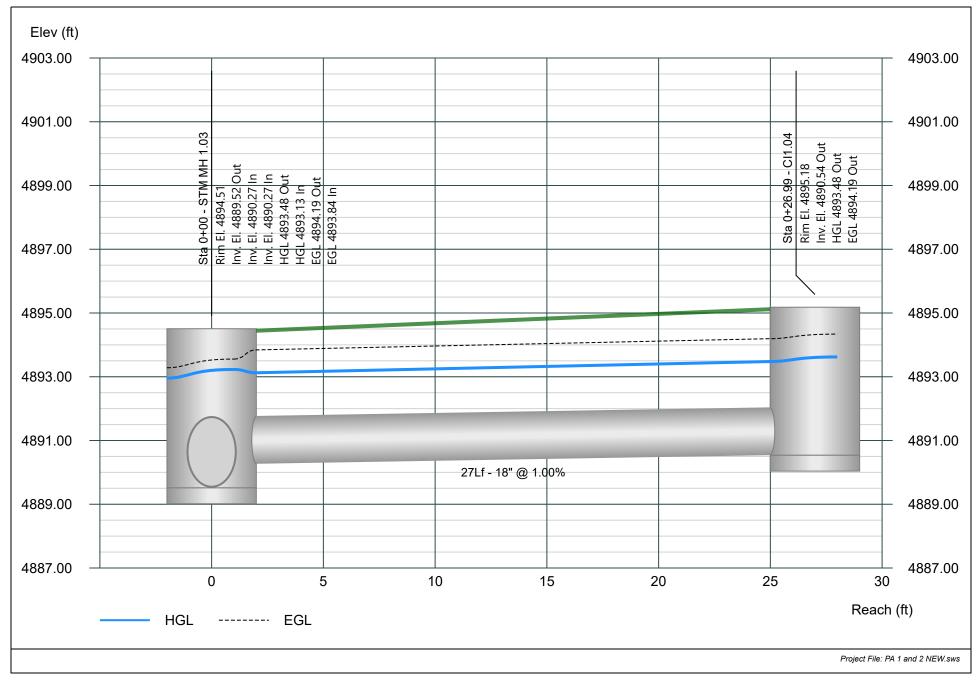
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

Line 9 - Pipe - (358) (Storm Sewer PAs 1 and 2)

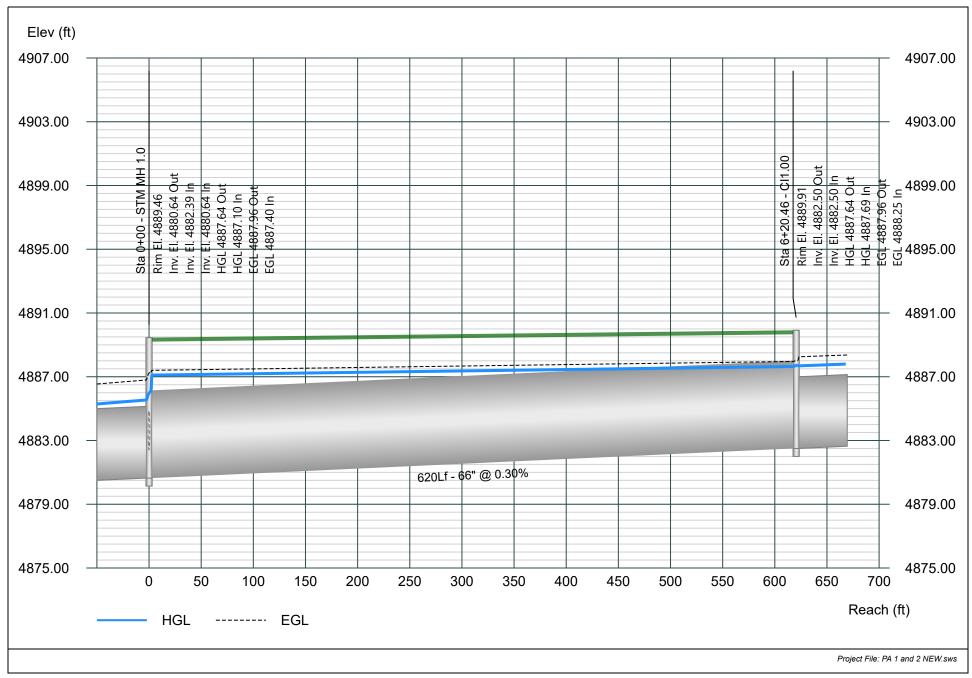
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

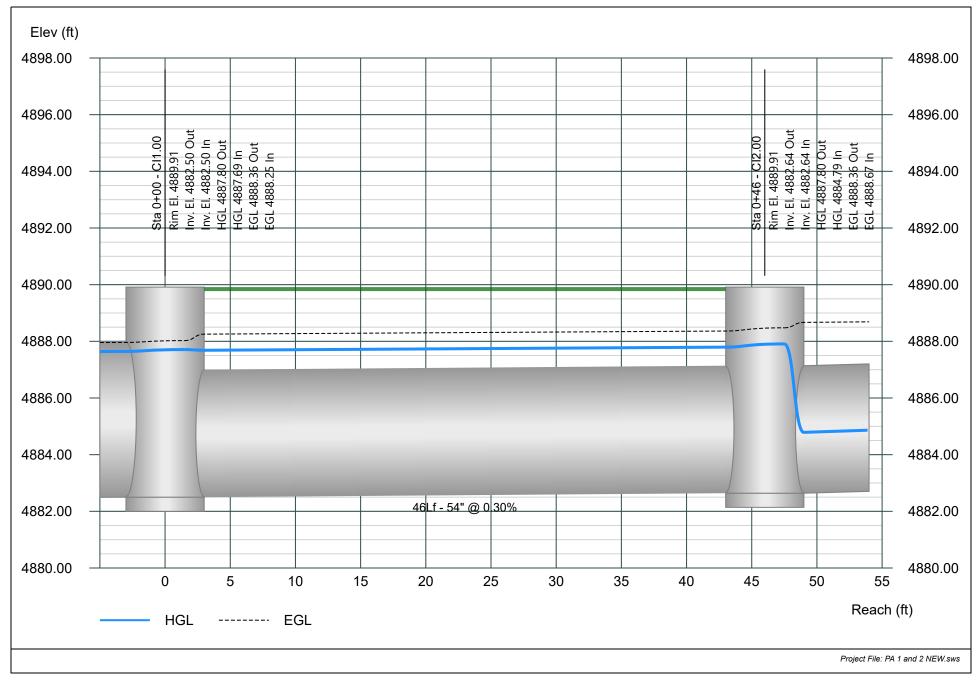
Line 10 - Pipe - (110) (Storm Sewer PAs 1 and 2)

Stormwater Studio 2021 v 3.0.0.24

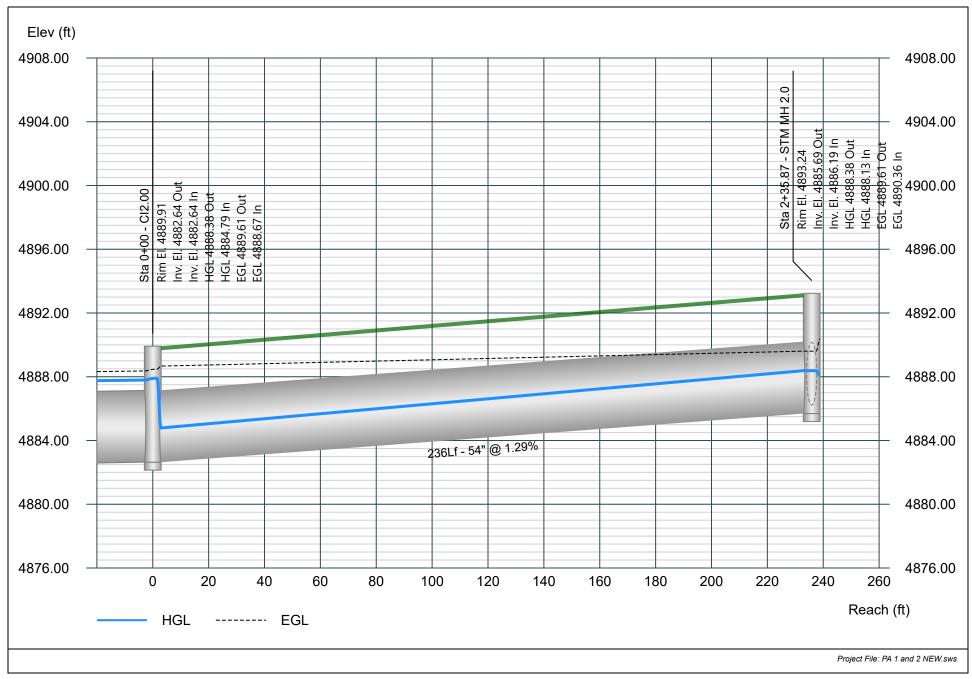


Project Name: Pioneer Village- PA 1 and 2

Line 11 - Pipe - (109) (Storm Sewer PAs 1 and 2)

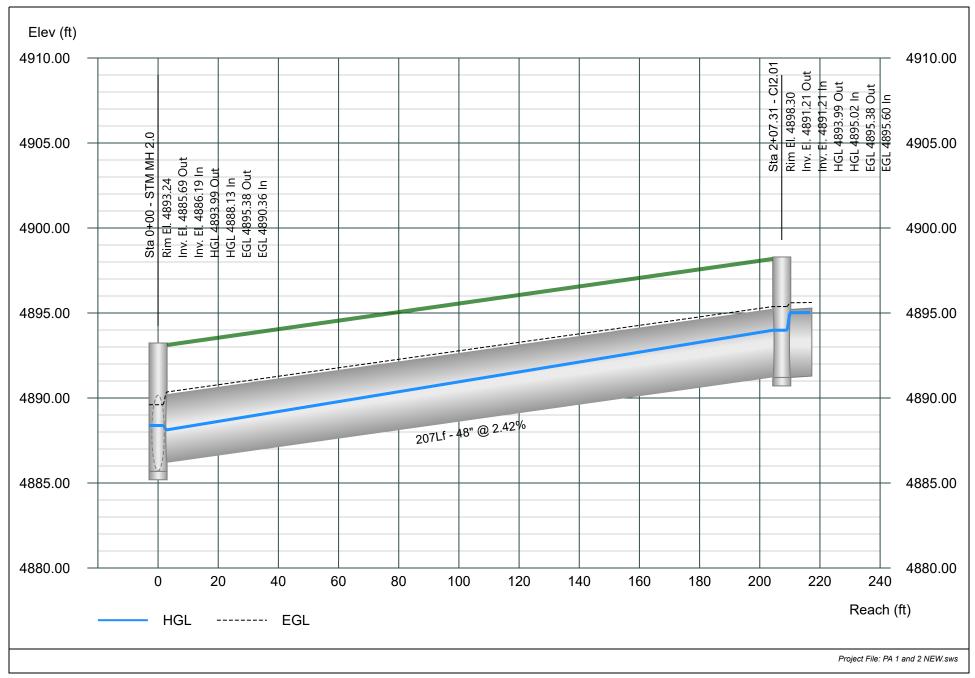


Line 12 - Pipe - (108) (Storm Sewer PAs 1 and 2)



Line 13 - Pipe - (107) (Storm Sewer PAs 1 and 2)

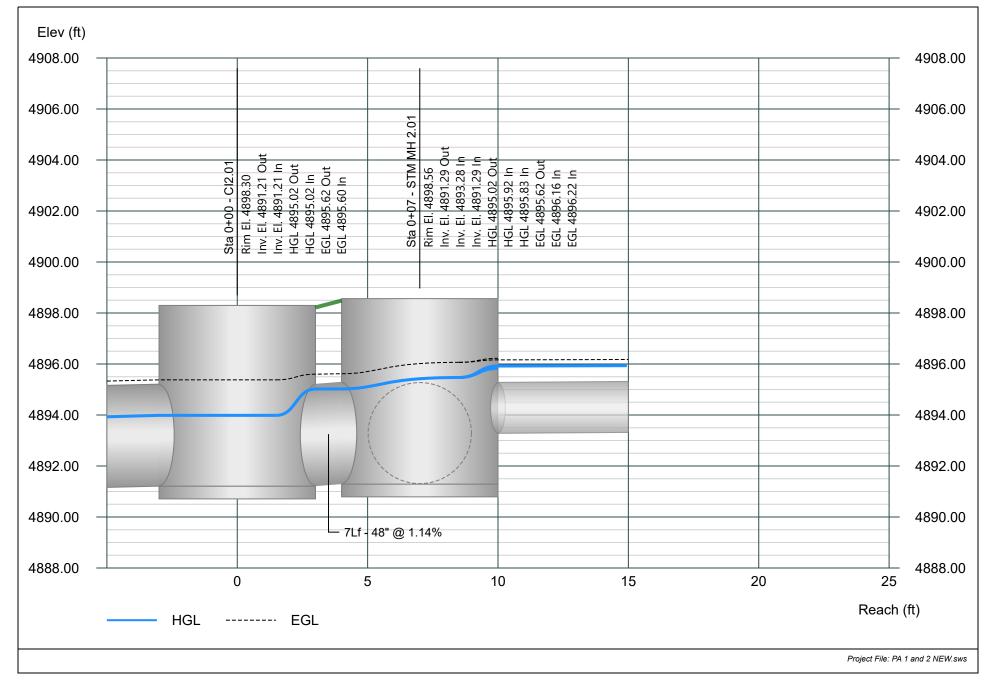
Stormwater Studio 2021 v 3.0.0.24



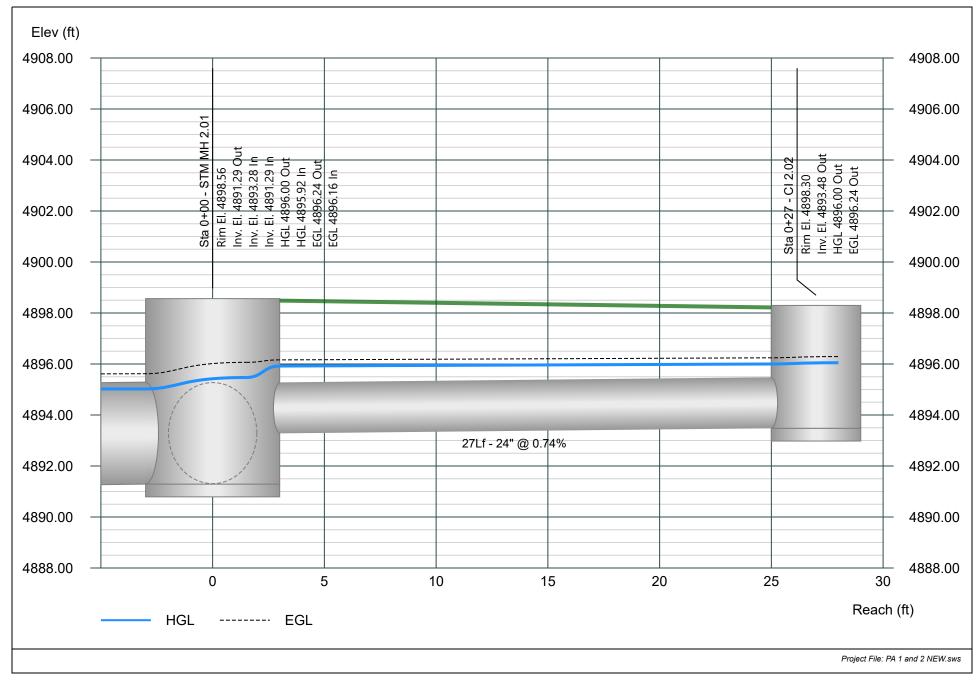
Project Name: Pioneer Village- PA 1 and 2

Line 14 - Pipe - (106) (Storm Sewer PAs 1 and 2)

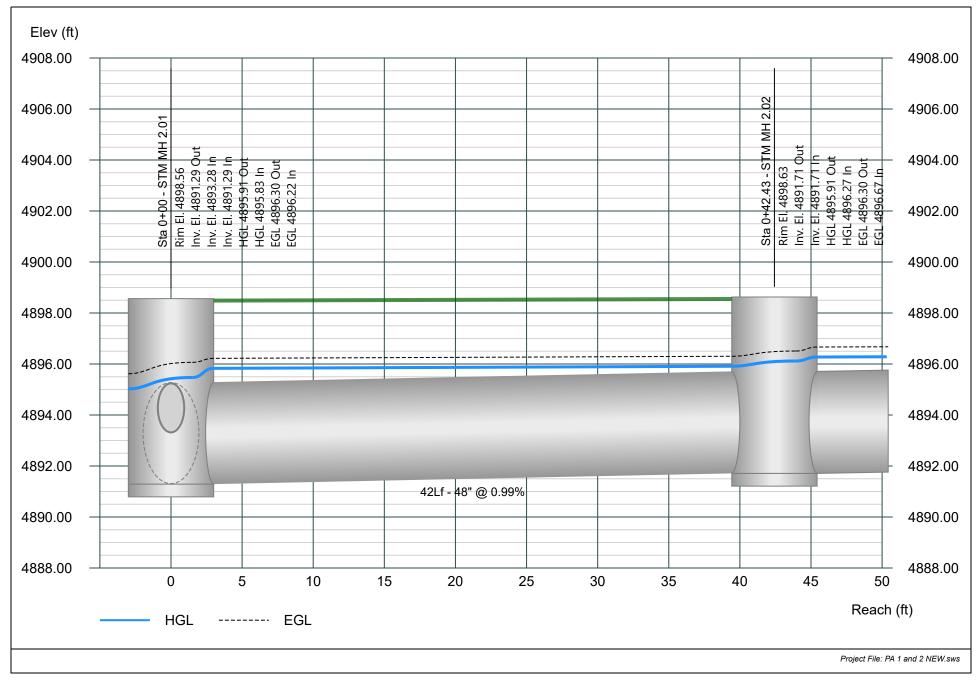
Stormwater Studio 2021 v 3.0.0.24



Line 15 - Pipe - (354) (Storm Sewer PAs 1 and 2)

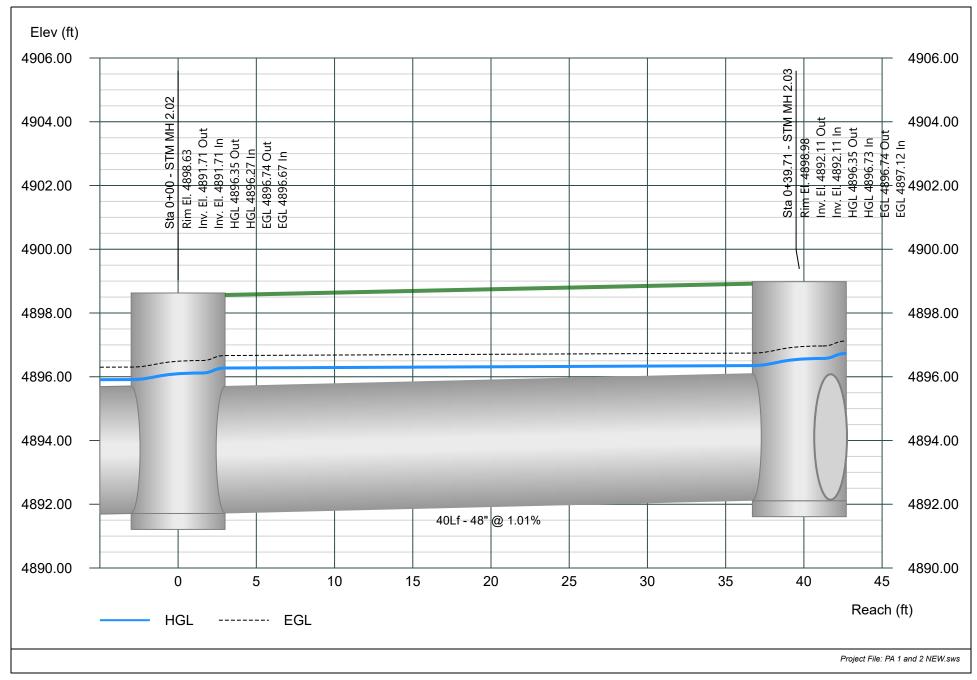


Line 16 - Pipe - (105) (Storm Sewer PAs 1 and 2)



Line 17 - Pipe - (104) (Storm Sewer PAs 1 and 2)

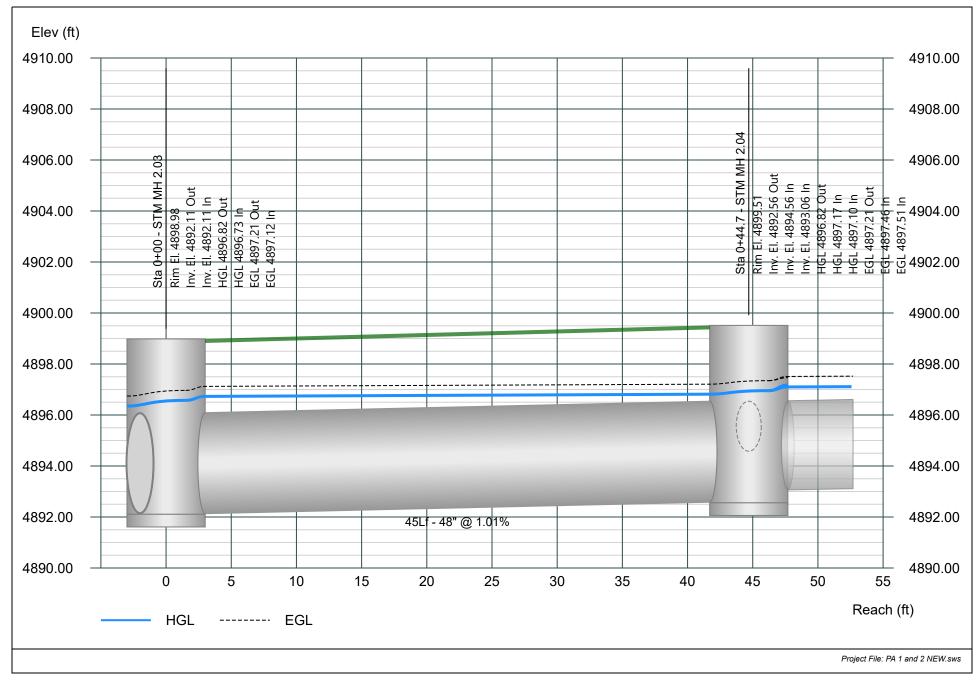
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

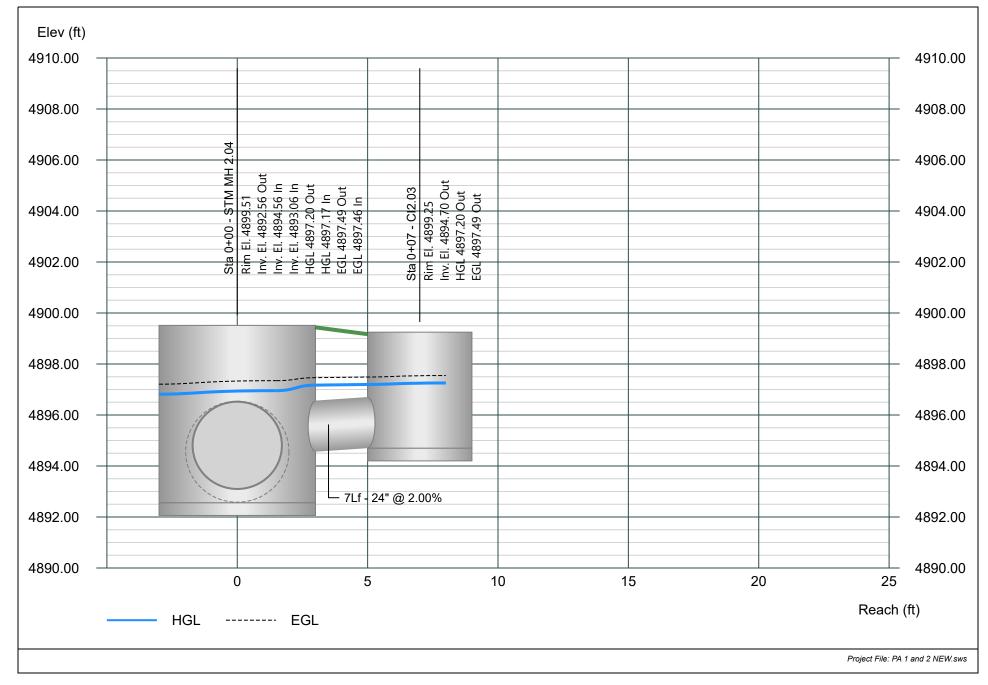
Line 18 - Pipe - (103) (Storm Sewer PAs 1 and 2)

Stormwater Studio 2021 v 3.0.0.24

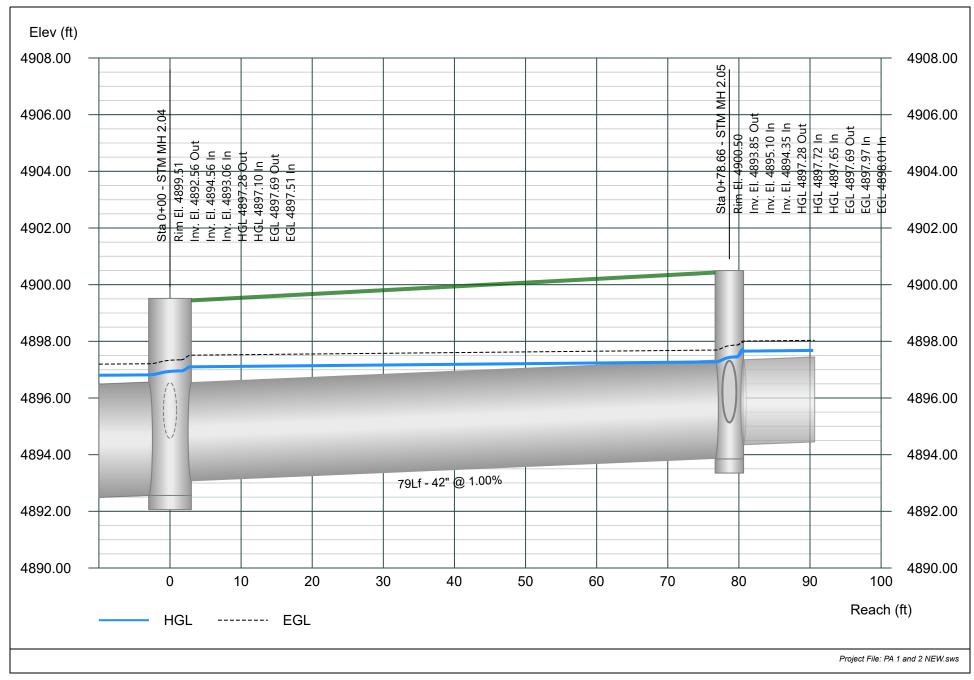


Project Name: Pioneer Village- PA 1 and 2

Line 19 - Pipe - (366) (Storm Sewer PAs 1 and 2)

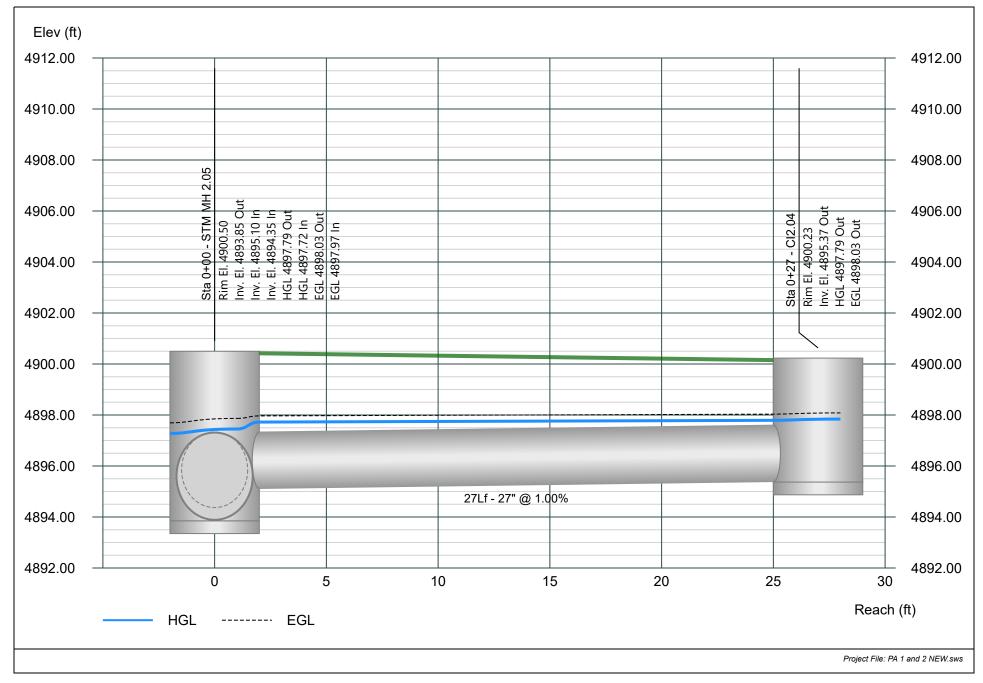


Line 20 - Pipe - (102) (Storm Sewer PAs 1 and 2)

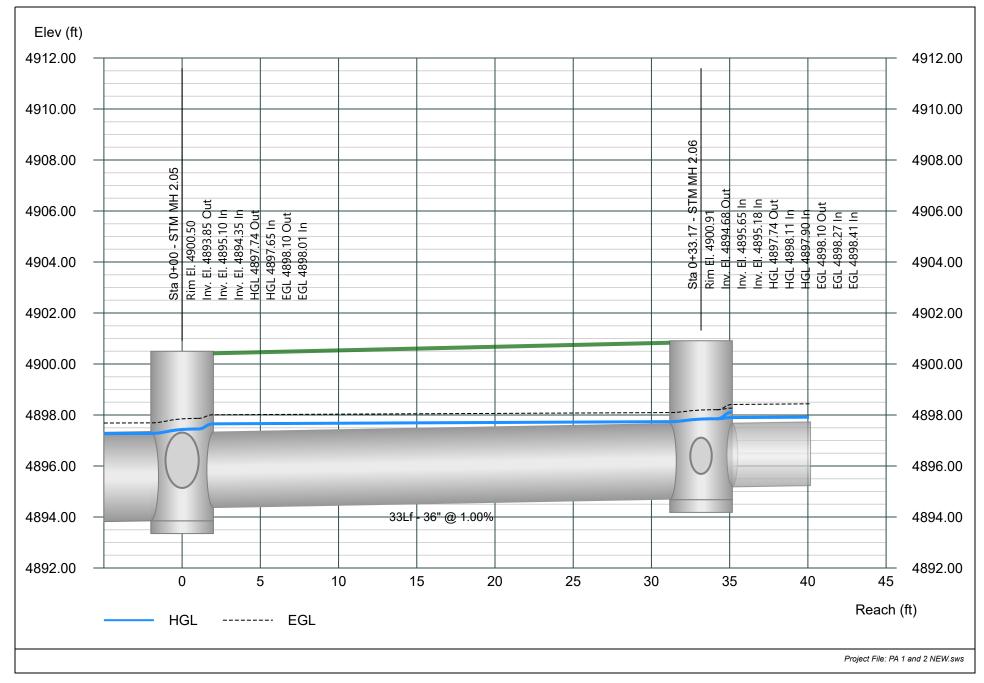


Line 21 - Pipe - (101) (Storm Sewer PAs 1 and 2)

Stormwater Studio 2021 v 3.0.0.24

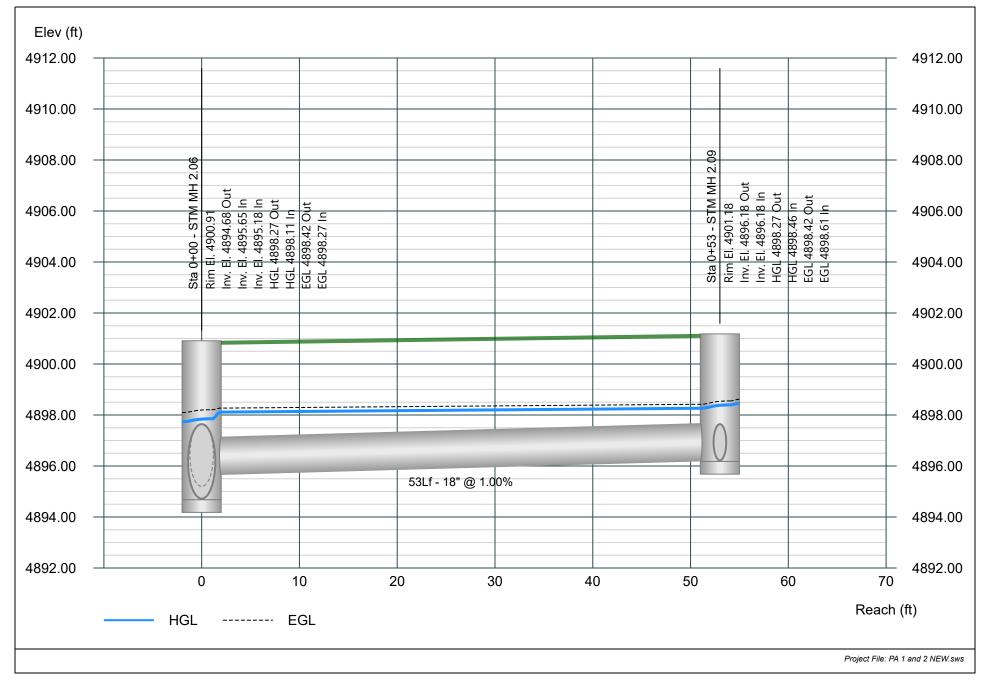


Line 22 - Pipe - (576) (1) (Storm Sewer PAs 1 and 2)



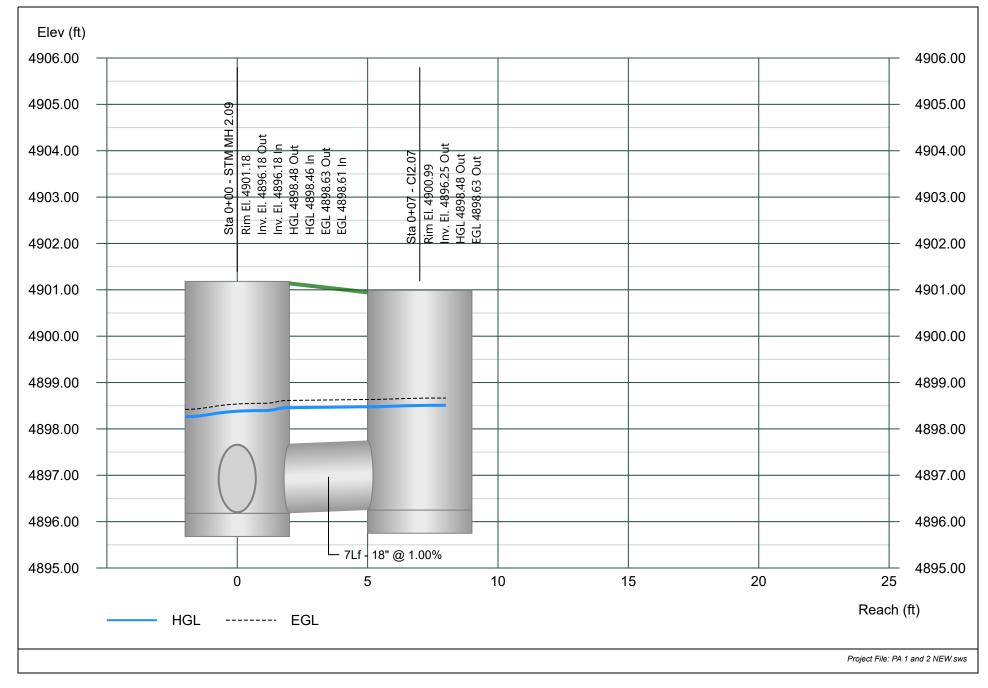
Line 23 - Pipe - (580) (Storm Sewer PAs 1 and 2)

Stormwater Studio 2021 v 3.0.0.24



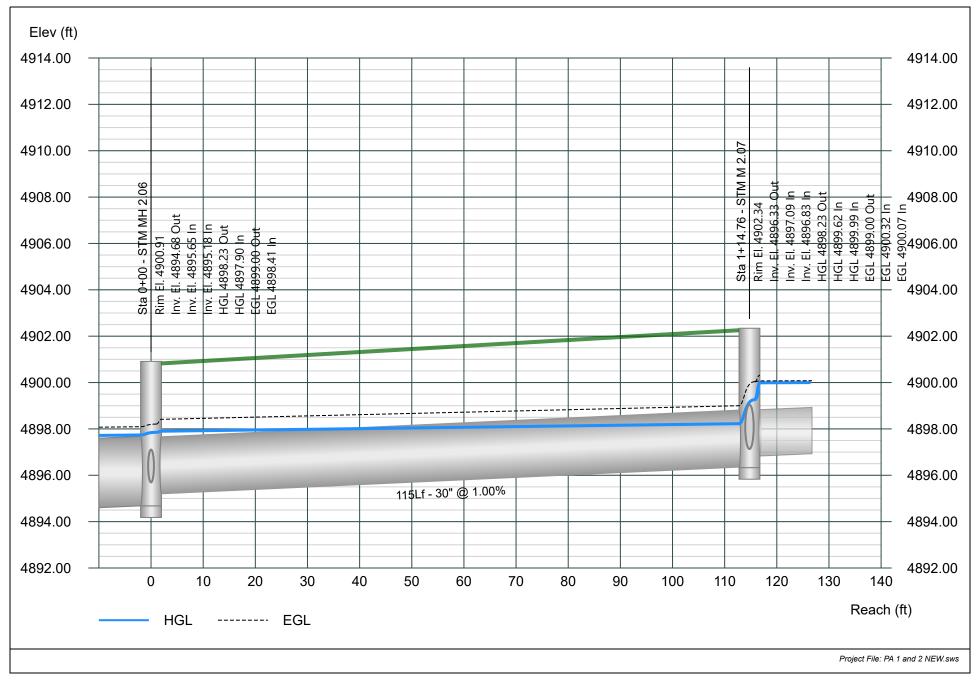
Line 24 - Pipe - (579) (Storm Sewer PAs 1 and 2)

Stormwater Studio 2021 v 3.0.0.24

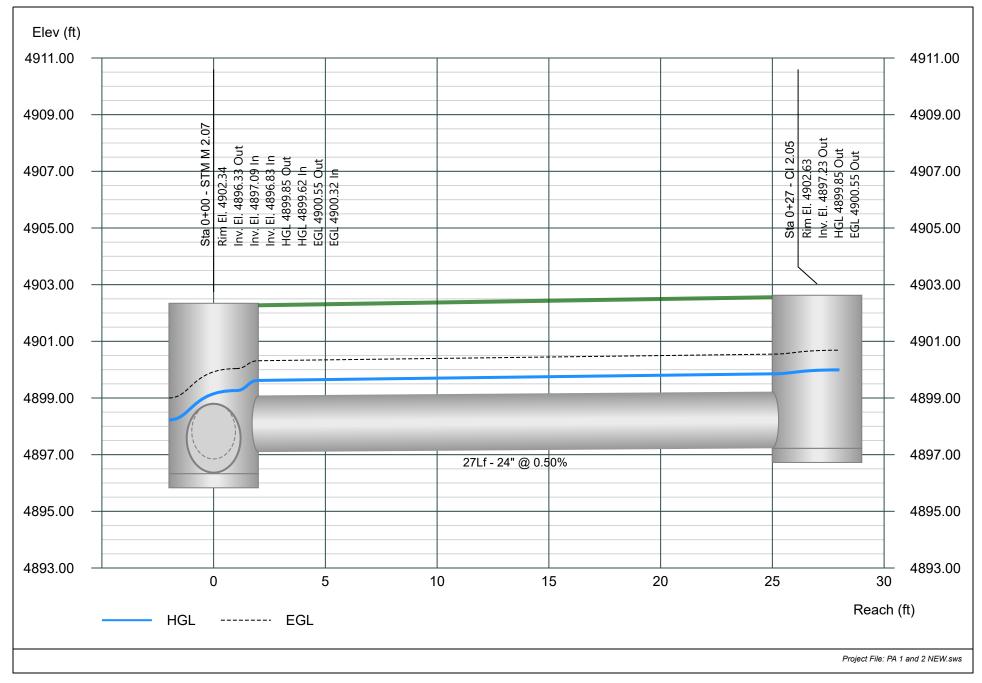


Project Name: Pioneer Village- PA 1 and 2

Line 25 - Pipe - (576) (Storm Sewer PAs 1 and 2)



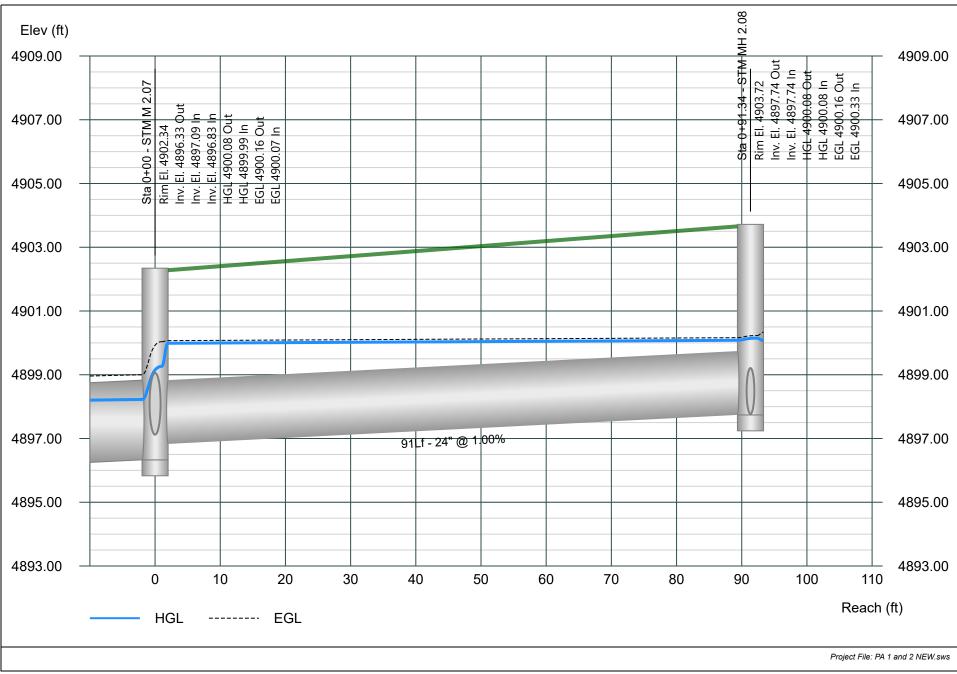
Line 26 - Pipe - (577) (Storm Sewer PAs 1 and 2)



Line 27 - Pipe - (575) (Storm Sewer PAs 1 and 2)

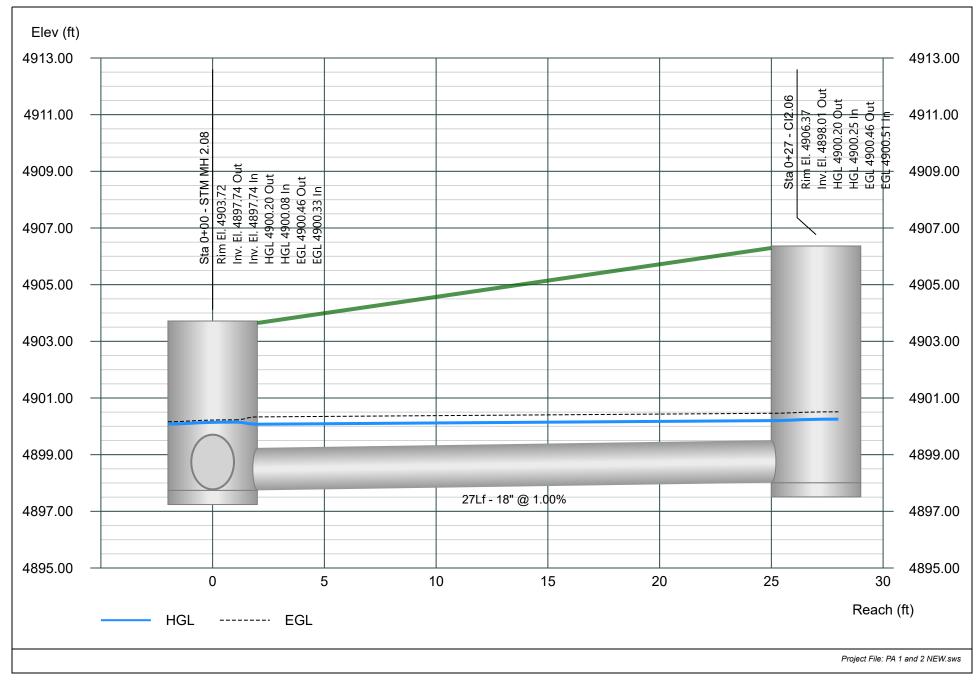
Project Name: Pioneer Village- PA 1 and 2

03-24-2021



Line 28 - Pipe - (574) (Storm Sewer PAs 1 and 2)

Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village- PA 1 and 2

03-24-2021

Energy Grade Line Calculations

Stormwater Studio 2021 v 3.0.0.24

Line	Line				Do	ownstrea	m			Length			ι	Jpstream	ı			Pi	ре		Junction	1
No	Size	Q	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	Len	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	n Value	Enrgy Loss	HGLa Elev	EGLa Elev	Enrgy Loss
	(in)	(cfs)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)		(ft)	(ft)	(ft)	(ft)
1	54	142.80	4880.11	4.50 ³	15.90	4884.61	8.98	1.25	4885.86	176.33	4880.64	4.50	15.90	4885.54	8.98	1.25	4886.79	0.013	0.930	4886.03	4887.28	0.49
2	30	38.50	4882.39	2.50	4.91	4886.71	7.84	0.96	4887.67	149.26	4886.81	2.07²	4.35	4888.88	8.84	1.22	4890.10	0.013	2.435	4888.88	4890.10	0.00
3	30	35.40	4886.80	2.50	4.91	4889.62	7.21	0.81	4890.42	7.00	4886.87	2.50	4.91	4889.67	7.21	0.81	4890.48	0.013	0.052	4890.23	4891.04	0.56
4	18	9.10	4887.62	1.50	1.77	4890.79	5.15	0.41	4891.20	27.00	4887.89	1.50	1.77	4890.99	5.15	0.41	4891.41	0.013	0.203	4891.08	4891.49	0.08
5	27	26.30	4887.12	2.25	3.98	4890.63	6.62	0.68	4891.31	111.84	4889.26	2.08	3.83	4891.33	6.86	0.73	4892.06	0.013	0.753	4892.23	4892.96	0.90
6	15	8.10	4890.26	1.25 ³	1.23	4892.55	6.60	0.68	4893.23	9.09	4890.33	1.25	1.23	4892.70	6.60	0.68	4893.38	0.013	0.143	4892.83	4893.51	0.14
7	27	18.20	4889.26	2.25	3.98	4892.77	4.58	0.33	4893.09	55.66	4889.52	2.25	3.98	4892.96	4.58	0.33	4893.28	0.013	0.192	4893.23	4893.56	0.27
8	18	6.20	4890.27	1.50	1.77	4893.44	3.51	0.19	4893.63	7.01	4890.59	1.50	1.77	4893.46	3.51	0.19	4893.66	0.013	0.024	4893.50	4893.69	0.04
9	18	12.00	4890.27	1.50 ³	1.77	4893.13	6.79	0.72	4893.84	26.99	4890.54	1.50	1.77	4893.48	6.79	0.72	4894.19	0.013	0.353	4893.62	4894.34	0.14
10	66	104.30	4880.64	5.50	23.75	4887.10	4.39	0.30	4887.40	620.46	4882.50	5.14	23.11	4887.64	4.51	0.32	4887.96	0.013	0.557	4887.71	4888.03	0.07
11	54	96.20	4882.50	4.50	15.90	4887.69	6.05	0.57	4888.25	46.00	4882.64	4.50	15.90	4887.80	6.05	0.57	4888.36	0.013	0.110	4887.91	4888.48	0.11
12	54	88.10	4882.64	2.15‡	7.49	4884.79	11.76	2.15	4888.67	235.87	4885.69	2.69²	9.93	4888.38	8.87	1.22	4889.61	0.013	0.938	4888.38	4889.61	0.00
13	48	88.10	4886.19	1.94‡	6.04	4888.13	14.59	3.31	4890.36	207.31	4891.21	2.78²	9.31	4893.99	9.46	1.39	4895.38	0.013	5.023	4893.99	4895.38	0.00
14	48	75.50	4891.21	3.81	12.35	4895.02	6.11	0.58	4895.60	7.00	4891.29	3.73	12.21	4895.02	6.18	0.59	4895.62	0.013	0.018	4895.47	4896.07	0.45
15	24	12.40	4893.28	2.00	3.14	4895.92	3.95	0.24	4896.16	27.00	4893.48	2.00	3.14	4896.00	3.95	0.24	4896.24	0.013	0.081	4896.05	4896.29	0.05
16	48	63.10	4891.29	4.00	12.56	4895.83	5.02	0.39	4896.22	42.43	4891.71	4.00	12.57	4895.91	5.02	0.39	4896.30	0.013	0.082	4896.12	4896.51	0.21
17	48	63.10	4891.71	4.00	12.56	4896.27	5.02	0.39	4896.67	39.71	4892.11	4.00	12.57	4896.35	5.02	0.39	4896.74	0.013	0.077	4896.57	4896.97	0.22
18	48	63.10	4892.11	4.00	12.56	4896.73	5.02	0.39	4897.12	44.70	4892.56	4.00	12.57	4896.82	5.02	0.39	4897.21	0.013	0.086	4896.96	4897.35	0.14
19	24	13.60	4894.56	2.00	3.14	4897.17	4.33	0.29	4897.46	7.00	4894.70	2.00	3.14	4897.20	4.33	0.29	4897.49	0.013	0.025	4897.26	4897.55	0.06
20	42	49.50	4893.06	3.50	9.62	4897.10	5.15	0.41	4897.51	78.66	4893.85	3.43	9.57	4897.28	5.17	0.42	4897.69	0.013	0.181	4897.45	4897.87	0.18
21	27	15.70	4895.10	2.25	3.98	4897.72	3.95	0.24	4897.97	27.00	4895.37	2.25	3.98	4897.79	3.95	0.24	4898.03	0.013	0.069	4897.84	4898.08	0.05
22	36	33.80	4894.35	3.00	7.07	4897.65	4.78	0.36	4898.01	33.17	4894.68	3.00	7.07	4897.74	4.78	0.36	4898.10	0.013	0.085	4897.85	4898.21	0.11
Notes:	² Critical dep	oth. ³ Nor	mal depth.	‡ Super	critical.							•								Project	File: PA 1 and	2 NEW.sws

Project Name: Enter Project Name...

03-24-2021

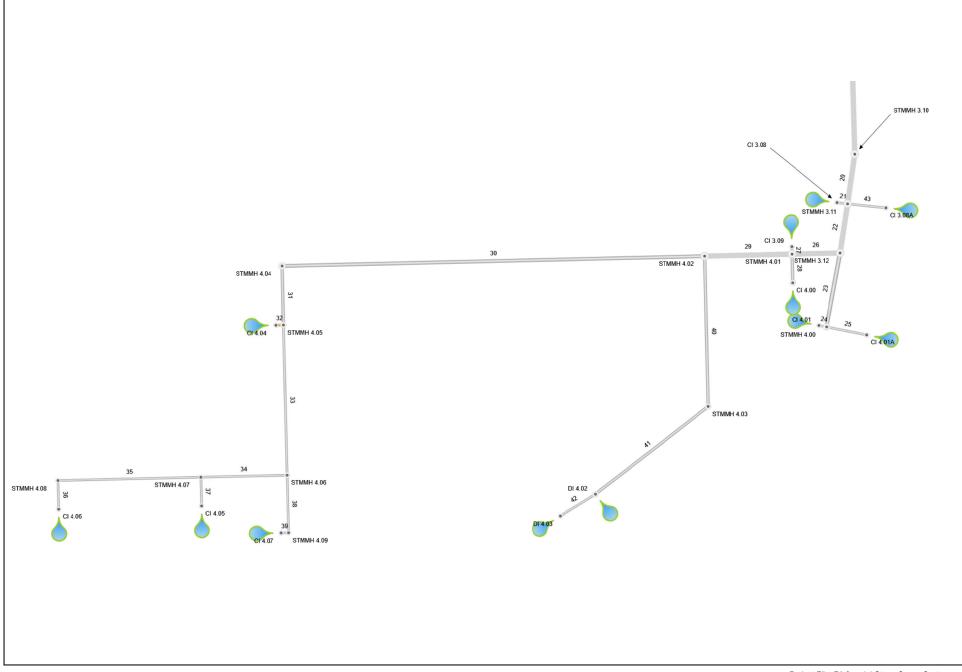
Energy Grade Line Calculations

Stormwater Studio 2021 v 3.0.0.24

Line	Line				De	ownstrea	ım			Length			ι	Jpstrean	ı			Pi	ре		Junction	l
No	Size	Q	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	Len	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	n Value	Enrgy Loss	HGLa Elev	EGLa Elev	Enrgy Loss
	(in)	(cfs)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)		(ft)	(ft)	(ft)	(ft)
23	18	5.60	4895.65	1.50	1.77	4898.11	3.17	0.16	4898.27	53.00	4896.18	1.50	1.77	4898.27	3.17	0.16	4898.42	0.013	0.151	4898.40	4898.55	0.13
24	18	5.60	4896.18	1.50	1.77	4898.46	3.17	0.16	4898.61	7.00	4896.25	1.50	1.77	4898.48	3.17	0.16	4898.63	0.013	0.020	4898.51	4898.67	0.03
25	30	28.20	4895.18	2.50	4.91	4897.90	5.75	0.51	4898.41	114.76	4896.33	1.90	3.99	4898.23	7.06	0.77	4899.00	0.013	0.588	4899.26	4900.04	1.04
26	24	21.00	4897.09	2.00 ³	3.14	4899.62	6.69	0.69	4900.32	27.00	4897.23	2.00	3.14	4899.85	6.68	0.69	4900.55	0.013	0.233	4899.99	4900.69	0.14
27	24	7.20	4896.83	2.00	3.14	4899.99	2.29	0.08	4900.07	91.34	4897.74	2.00	3.14	4900.08	2.29	0.08	4900.16	0.013	0.093	4900.15	4900.23	0.07
28	18	7.20	4897.74	1.50	1.77	4900.08	4.08	0.26	4900.33	27.00	4898.01	1.50	1.77	4900.20	4.07	0.26	4900.46	0.013	0.127	4900.25	4900.51	0.05
	³ Normal de																				File: PA 1 and	

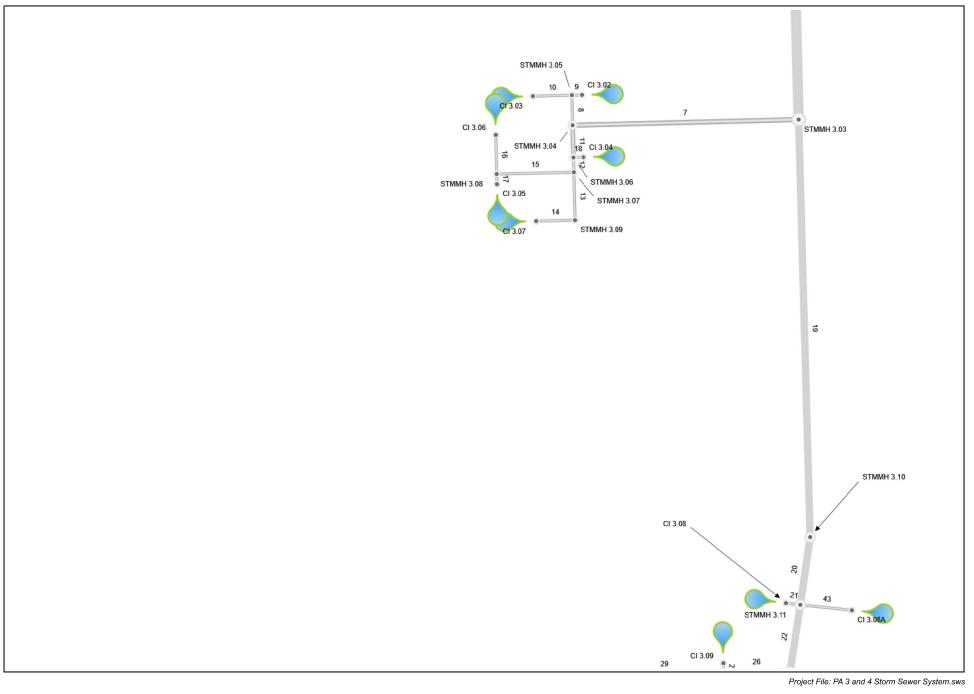
Project Name: Enter Project Name...

03-24-2021

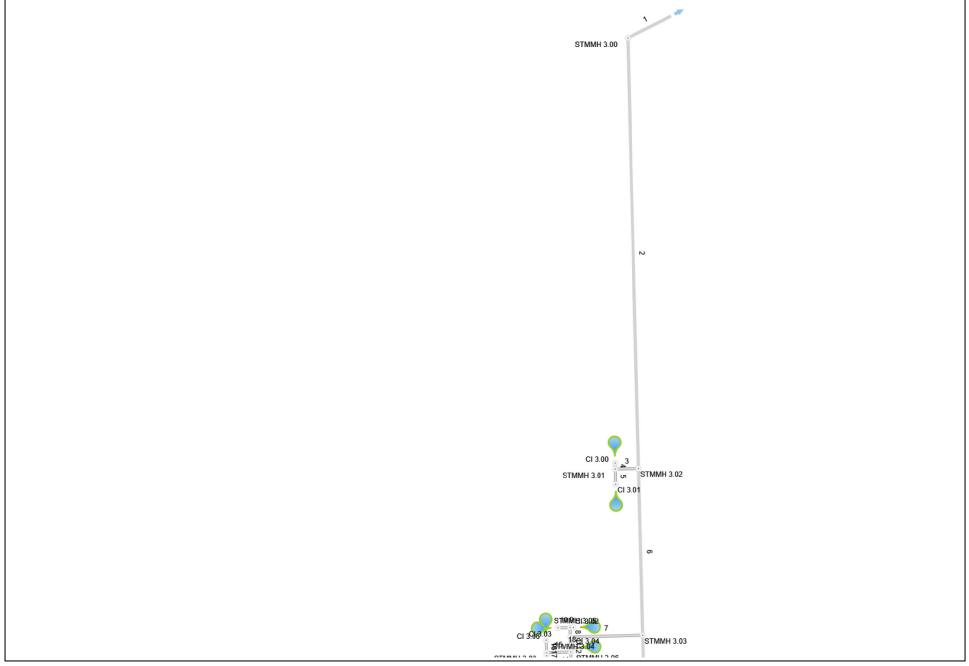


Plan View

Stormwater Studio 2021 v 3.0.0.24

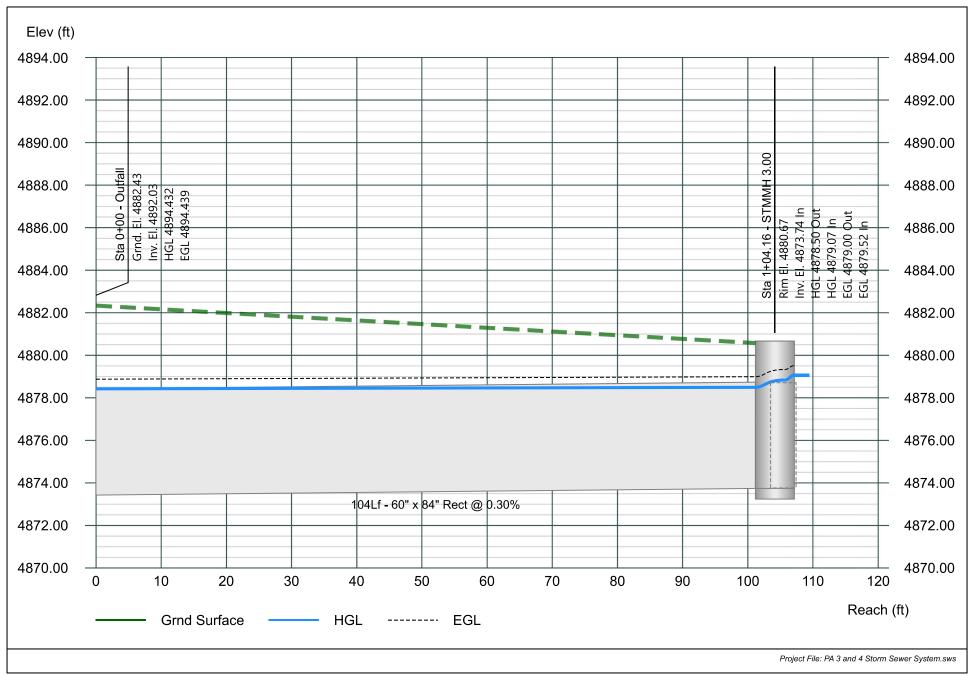


Stormwater Studio 2021 v 3.0.0.24

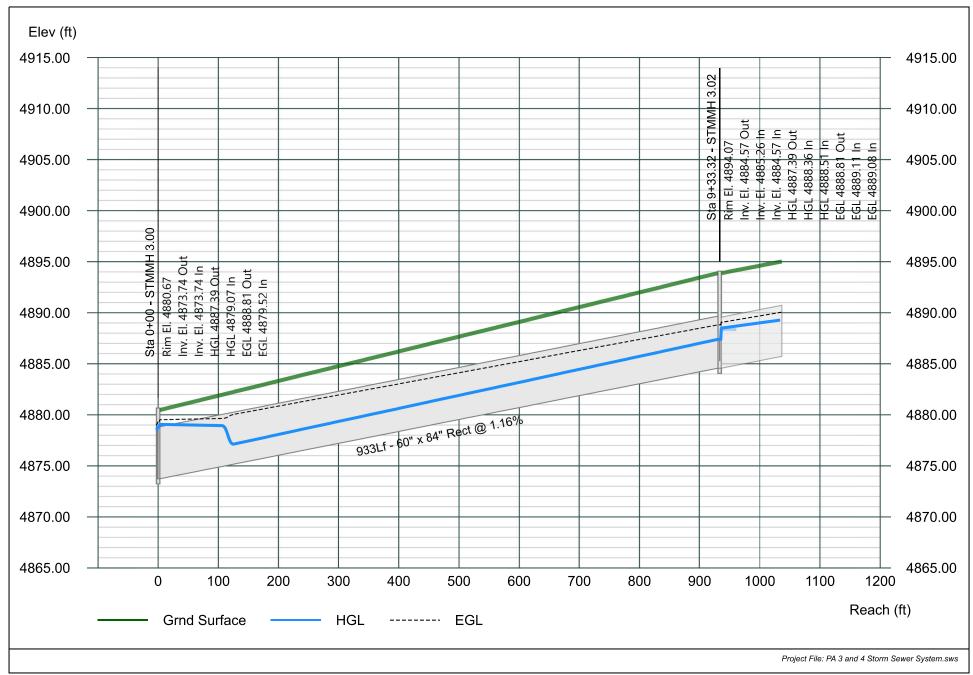


Line 1 - Pipe - (121) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

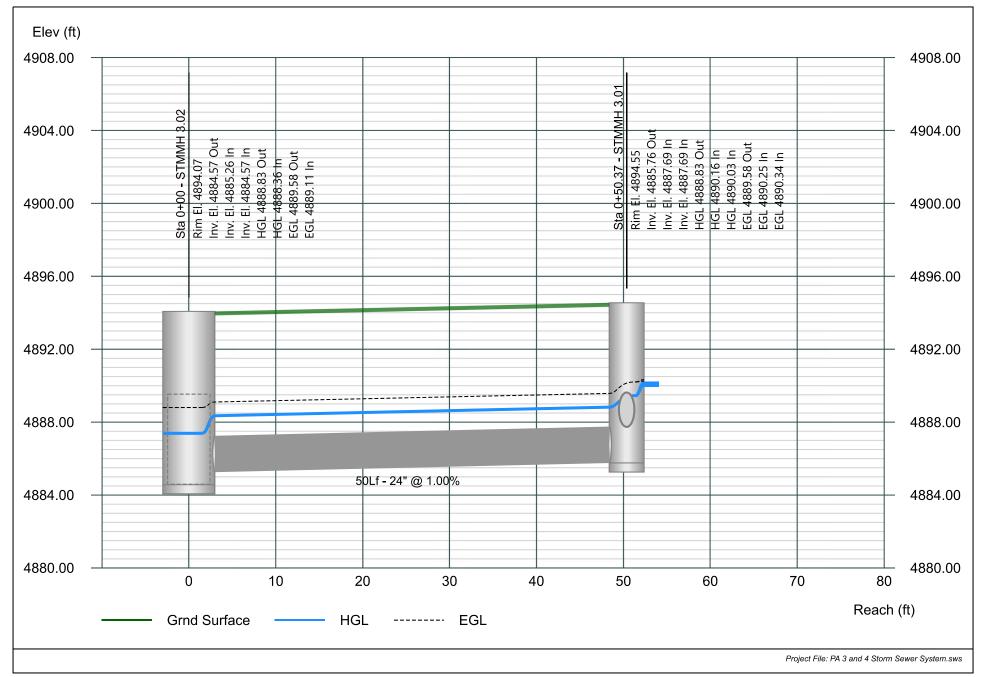


Line 2 - Pipe - (588) (PA 3 and 4 Storm Sewer Network)



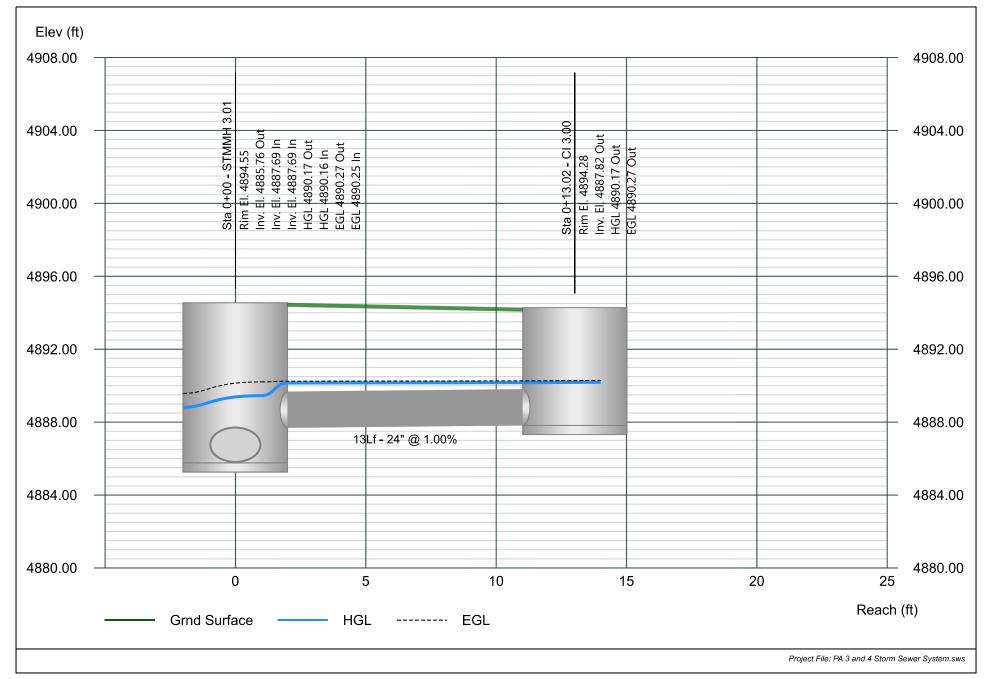
Line 3 - Pipe - (581) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



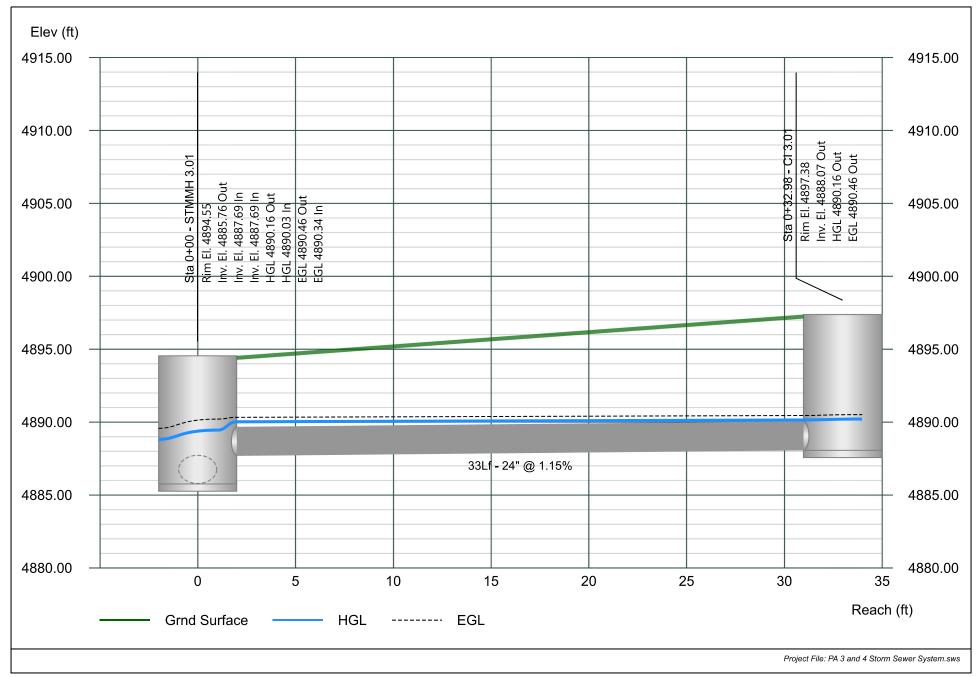
Line 4 - Pipe - (567) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

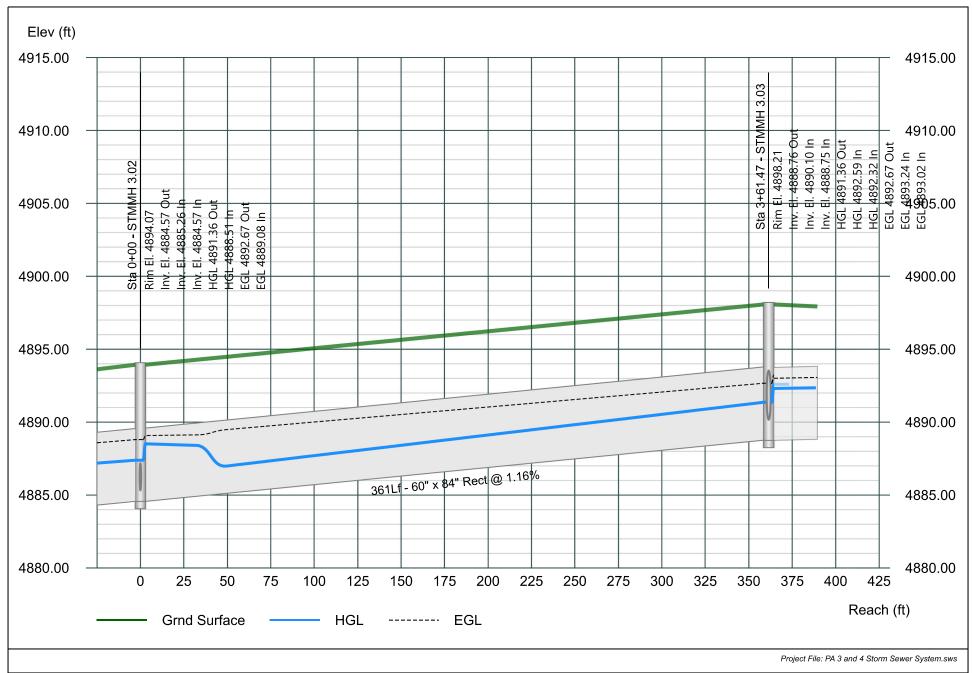


Line 5 - Pipe - (589) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

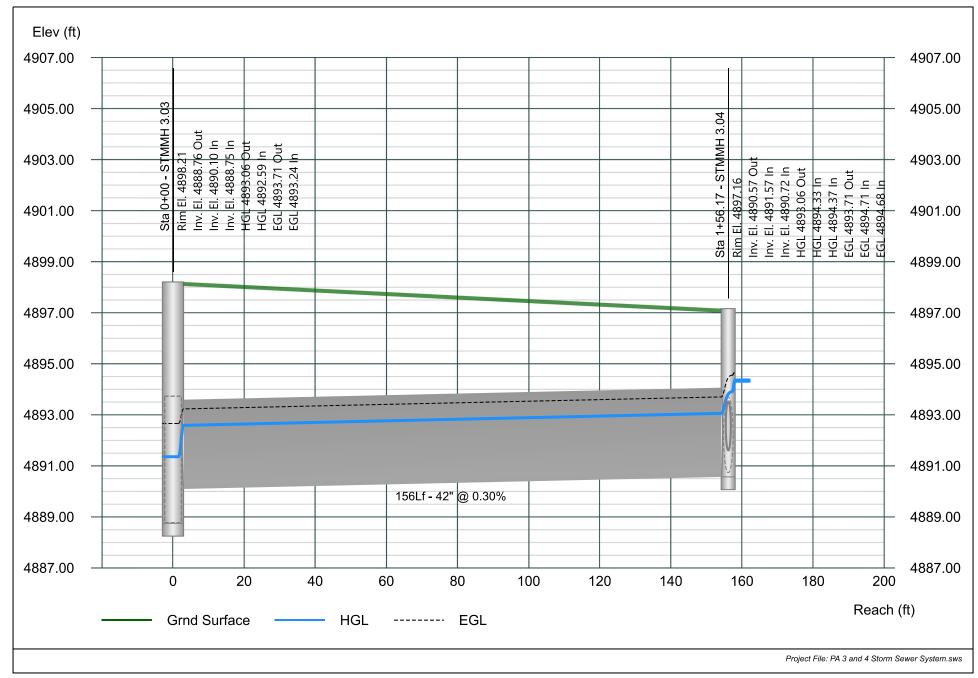


Line 6 - Pipe - (590) (PA 3 and 4 Storm Sewer Network)



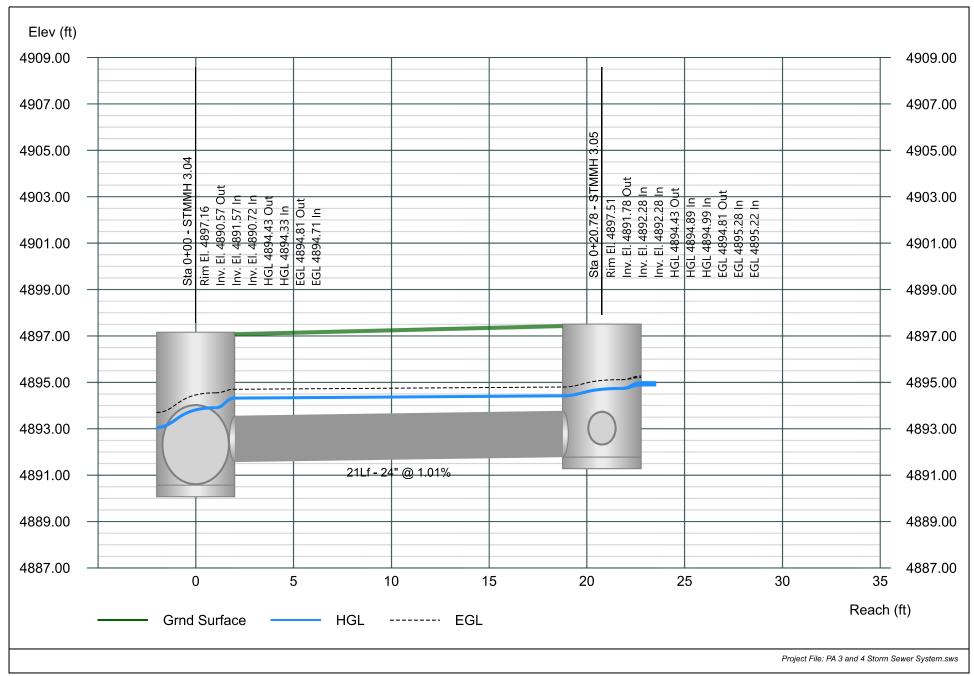
Line 7 - Pipe - (372) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



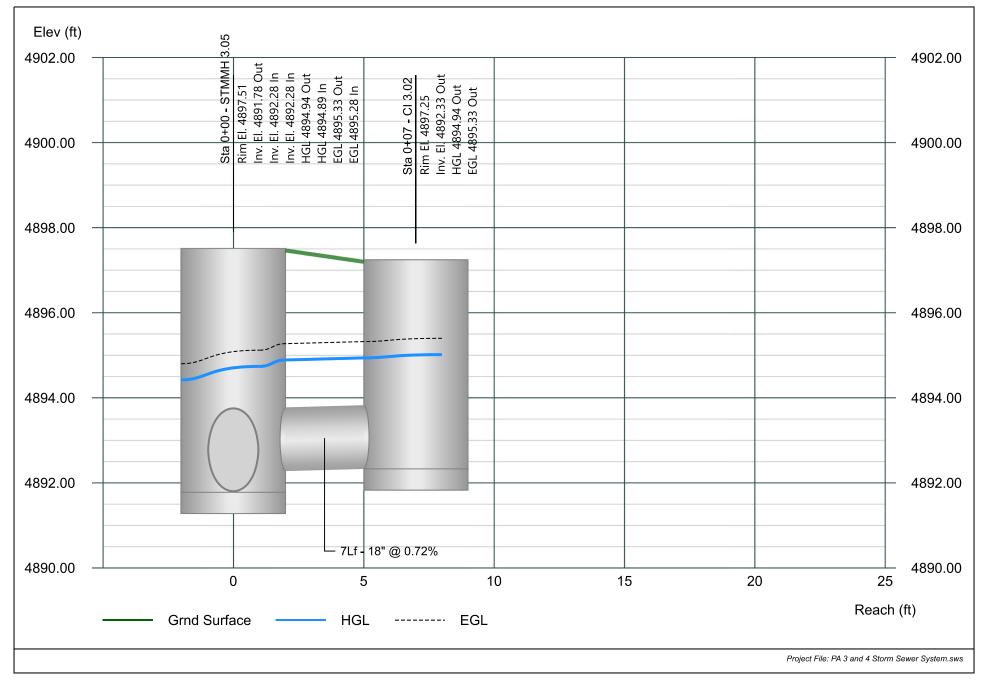
Line 8 - Pipe - (378) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

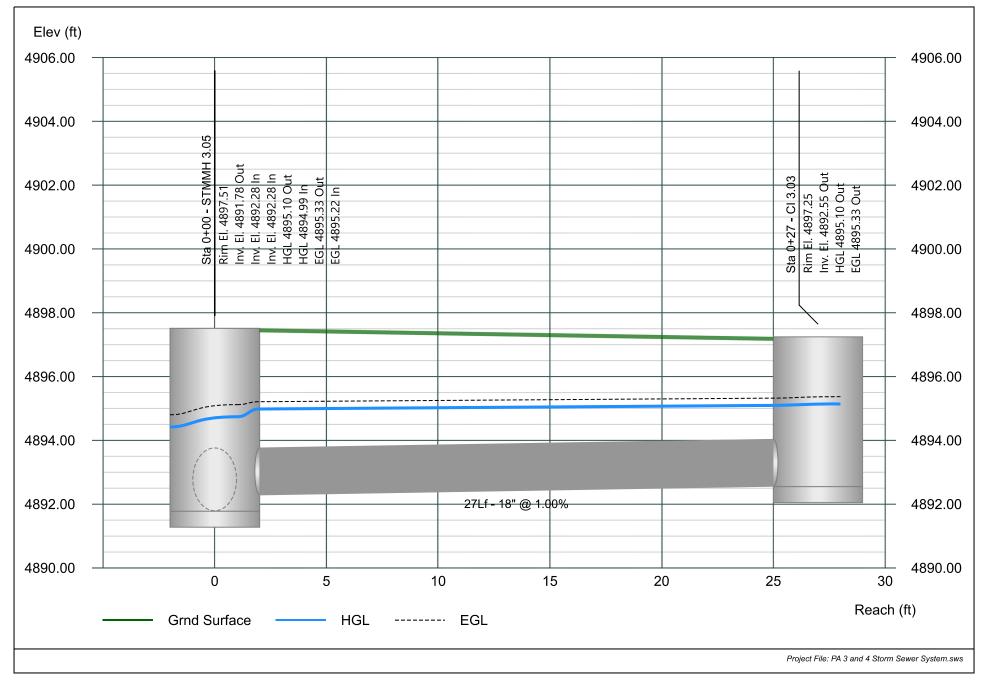


Line 9 - Pipe - (379) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

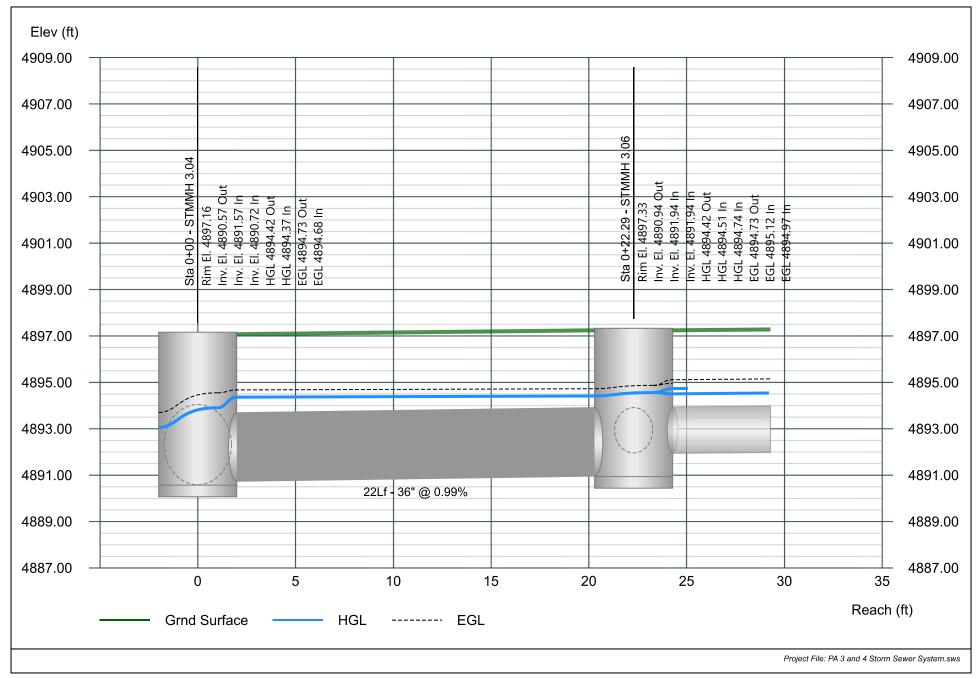


Line 10 - Pipe - (377) (PA 3 and 4 Storm Sewer Network)



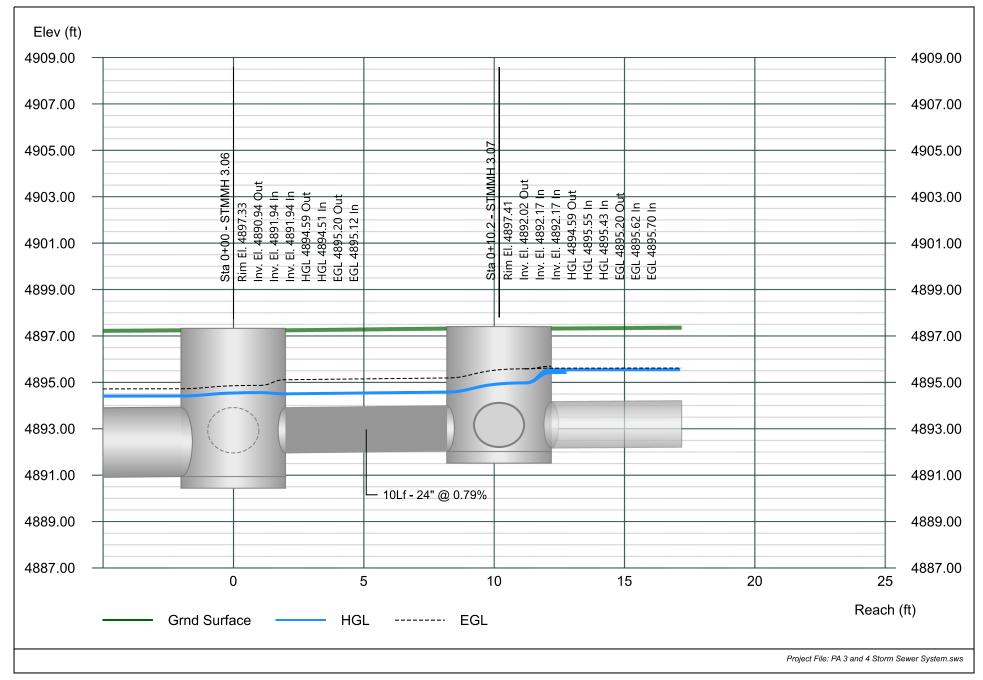
Line 11 - Pipe - (371) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



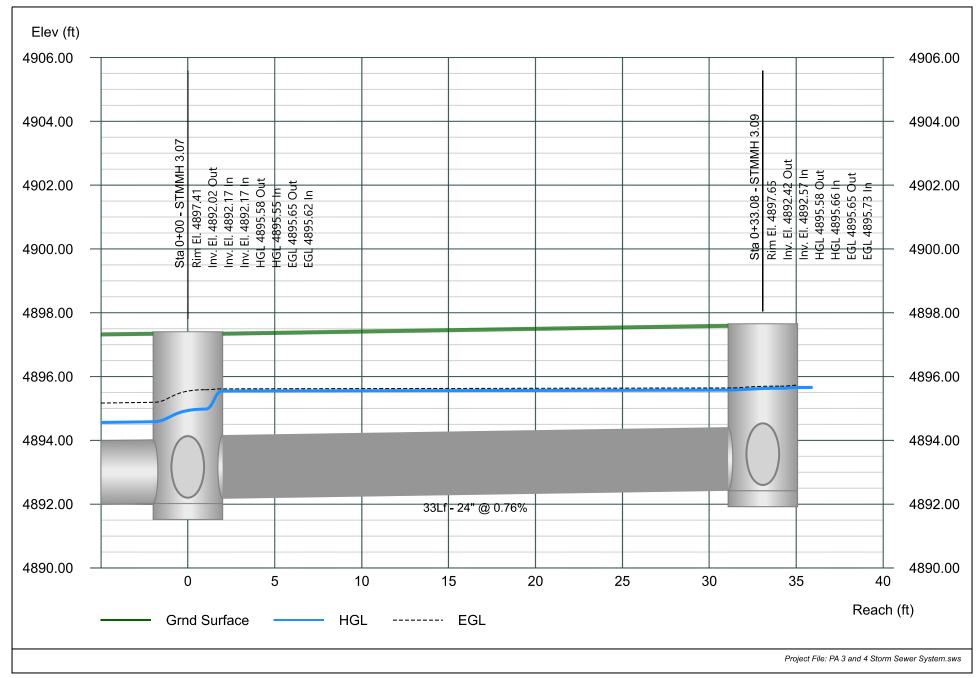
Line 12 - Pipe - (370) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



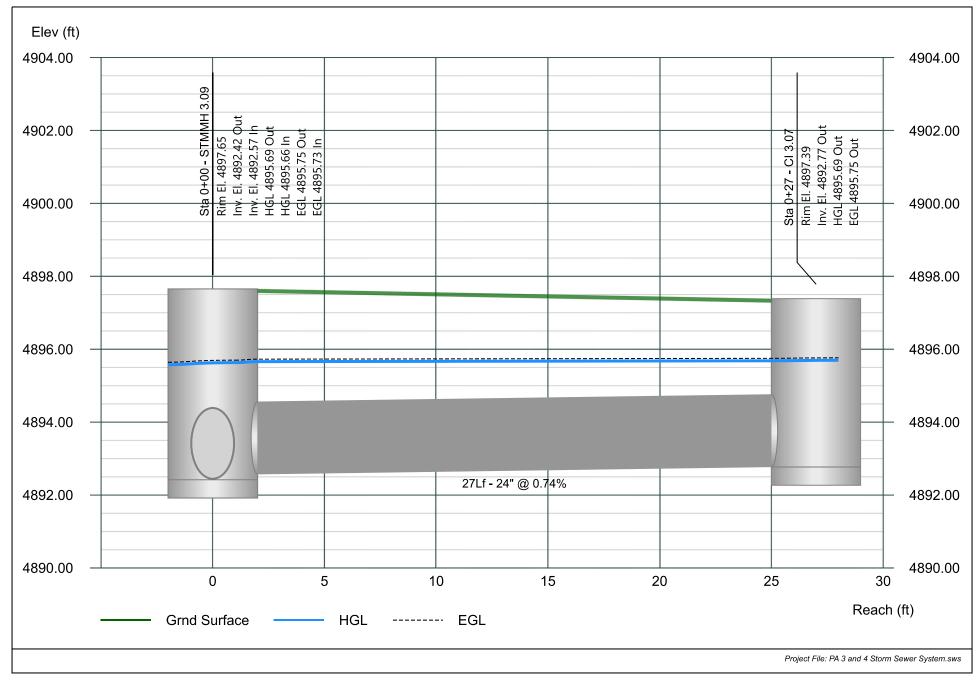
Line 13 - Pipe - (369) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

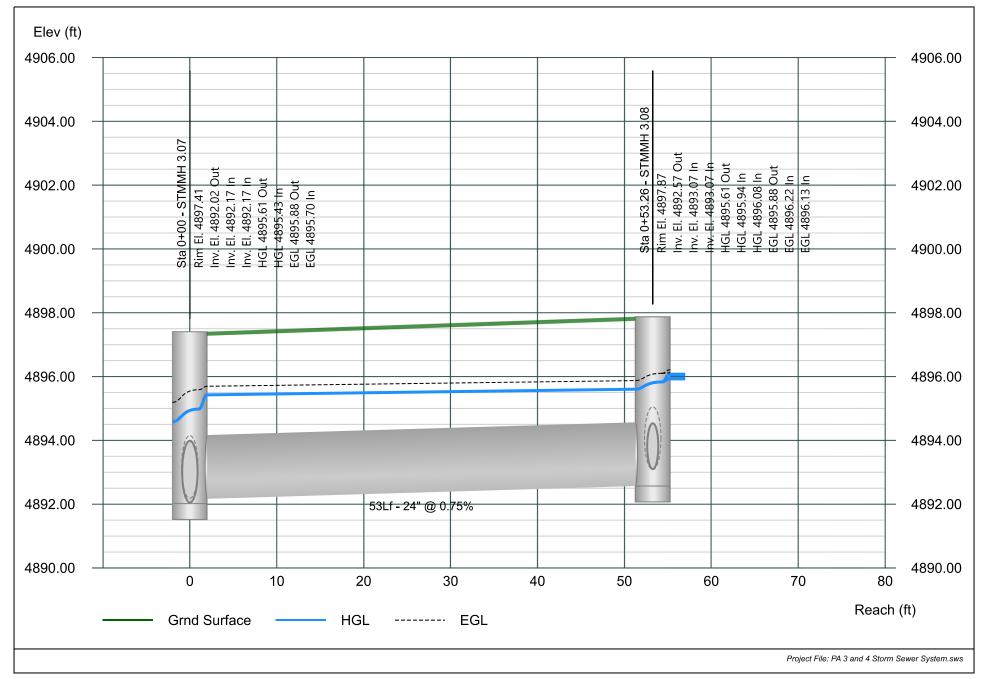


Line 14 - Pipe - (373) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

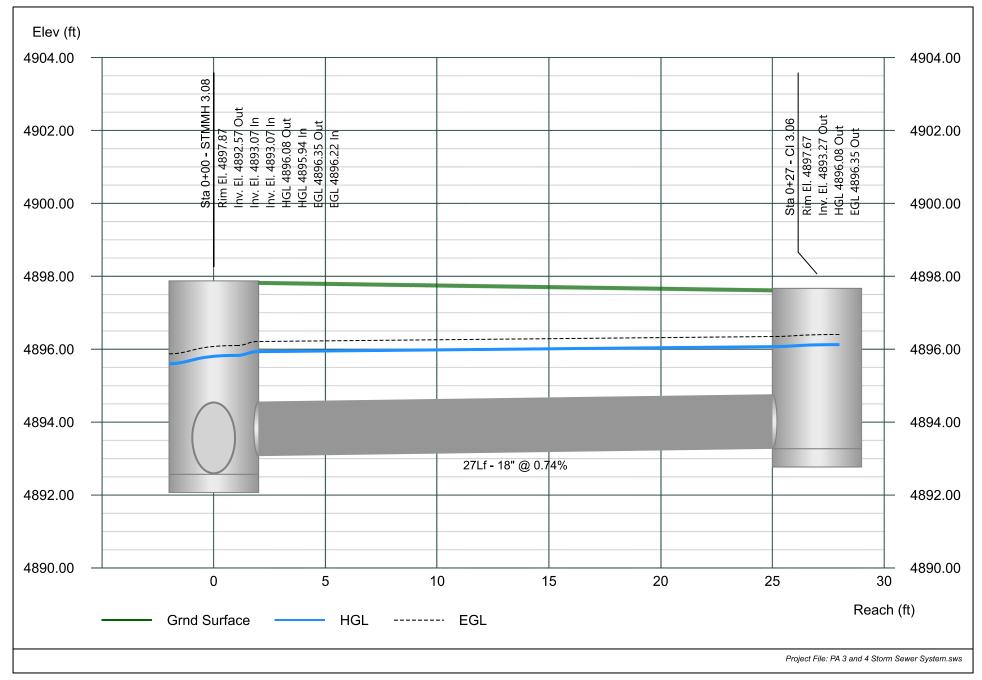


Line 15 - Pipe - (375) (PA 3 and 4 Storm Sewer Network)



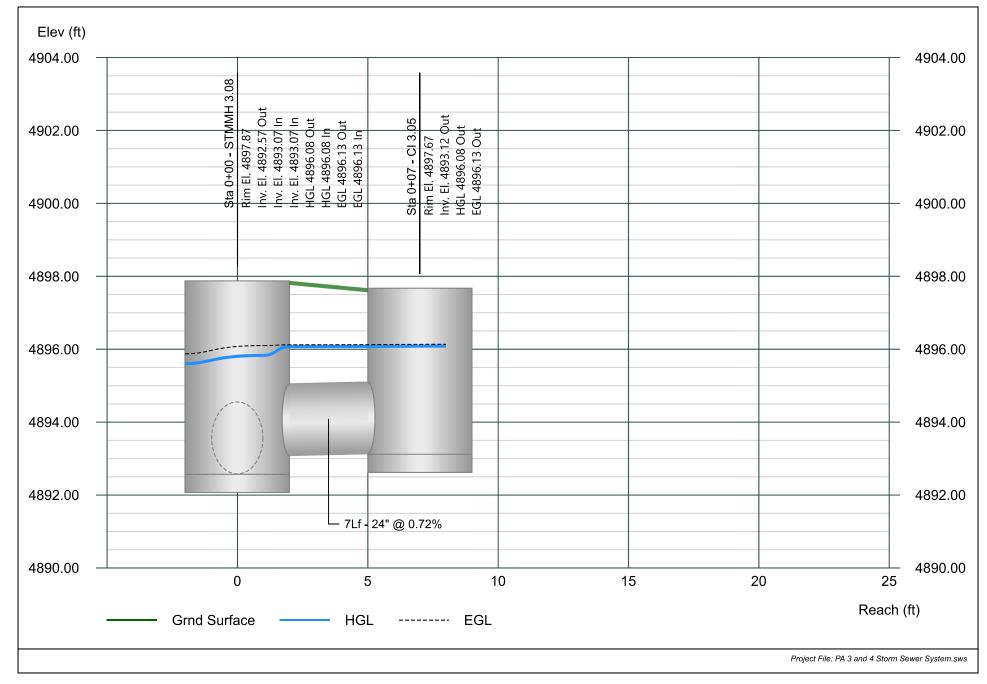
Line 16 - Pipe - (374) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



Line 17 - Pipe - (376) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



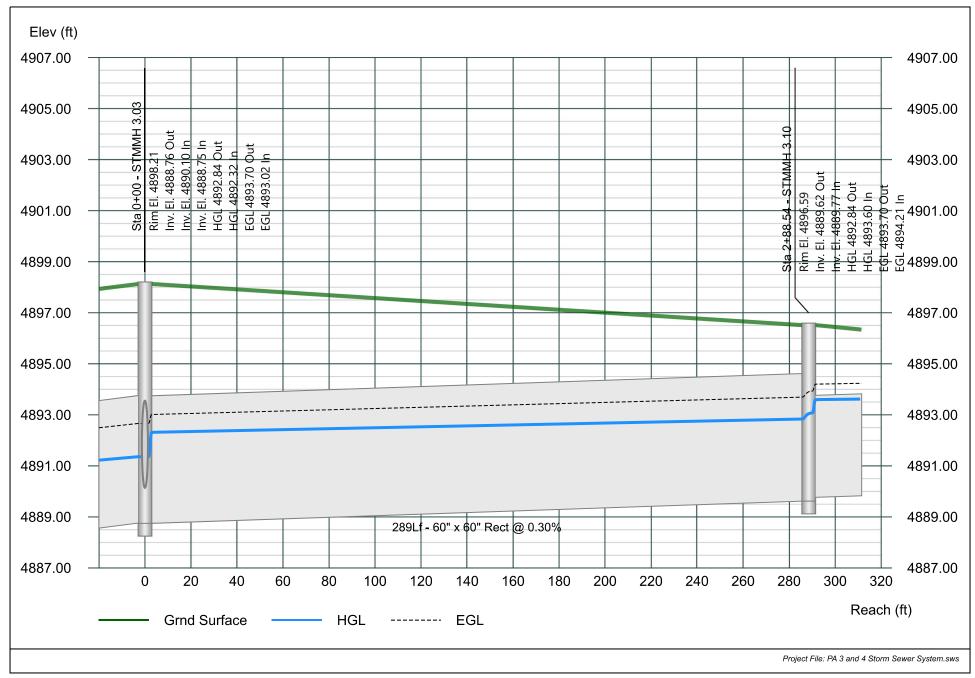
Line 18 - Pipe - (380) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

899.00		Sta 0+07 - Cl 3.04 Rim El. 4897.06 Inv. El. 4892.01 Out HGL 4894.76 Out EGL 4894.99 Out			4899.0
897.00					4897.0
895.00					4895.0
893.00					4893.0
801.00					4901
891.00		@ 1 00%			4891.0
		7Lf - 24"	- 7Lf - 24" @ 1.00%	- 7Lf - 24" @ 1.00%	- 7Lf - 24" @ 1.00%
	└── 7Lf - 24"	@ 1.00%			48
39.00					488

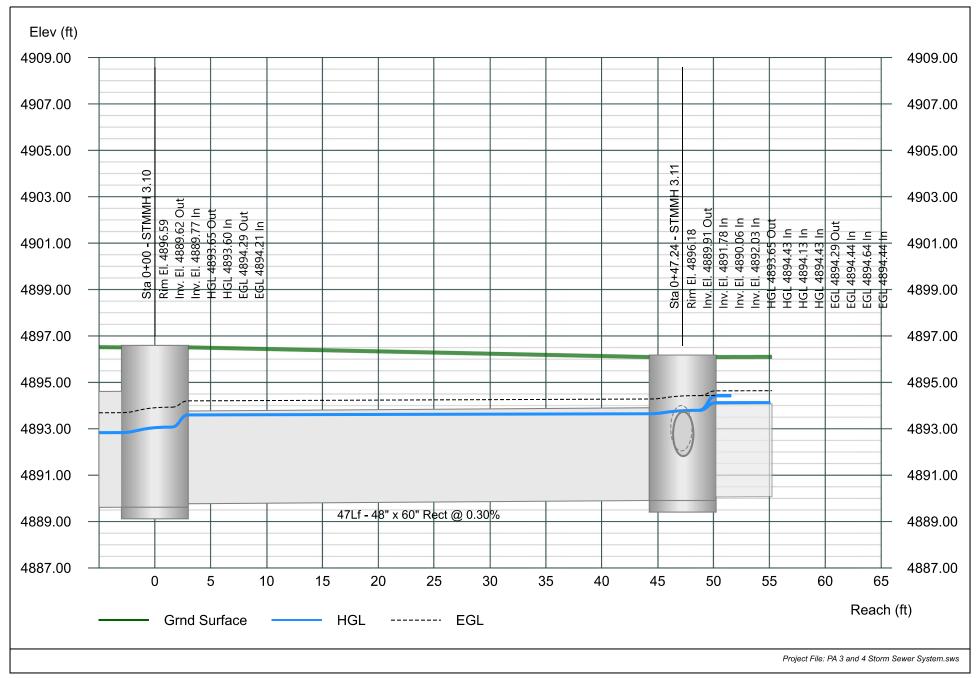
Line 19 - Pipe - (117) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

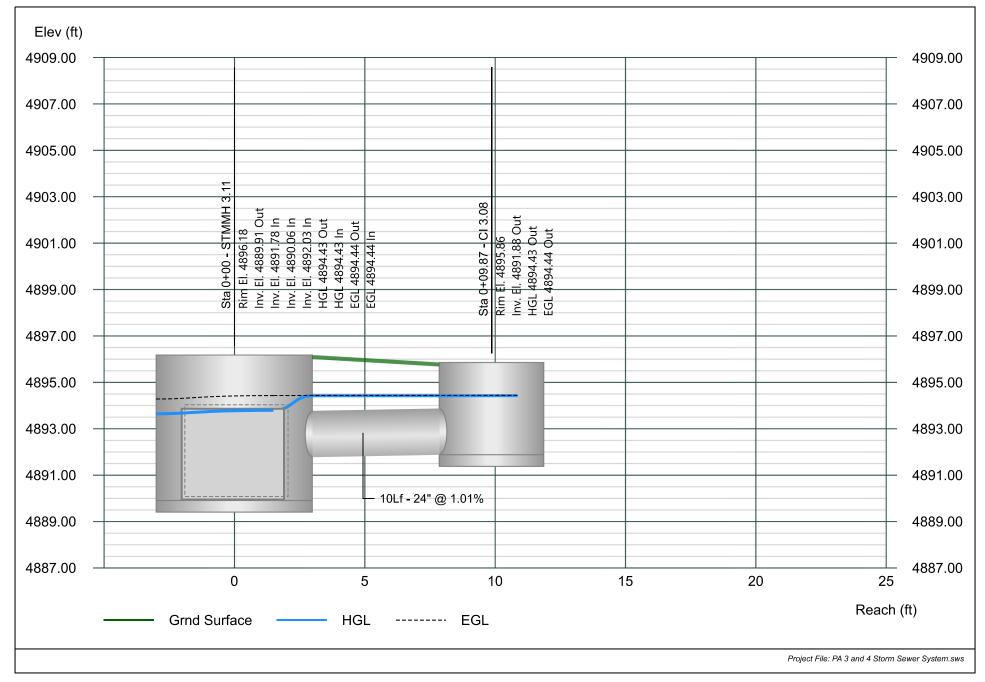


Line 20 - Pipe - (116) (1) (PA 3 and 4 Storm Sewer Network)

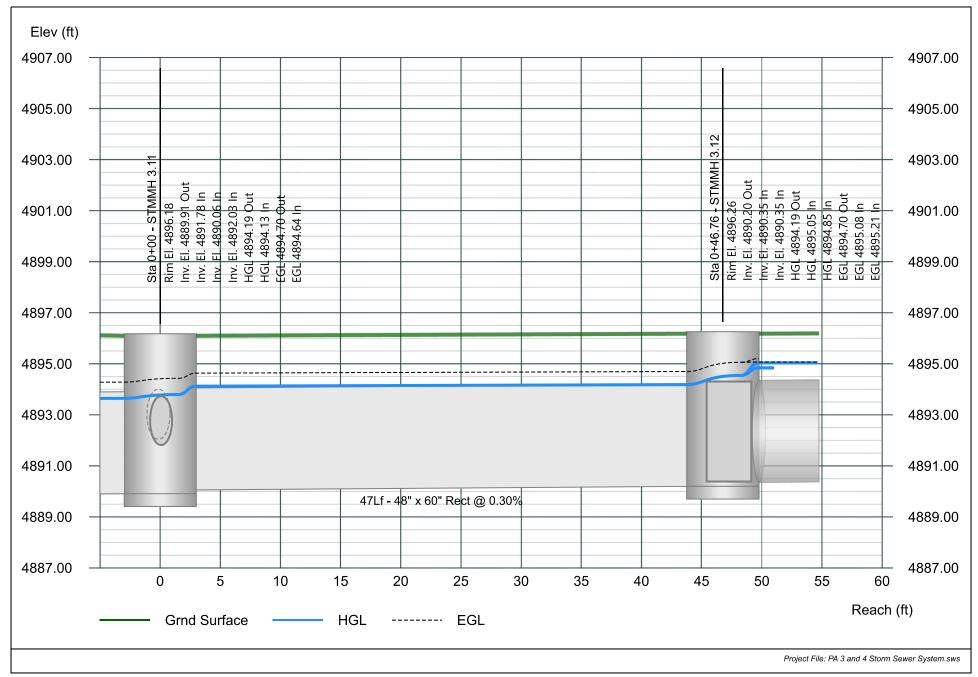
Stormwater Studio 2021 v 3.0.0.24



Line 21 - Pipe - (410) (PA 3 and 4 Storm Sewer Network)

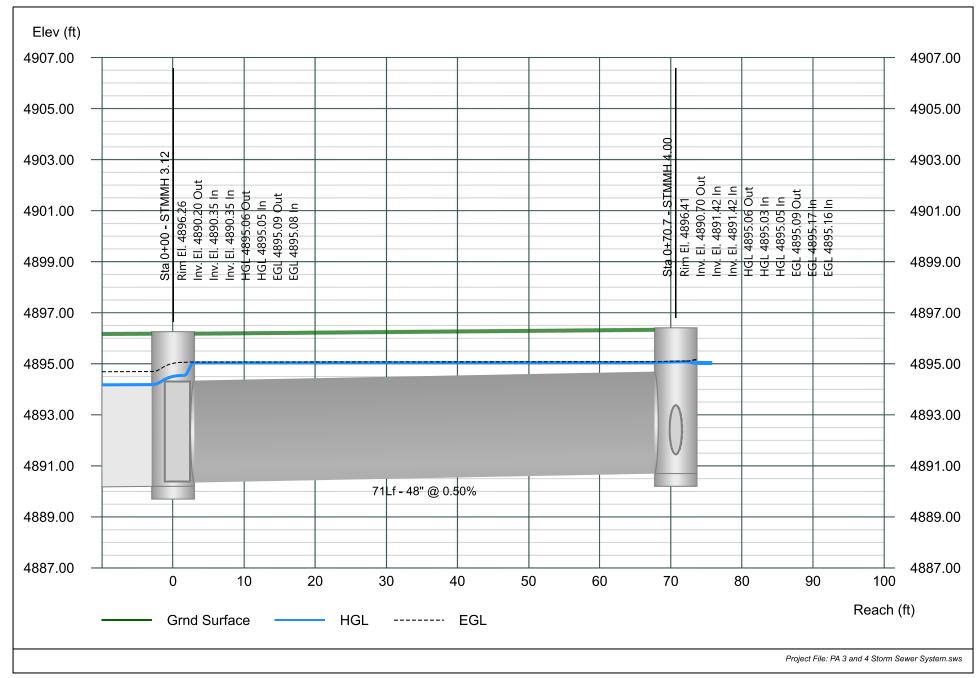


Line 22 - Pipe - (116) (PA 3 and 4 Storm Sewer Network)



Line 23 - Pipe - (413) (PA 3 and 4 Storm Sewer Network)

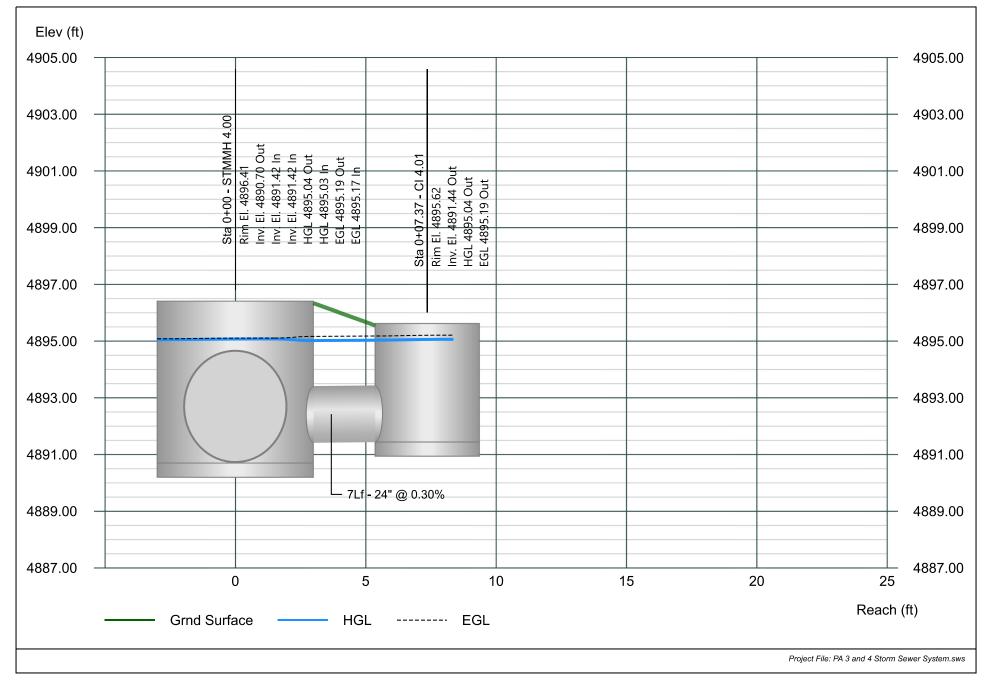
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village ~ PA 3 and 4

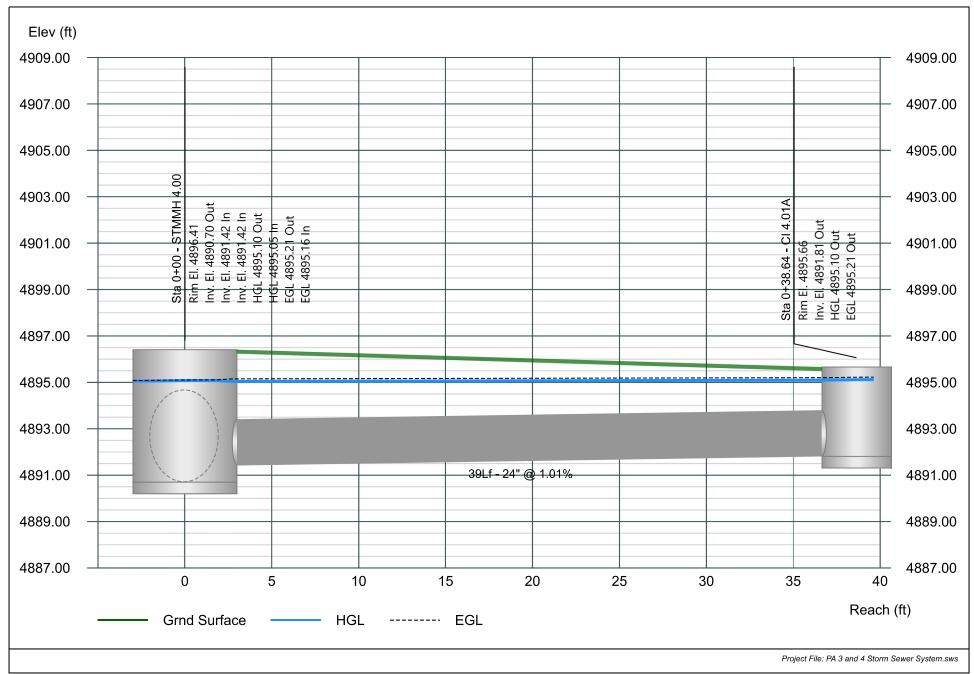
Line 24 - Pipe - (412) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



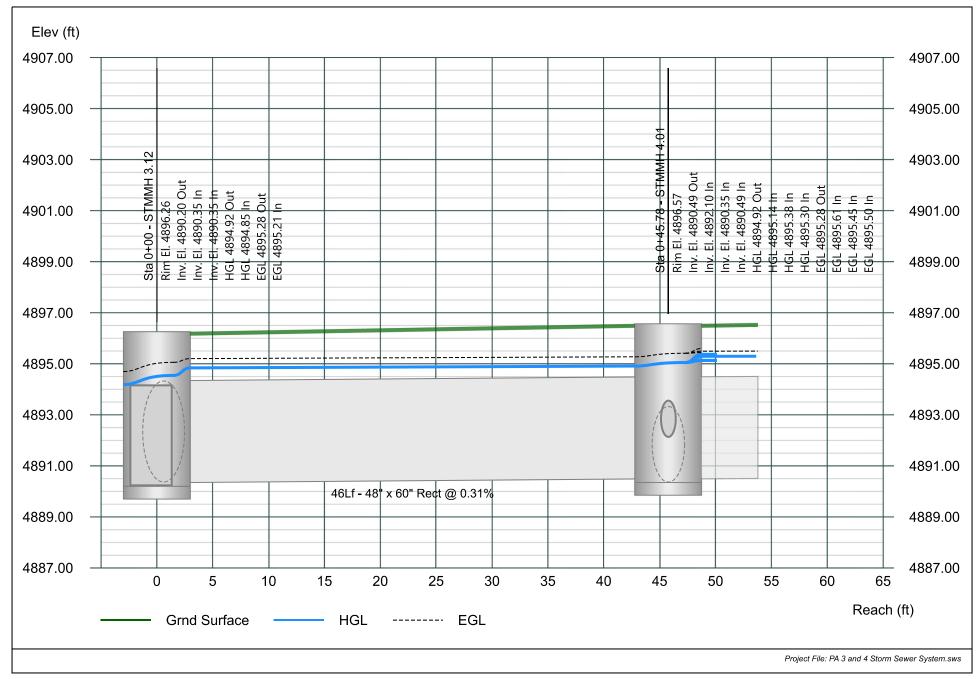
Line 25 - Pipe - (598) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



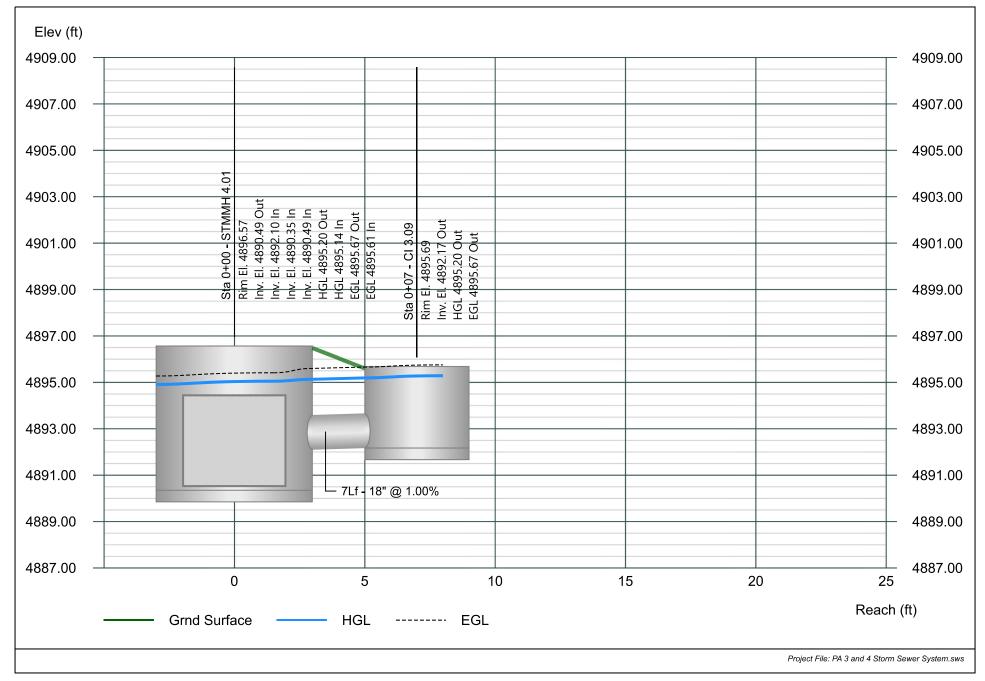
Line 26 - Pipe - (115) (1) (1) (1) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



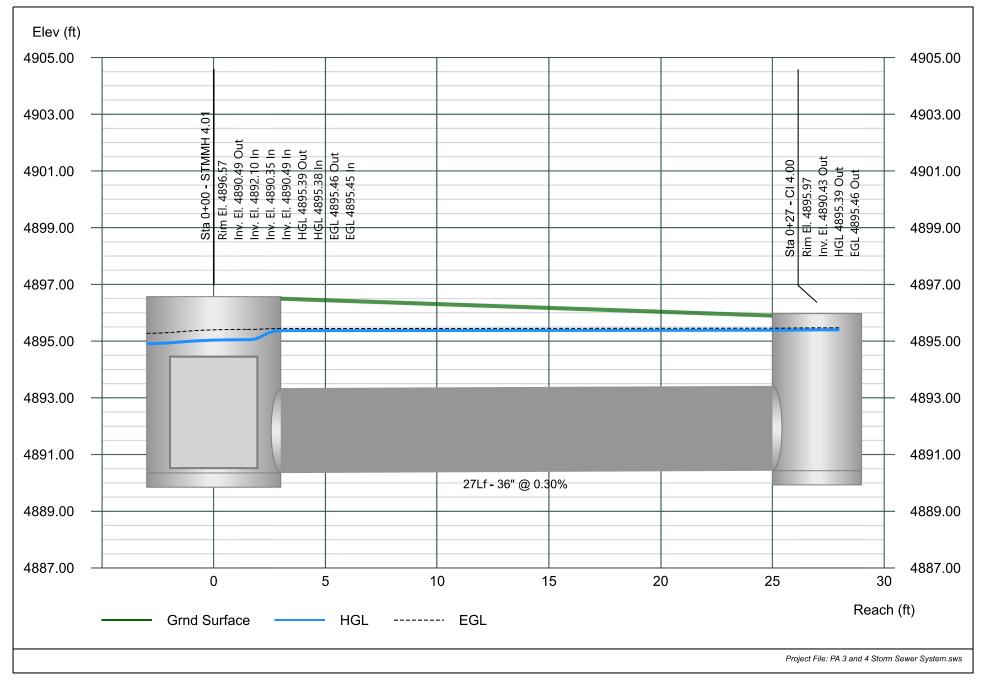
Line 27 - Pipe - (394) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24

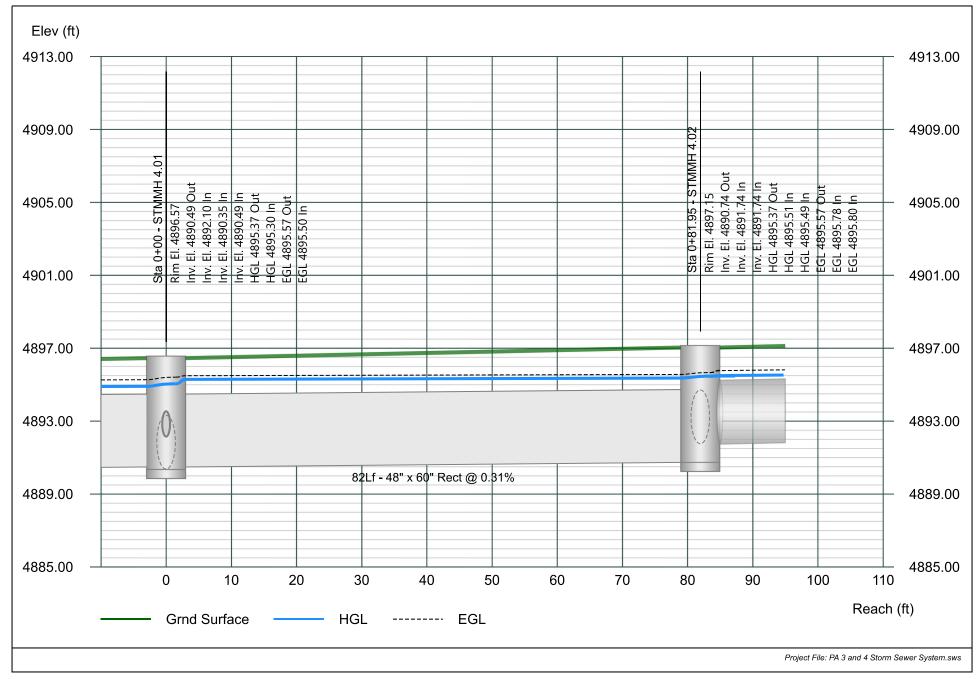


Line 28 - Pipe - (115) (1) (1) (PA 3 and 4 Storm Sewer Network)

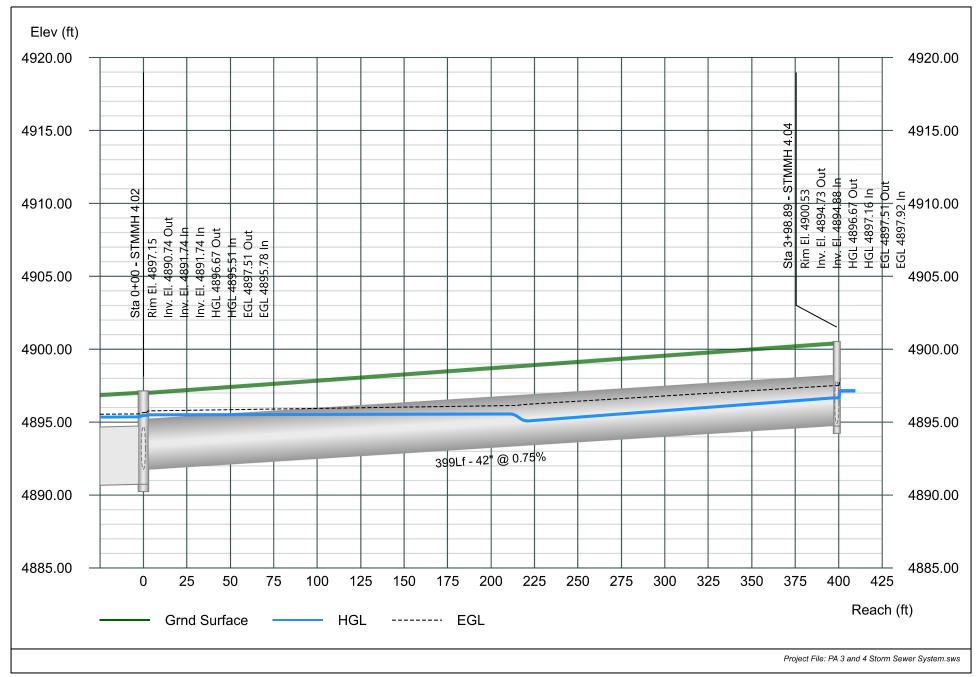
Stormwater Studio 2021 v 3.0.0.24



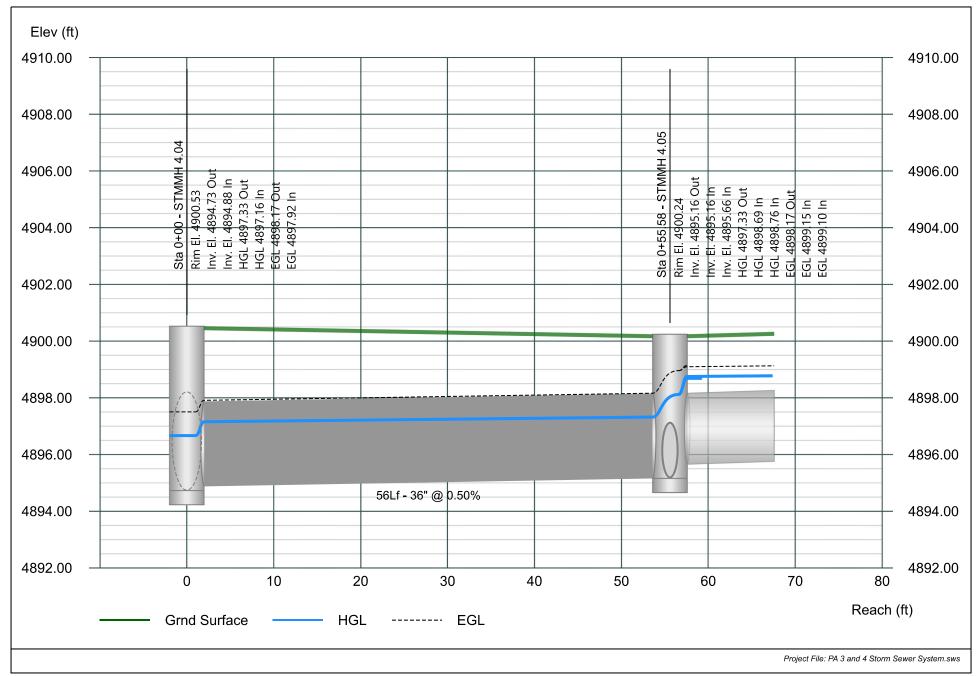
Line 29 - Pipe - (584) (1) (PA 3 and 4 Storm Sewer Network)



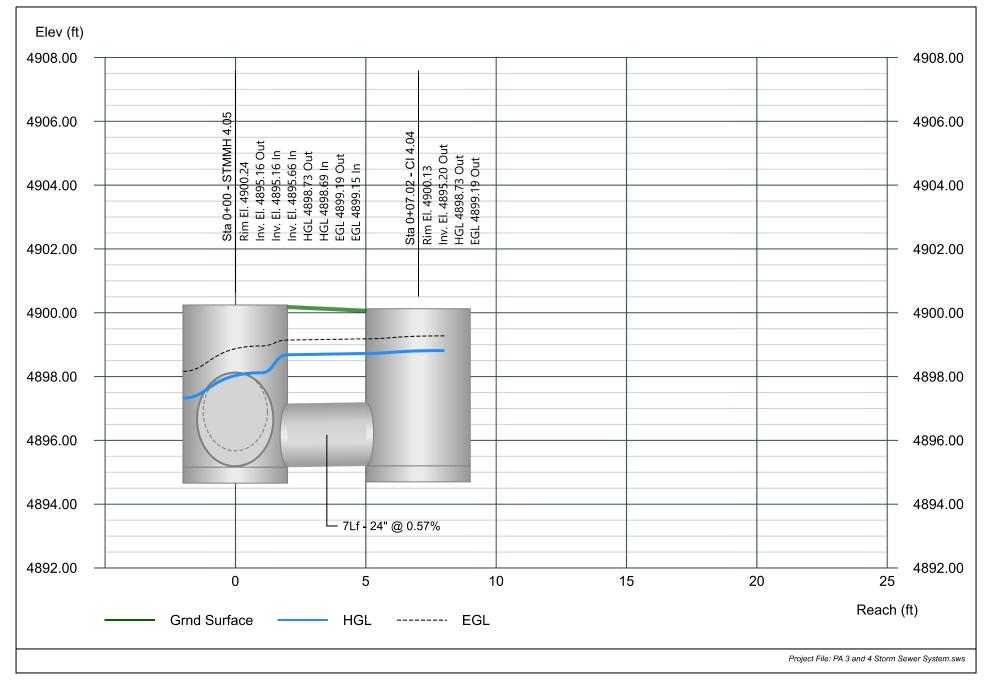
Line 30 - Pipe - (584) (PA 3 and 4 Storm Sewer Network)



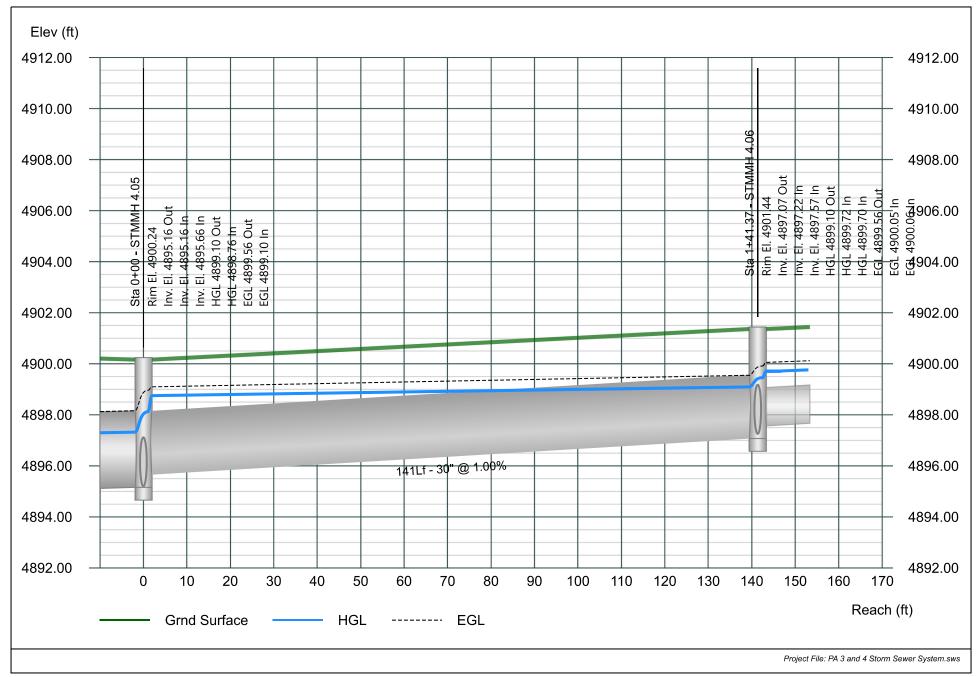
Line 31 - Pipe - (583) (PA 3 and 4 Storm Sewer Network)



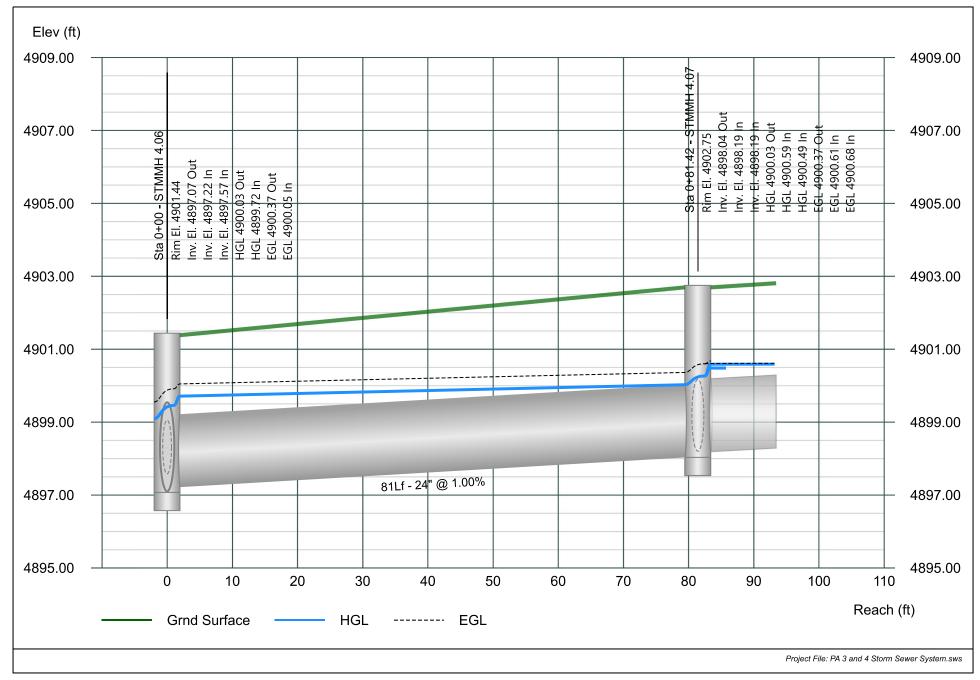
Line 32 - Pipe - (582) (PA 3 and 4 Storm Sewer Network)



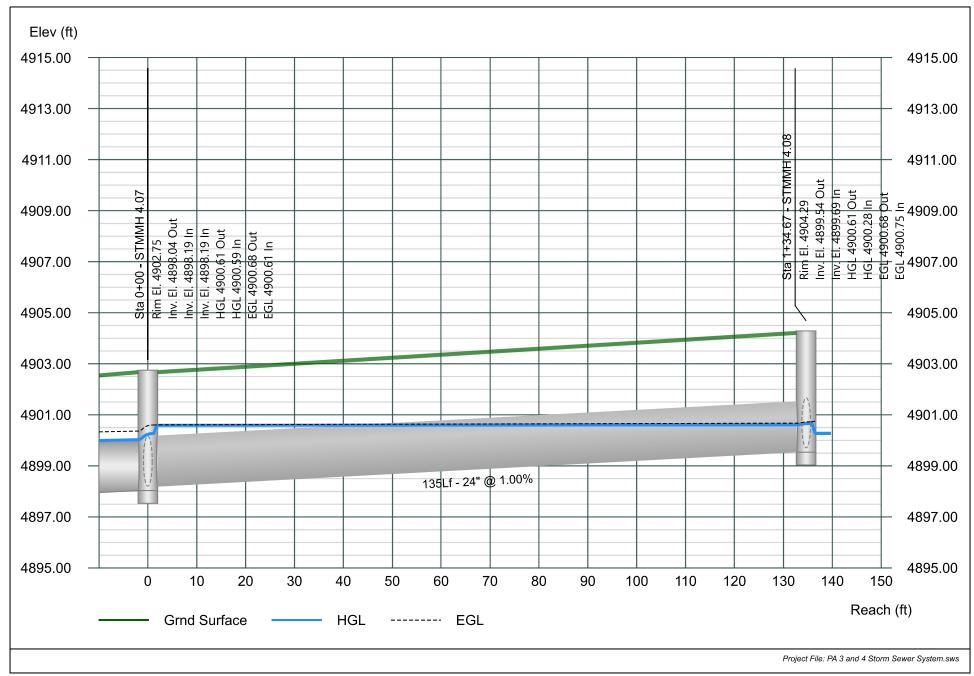
Line 33 - Pipe - (594) (PA 3 and 4 Storm Sewer Network)



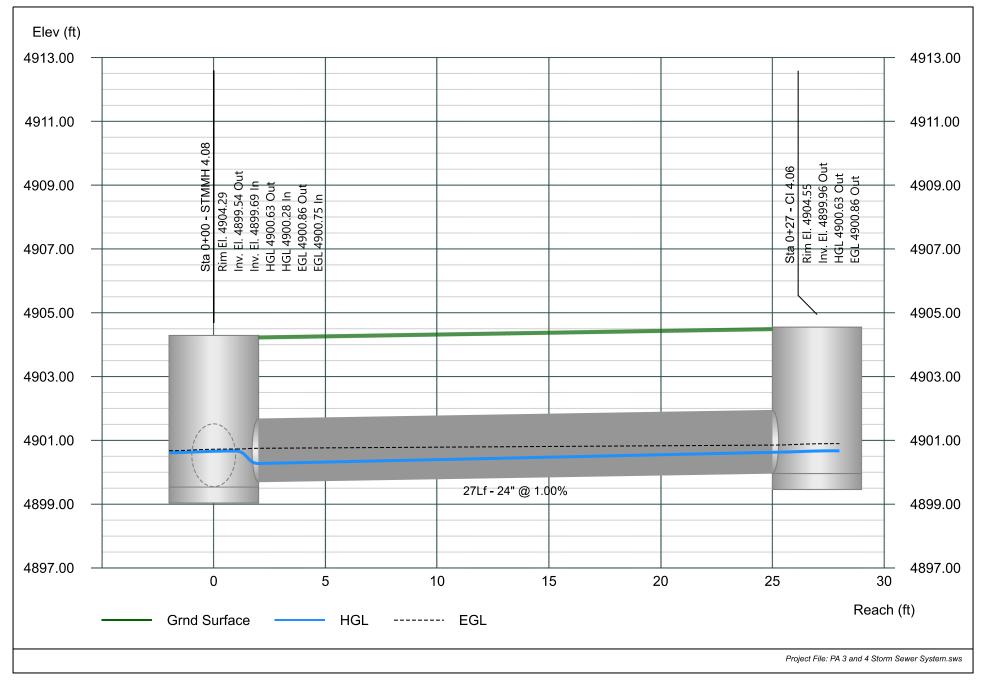
Line 34 - Pipe - (593) (PA 3 and 4 Storm Sewer Network)



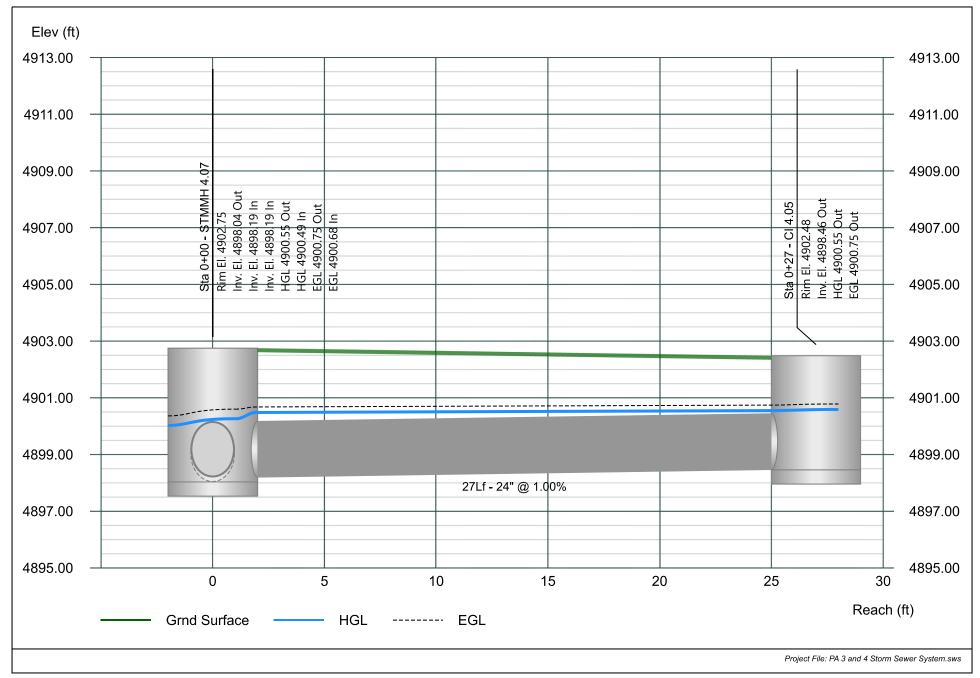
Line 35 - Pipe - (592) (PA 3 and 4 Storm Sewer Network)



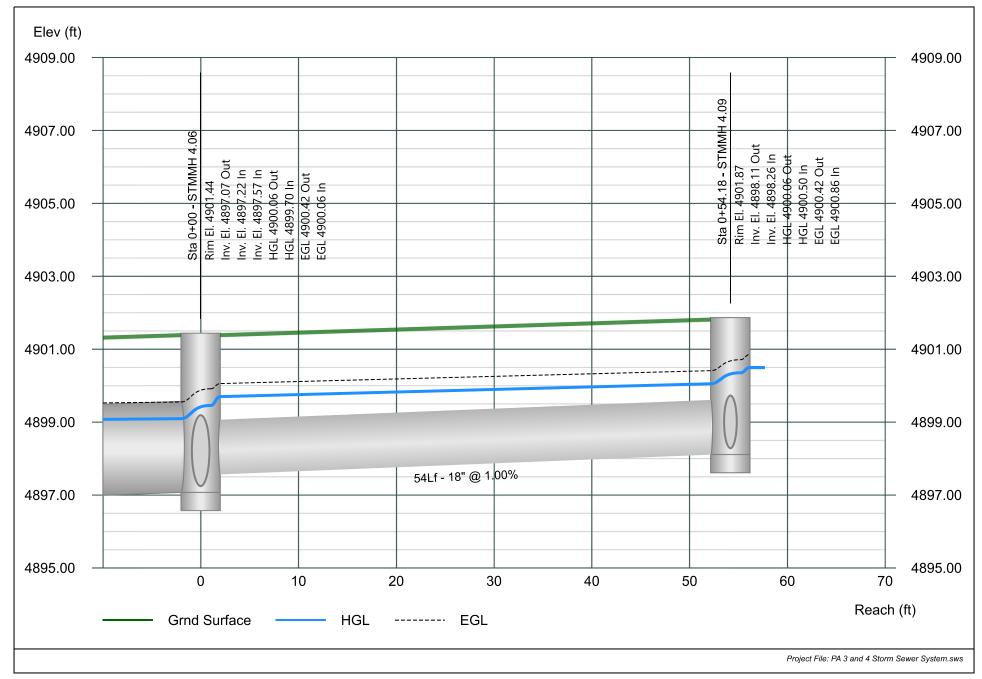
Line 36 - Pipe - (591) (PA 3 and 4 Storm Sewer Network)



Line 37 - Pipe - (595) (PA 3 and 4 Storm Sewer Network)

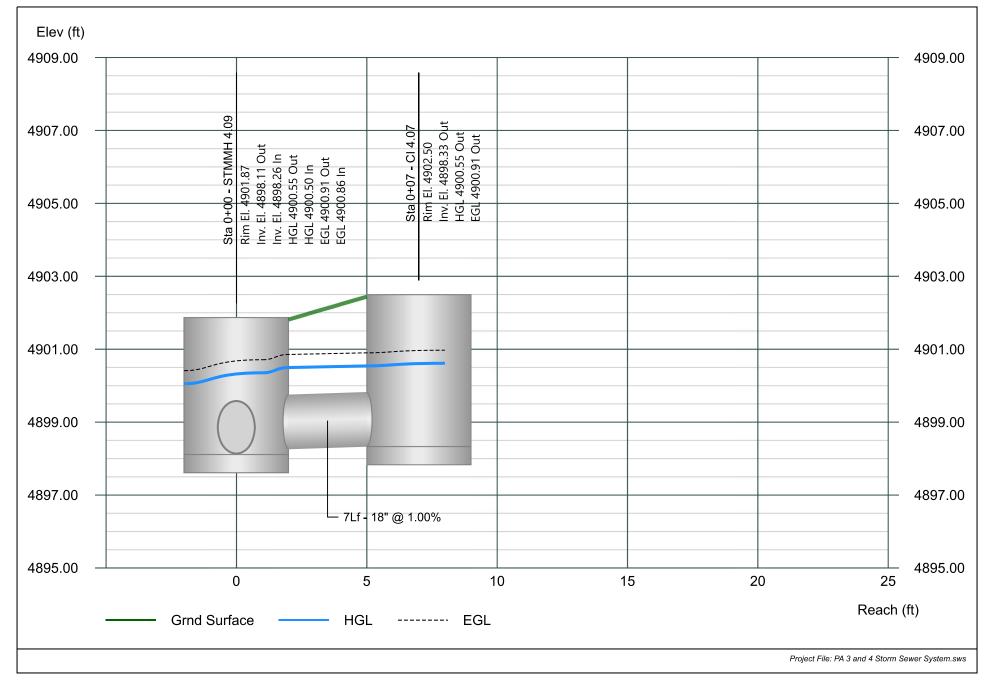


Line 38 - Pipe - (597) (PA 3 and 4 Storm Sewer Network)



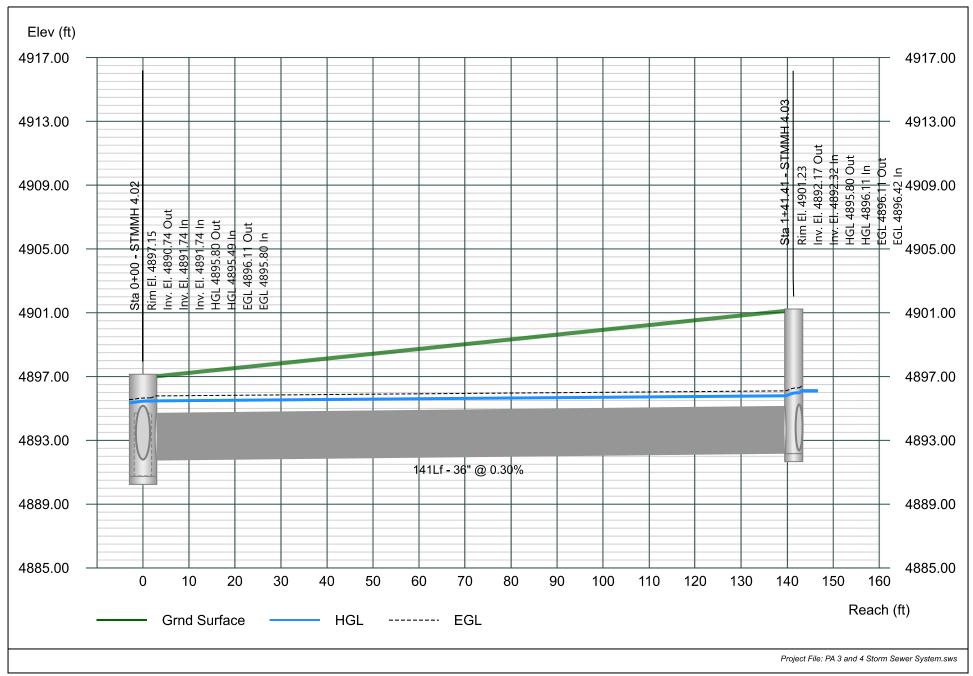
Line 39 - Pipe - (596) (PA 3 and 4 Storm Sewer Network)

Stormwater Studio 2021 v 3.0.0.24



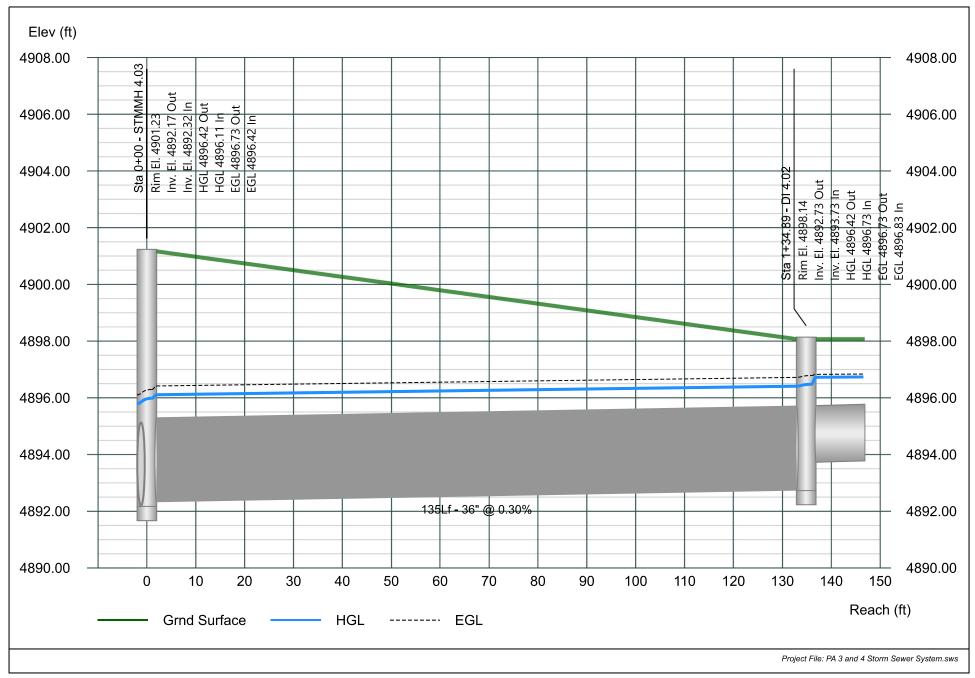
03-18-2021

Line 40 - Pipe - (585) (PA 3 and 4 Storm Sewer Network)



Line 41 - Pipe - (114) (1) (PA 3 and 4 Storm Sewer Network)

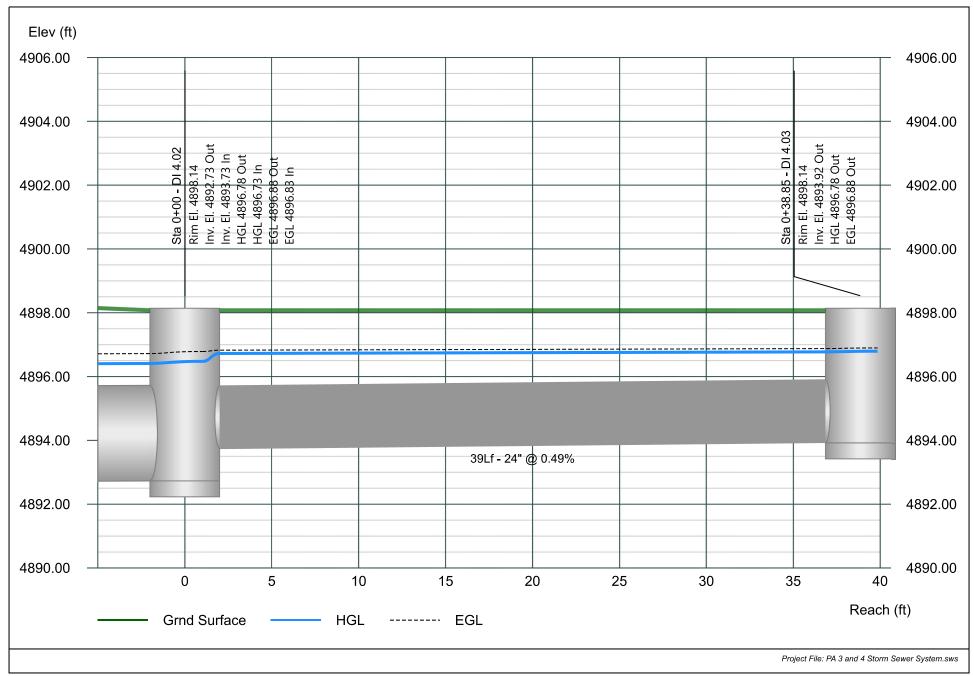
Stormwater Studio 2021 v 3.0.0.24



03-18-2021

Line 42 - Pipe - (114) (PA 3 and 4 Storm Sewer Network)

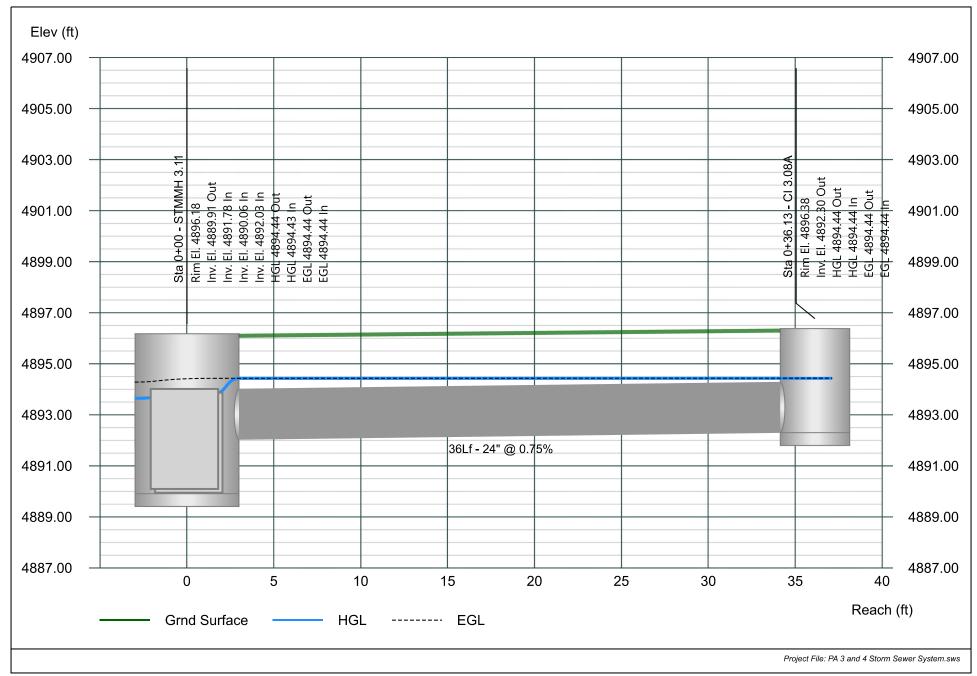
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village ~ PA 3 and 4

03-18-2021

Line 43 - Pipe - (600) (PA 3 and 4 Storm Sewer Network)



Energy Grade Line Calculations

Stormwater Studio 2021 v 3.0.0.24

Line	Line Size	Ø	Downstream							Length	Upstream								Pipe		Junction		
No			Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	Len	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	n Value	Enrgy Loss	HGLa Elev	EGLa Elev	Enrgy Loss	
	(in)	(cfs)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)		(ft)	(ft)	(ft)	(ft)	
1	60x84r	188.77	4873.43	5.00	35.00	4878.43	5.39	0.45	4878.88	104.16	4873.74	4.76	33.31	4878.50	5.67	0.50	4879.00	0.013	0.118	4878.84	4879.34	0.34	
2	60x84r	188.77	4873.74	5.00	35.00	4879.07	5.39	0.45	4879.52	933.32	4884.57	2.82²	19.77	4887.39	9.55	1.42	4888.81	0.013	9.288	4887.39	4888.81	0.00	
3	24	21.90	4885.26	2.00	3.14	4888.36	6.97	0.76	4889.11	50.37	4885.76	2.00	3.14	4888.83	6.97	0.76	4889.58	0.013	0.472	4889.46	4890.21	0.63	
4	24	7.96	4887.69	2.00	3.14	4890.16	2.53	0.10	4890.25	13.02	4887.82	2.00	3.14	4890.17	2.53	0.10	4890.27	0.013	0.016	4890.19	4890.29	0.02	
5	24	13.94	4887.69	2.00	3.14	4890.03	4.44	0.31	4890.34	32.98	4888.07	2.00	3.14	4890.16	4.44	0.31	4890.46	0.013	0.125	4890.22	4890.52	0.06	
6	60x84r	166.87	4884.57	3.94	27.61	4888.51	6.04	0.57	4889.08	361.47	4888.76	2.60²	18.21	4891.36	9.16	1.30	4892.67	0.013	3.585	4891.36	4892.67	0.00	
7	42	47.21	4890.10	2.49³	7.33	4892.59	6.44	0.65	4893.24	156.17	4890.57	2.49	7.33	4893.06	6.44	0.64	4893.71	0.013	0.470	4893.91	4894.56	0.85	
8	24	15.55	4891.57	2.00	3.14	4894.33	4.95	0.38	4894.71	20.78	4891.78	2.00	3.14	4894.43	4.95	0.38	4894.81	0.013	0.098	4894.74	4895.12	0.32	
9	18	8.78	4892.28	1.50	1.77	4894.89	4.97	0.38	4895.28	7.00	4892.33	1.50	1.77	4894.94	4.97	0.38	4895.33	0.013	0.049	4895.02	4895.40	0.08	
10	18	6.77	4892.28	1.50	1.77	4894.99	3.83	0.23	4895.22	27.00	4892.55	1.50	1.77	4895.10	3.83	0.23	4895.33	0.013	0.112	4895.15	4895.37	0.05	
11	36	31.66	4890.72	3.00	7.07	4894.37	4.48	0.31	4894.68	22.29	4890.94	3.00	7.07	4894.42	4.48	0.31	4894.73	0.013	0.050	4894.56	4894.88	0.15	
12	24	19.66	4891.94	2.00	3.14	4894.51	6.26	0.61	4895.12	10.20	4892.02	2.00	3.14	4894.59	6.26	0.61	4895.20	0.013	0.077	4894.98	4895.59	0.40	
13	24	6.56	4892.17	2.00	3.14	4895.55	2.09	0.07	4895.62	33.08	4892.42	2.00	3.14	4895.58	2.09	0.07	4895.65	0.013	0.028	4895.64	4895.70	0.06	
14	24	6.56	4892.57	2.00	3.14	4895.66	2.09	0.07	4895.73	27.00	4892.77	2.00	3.14	4895.69	2.09	0.07	4895.75	0.013	0.023	4895.70	4895.77	0.01	
15	24	13.10	4892.17	2.00	3.14	4895.43	4.17	0.27	4895.70	53.26	4892.57	2.00	3.14	4895.61	4.17	0.27	4895.88	0.013	0.179	4895.83	4896.11	0.23	
16	18	7.47	4893.07	1.50	1.77	4895.94	4.23	0.28	4896.22	27.00	4893.27	1.50	1.77	4896.08	4.23	0.28	4896.35	0.013	0.137	4896.13	4896.41	0.06	
17	24	5.63	4893.07	2.00	3.14	4896.08	1.79	0.05	4896.13	7.00	4893.12	2.00	3.14	4896.08	1.79	0.05	4896.13	0.013	0.004	4896.09	4896.14	0.01	
18	24	12.00	4891.94	2.00	3.14	4894.74	3.82	0.23	4894.97	7.00	4892.01	2.00	3.14	4894.76	3.82	0.23	4894.99	0.013	0.020	4894.81	4895.03	0.05	
19	60x60r	119.66	4888.75	3.57	17.84	4892.32	6.71	0.70	4893.02	288.54	4889.62	3.22	16.10	4892.84	7.43	0.86	4893.70	0.013	0.681	4893.08	4893.94	0.24	
20	48x60r	119.66	4889.77	3.83	19.16	4893.60	6.25	0.61	4894.21	47.24	4889.91	3.74	18.71	4893.65	6.40	0.64	4894.29	0.013	0.080	4893.80	4894.44	0.15	
21	24	2.89	4891.78	2.00	3.14	4894.43	0.92	0.01	4894.44	9.87	4891.88	2.00	3.14	4894.43	0.92	0.04	4894.44	0.010	0.000	4894.43	4894.45	0.00	
22	48x60r	114.64	4890.06	4.00	20.00	4894.13	5.73	0.51	4894.64	46.76	4890.20	3.99	19.95	4894.19	5.75	0.51	4894.70	0.013	0.063	4894.55	4895.06	0.36	
22	407001	114.04	+030.00	4.00	20.00	-034.13	5.15	0.01	-034.04	40.70	4030.20	5.55	19.95	-034.19	5.75	0.01	-034.70	0.013	0.003	-034.33	+035.00	0.50	
	Datum Du i	- 102			3 1	- 1 - 1 - 1 - 41-					-										<u> </u>		
inotes:	Return Perio	a = 100-j	yrs. ² Critic	cal depth	i. [°] Norm	iai depth.	r = recta	angular	e = elliptica	i a = arc	n								Project File	e: PA 3 and 4	Storm Sewer	System.sws	

03-18-2021

Energy Grade Line Calculations

Stormwater Studio 2021 v 3.0.0.24

Line	Line	Q (cfs)	Downstream							Length	Upstream								ре	Junction		
No	Size (in)		Invert Elev (ft)	Depth (ft)	Area (sqft)	HGL Elev (ft)	Vel (ft/s)	Vel Head (ft)	EGL Elev (ft)	Le L (ft)	Invert Elev (ft)	Depth (ft)	Area (sqft)	HGL Elev (ft)	Vel (ft/s)	Vel Head (ft)	EGL Elev (ft)	n Value	Enrgy Loss (ft)	HGLa Elev (ft)	EGLa Elev (ft)	Enrgy Loss (ft)
23	48	(CIS) 17.90	4890.35	4.00	(Sqlt)	4895.05	1.42	0.03	4895.08	70.70	4890.70	4.00	(Sqit) 12.57	4895.06	1.42	0.03	4895.09	0.013	0.011	4895.08	4895.11	0.03
24	24	9.66	4891.42	2.00	3.14	4895.03	3.08	0.15	4895.17	7.37	4891.44	2.00	3.14	4895.04	3.07	0.15	4895.19	0.013	0.014	4895.07	4895.22	0.03
25	24	8.24	4891.42	2.00	3.14	4895.05	2.62	0.11	4895.16	38.64	4891.81	2.00	3.14	4895.10	2.62	0.11	4895.21	0.013	0.051	4895.12	4895.23	0.02
26	48x60r	96.74	4890.35	4.00	20.00	4894.85	4.84	0.36	4895.21	45.78	4890.49	4.00	20.00	4894.92	4.84	0.36	4895.28	0.013	0.071	4895.06	4895.42	0.14
27	18	9.70	4892.10	1.50	1.77	4895.14	5.49	0.47	4895.61	7.00	4892.17	1.50	1.77	4895.20	5.49	0.47	4895.67	0.013	0.060	4895.29	4895.76	0.09
28	36	15.27	4890.35	3.00	7.07	4895.38	2.16	0.07	4895.45	27.00	4890.43	3.00	7.07	4895.39	2.16	0.07	4895.46	0.013	0.014	4895.40	4895.48	0.01
29	48x60r	71.77	4890.49	4.00	20.00	4895.30	3.59	0.20	4895.50	81.95	4890.74	4.00	20.00	4895.37	3.59	0.20	4895.57	0.013	0.070	4895.47	4895.67	0.10
30	42	40.21	4891.74	3.50	9.62	4895.51	4.18	0.27	4895.78	398.89	4894.73	1.94²	5.48	4896.67	7.34	0.84	4897.51	0.013	1.729	4896.67	4897.51	0.00
31	36	40.21	4894.88	2.28	5.76	4897.16	6.98	0.76	4897.92	55.58	4895.16	2.17	5.46	4897.33	7.36	0.84	4898.17	0.013	0.251	4898.12	4898.96	0.80
32	24	17.10	4895.16	2.00	3.14	4898.69	5.44	0.46	4899.15	7.02	4895.20	2.00	3.14	4898.73	5.44	0.46	4899.19	0.013	0.040	4898.82	4899.28	0.09
33	30	23.11	4895.66	2.50	4.91	4898.76	4.71	0.34	4899.10	141.37	4897.07	2.03	4.26	4899.10	5.42	0.46	4899.56	0.013	0.455	4899.46	4899.92	0.36
34	24	14.62	4897.22	2.00	3.14	4899.72	4.65	0.34	4900.05	81.42	4898.04	2.00	3.14	4900.03	4.65	0.34	4900.37	0.013	0.314	4900.27	4900.61	0.24
35	24	3.51	4898.19	2.00	3.14	4900.59	1.12	0.02	4900.61	134.67	4899.54	1.08	1.72	4900.61	2.04	0.06	4900.68	0.013	0.065	4900.67	4900.73	0.05
36	24	3.51	4899.69	0.59‡	0.77	4900.28	4.57	0.32	4900.75	27.00	4899.96	0.67	0.92	4900.63	3.82	0.23	4900.86	0.013	0.101	4900.67	4900.90	0.05
37	24	11.11	4898.19	2.00	3.14	4900.49	3.54	0.19	4900.68	27.00	4898.46	2.00	3.14	4900.55	3.54	0.19	4900.75	0.013	0.065	4900.59	4900.79	0.04
38	18	8.49	4897.57	1.50	1.77	4899.70	4.81	0.36	4900.06	54.18	4898.11	1.50	1.77	4900.06	4.80	0.36	4900.42	0.013	0.354	4900.36	4900.72	0.30
39	18	8.49	4898.26	1.50	1.77	4900.50	4.81	0.36	4900.86	7.00	4898.33	1.50	1.77	4900.55	4.80	0.36	4900.91	0.013	0.046	4900.62	4900.98	0.07
40	36	31.56	4891.74	3.00	7.07	4895.49	4.47	0.31	4895.80	141.41	4892.17	3.00	7.07	4895.80	4.46	0.31	4896.11	0.013	0.317	4895.99	4896.30	0.19
41	36	31.56	4892.32	3.00	7.07	4896.11	4.47	0.31	4896.42	134.89	4892.73	3.00	7.07	4896.42	4.46	0.31	4896.73	0.013	0.302	4896.48	4896.79	0.07
42	24	8.09	4893.73	2.00	3.14	4896.73	2.58	0.10	4896.83	38.85	4893.92	2.00	3.14	4896.78	2.58	0.10	4896.88	0.013	0.050	4896.80	4896.90	0.02
43	24	2.13	4892.03	2.00	3.14	4894.43	0.68	0.01	4894.44	36.13	4892.30	2.00	3.14	4894.44	0.68	0.01	4894.44	0.013	0.003	4894.44	4894.44	0.00

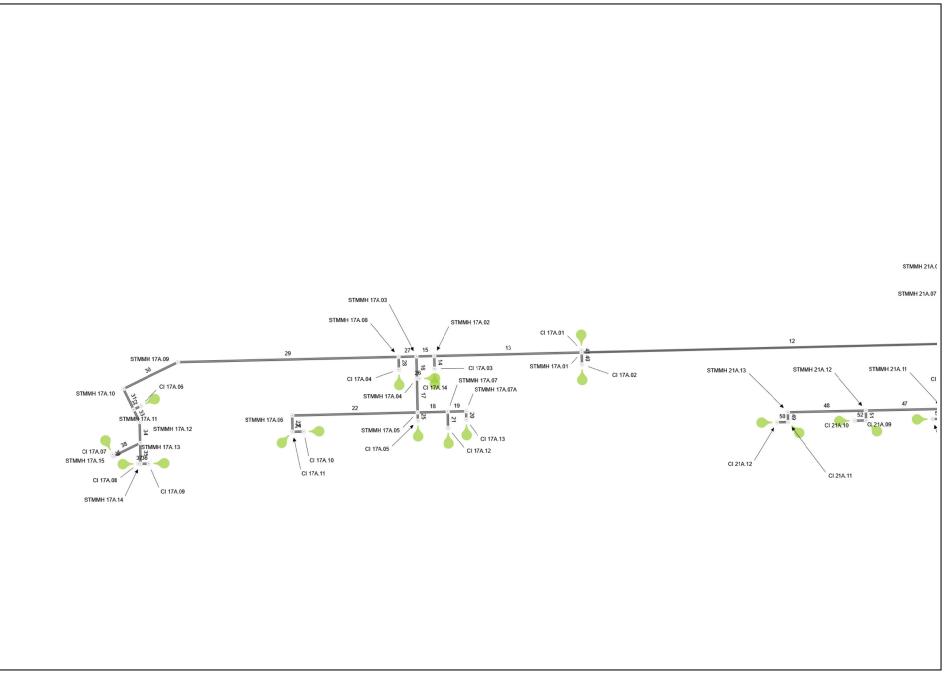
Notes: Return Period = 100-yrs. ² Critical depth. [‡] Supercritical. r = rectangular e = elliptical a = arch

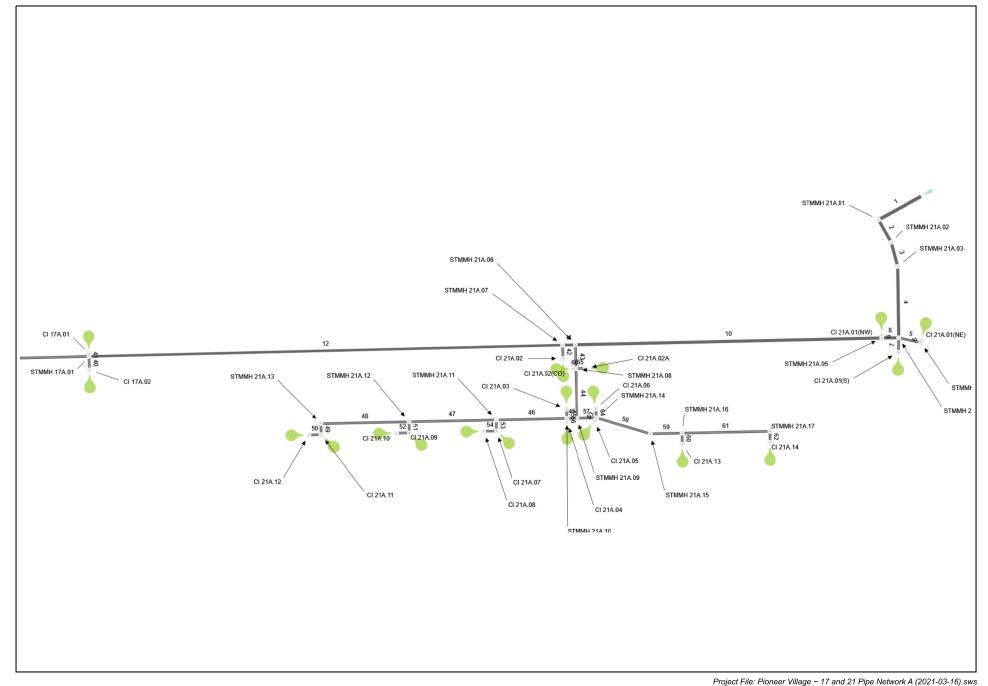
Project File: PA 3 and 4 Storm Sewer System.sws

Project Name: Pioneer Village ~ PA 3 and 4

03-18-2021

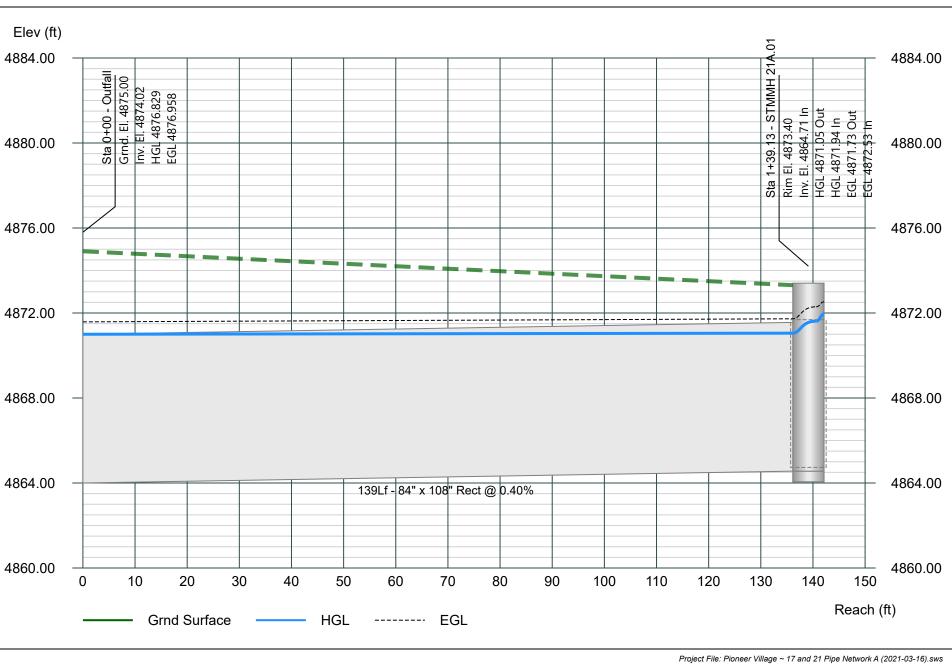
04-09-2021





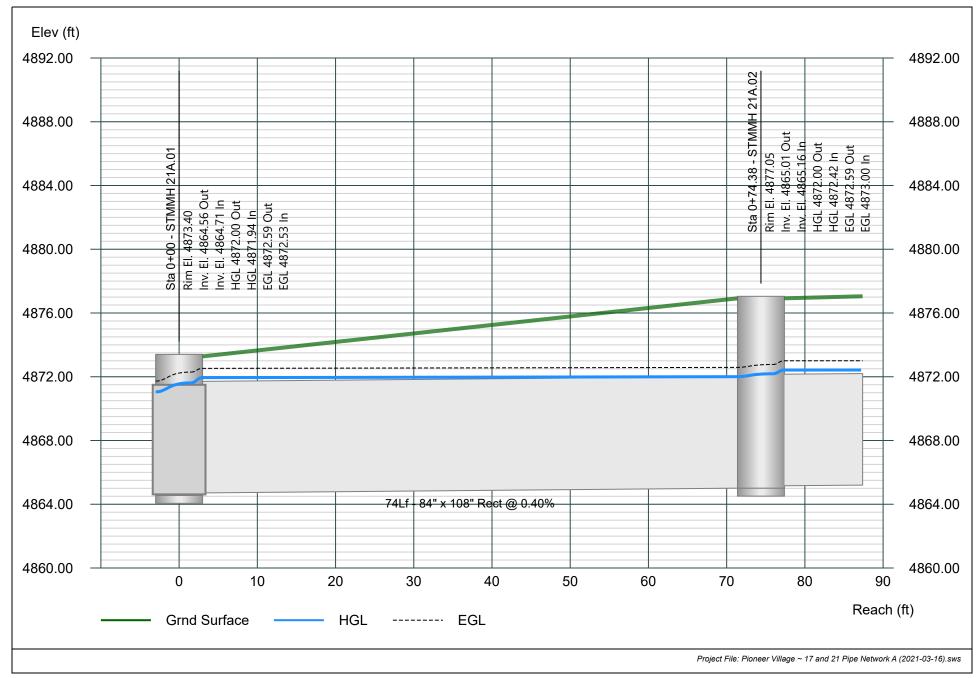
Line 1 - Pipe - (136) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



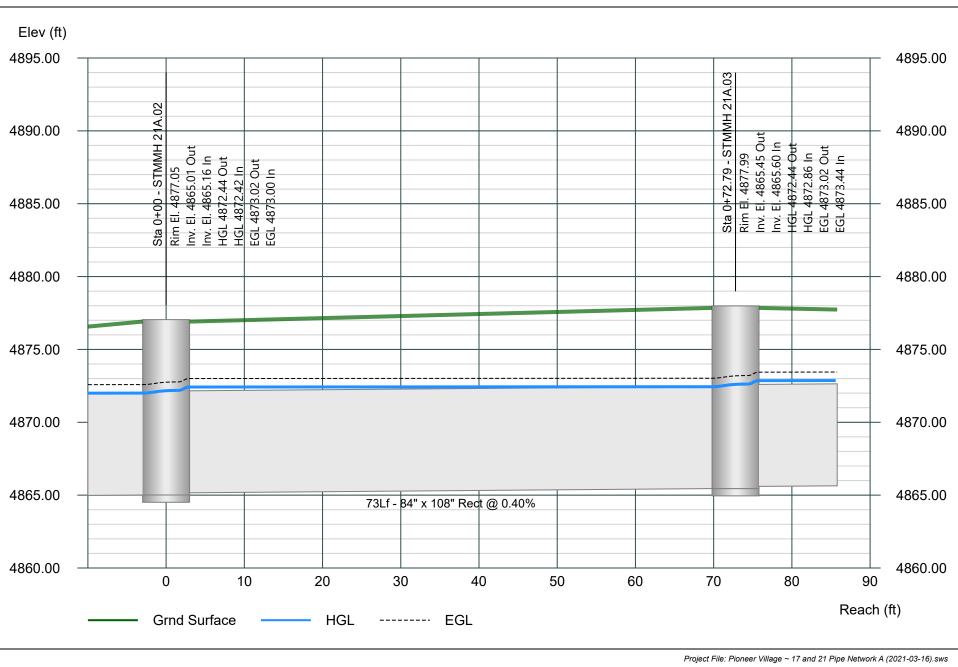
Line 2 - Pipe - (135) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



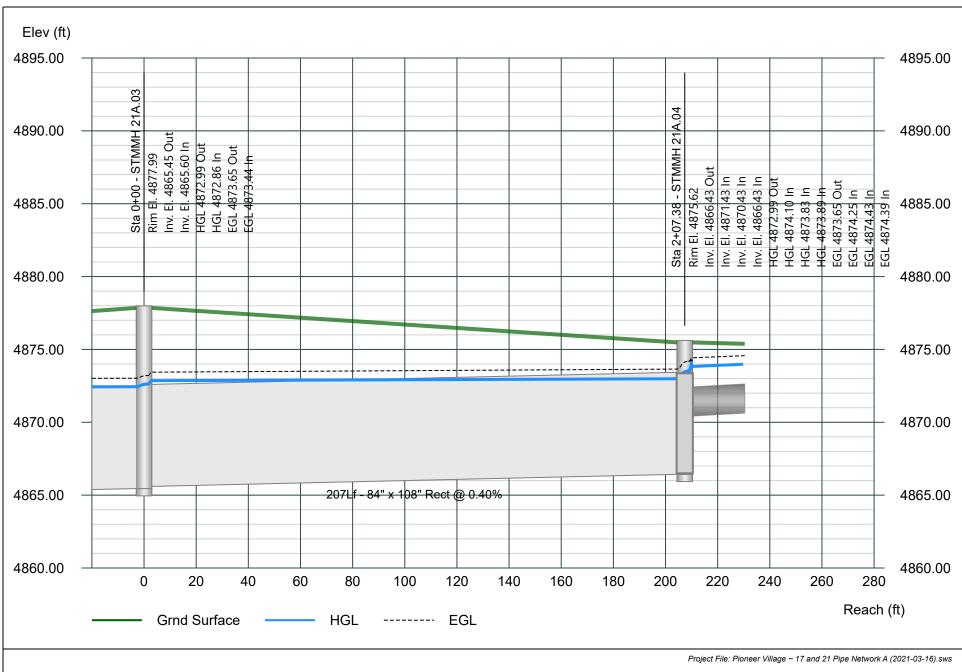
Line 3 - Pipe - (134) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



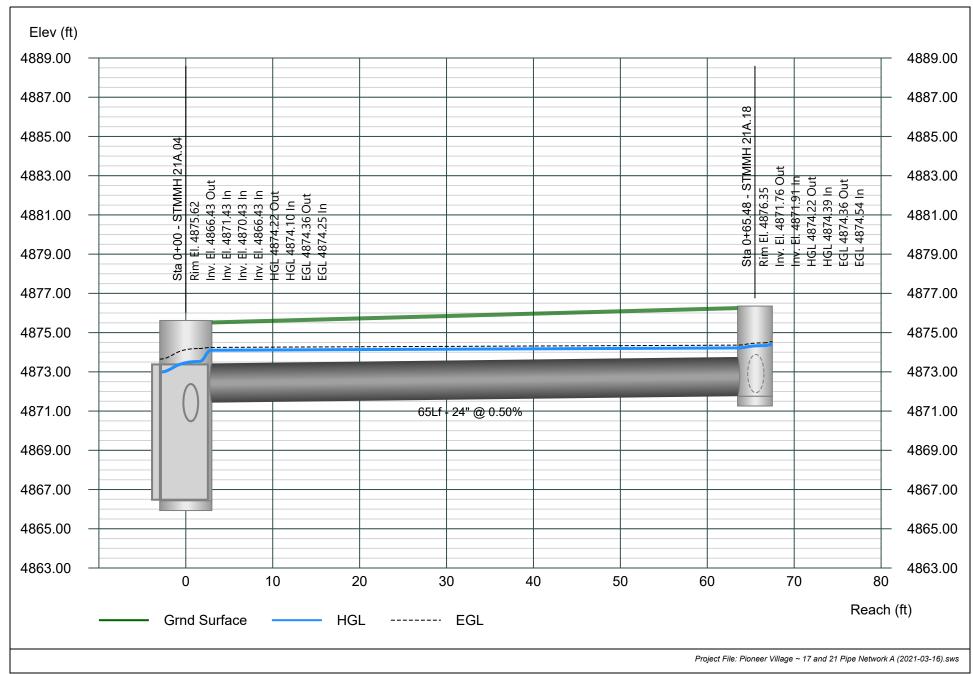
Line 4 - Pipe - (133) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



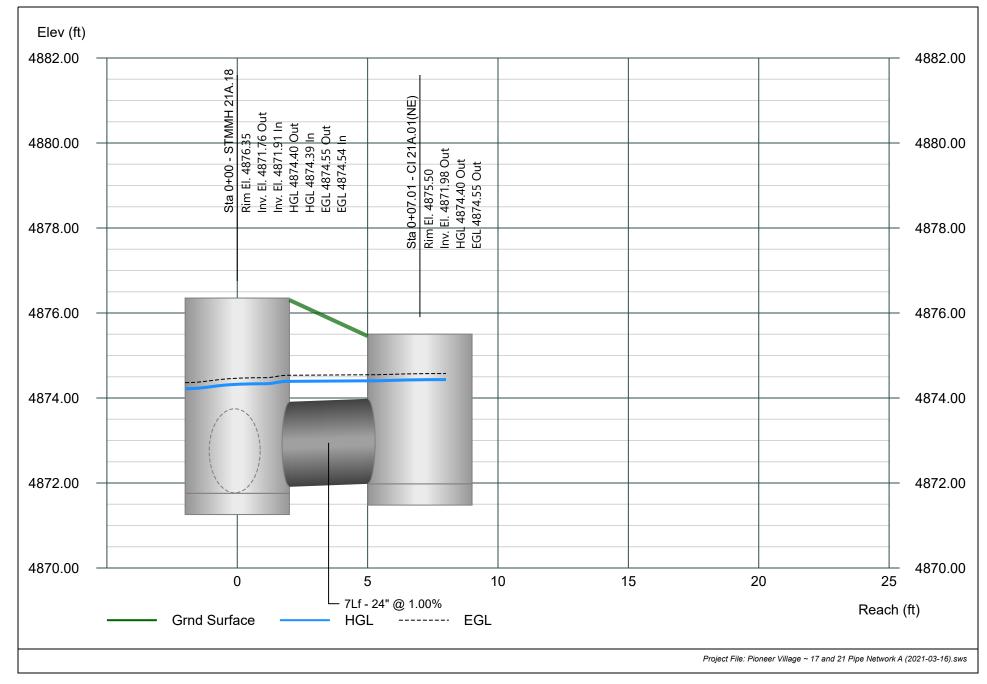
Line 5 - Pipe - (389) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



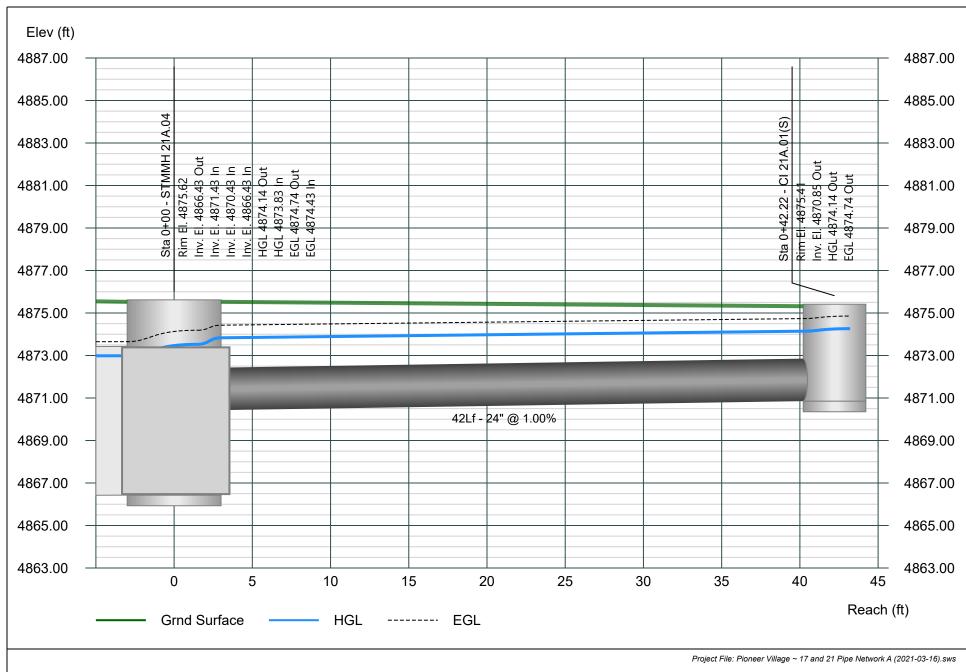
Line 6 - Pipe - (390) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



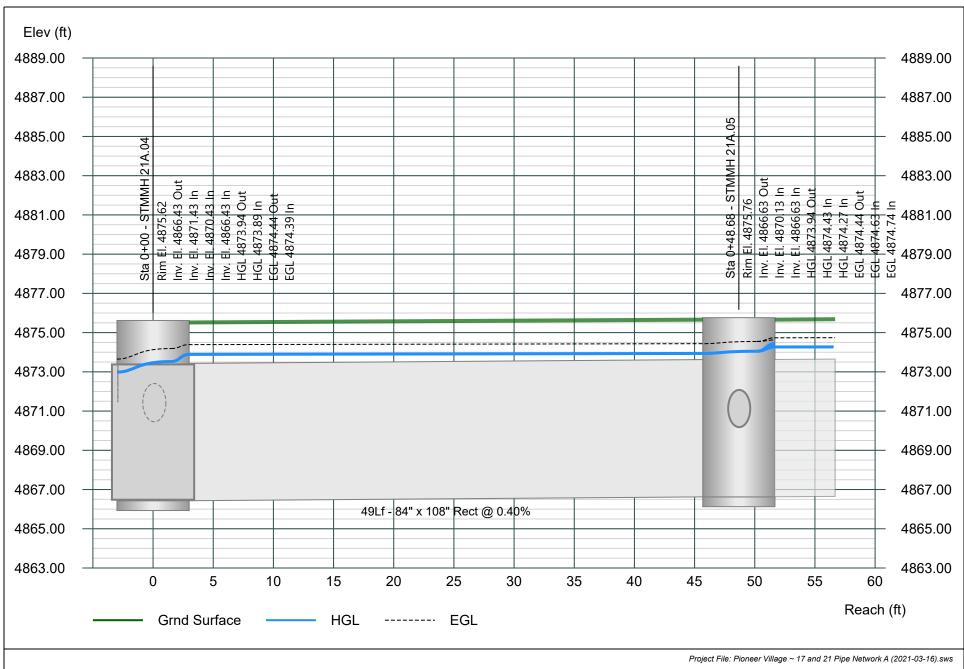
Line 7 - Pipe - (388) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24

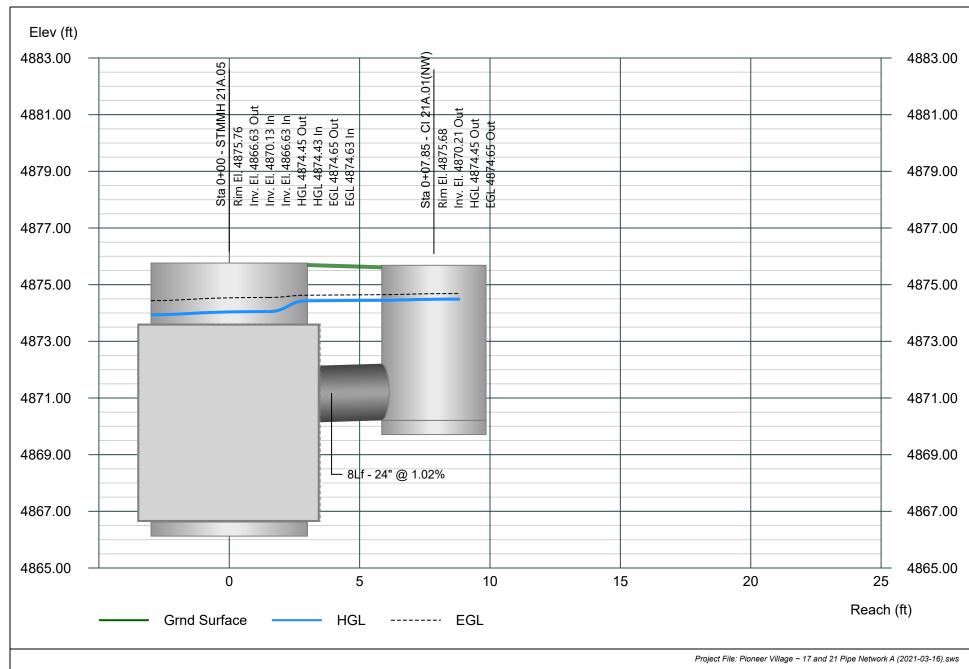


Line 8 - Pipe - (132) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24

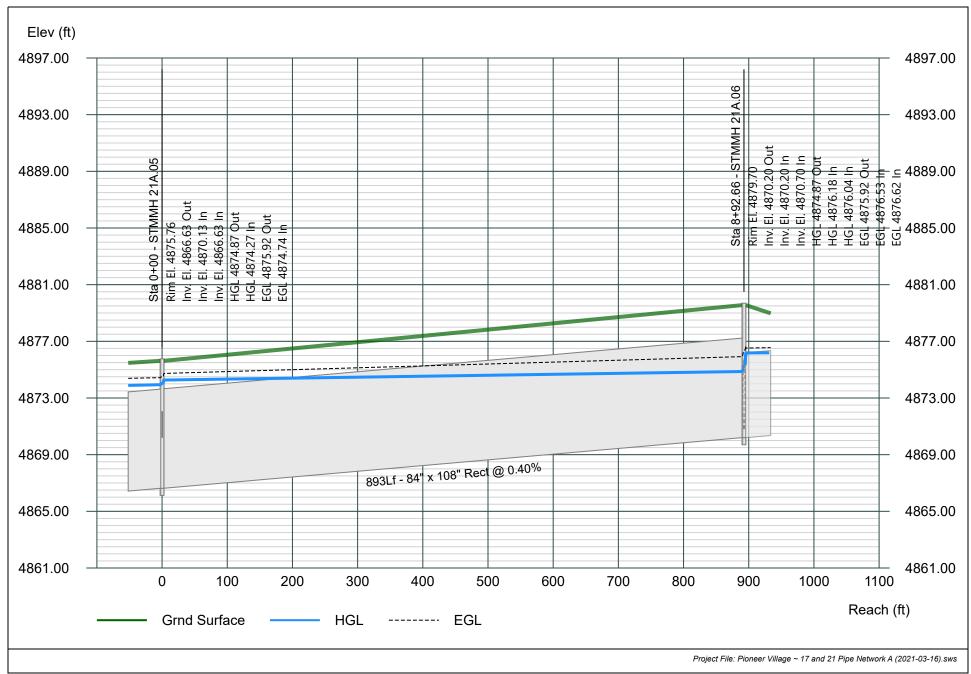


Line 9 - Pipe - (400) (PA 21A NETWORK)



Line 10 - Pipe - (130) (1)(0) (PA 21A NETWORK)

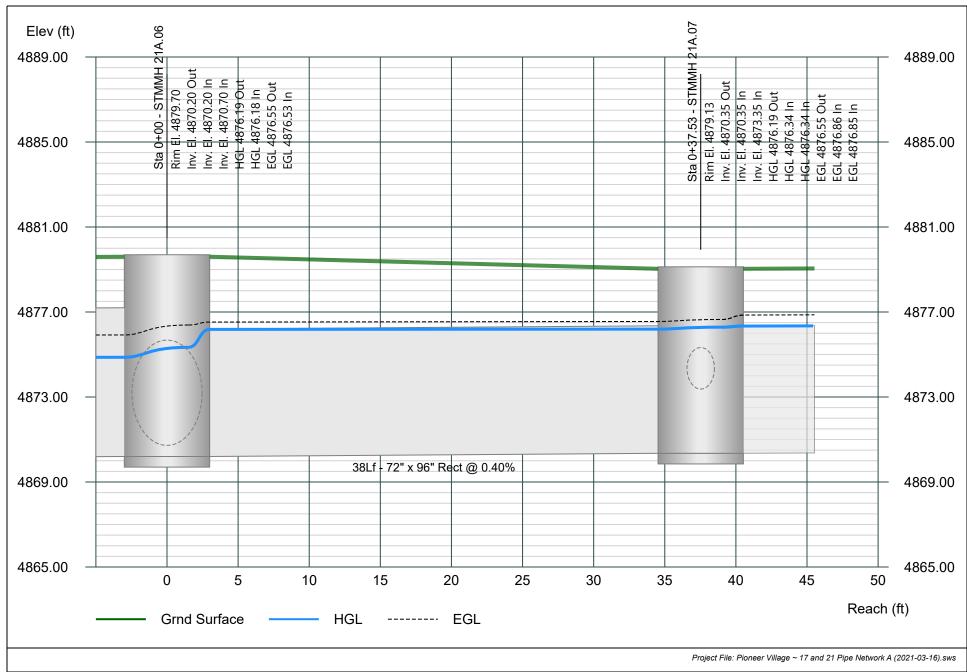
Stormwater Studio 2021 v 3.0.0.24



Line 11 - Pipe - (129) (1) (1) (1) (PA 21A NETWORK)

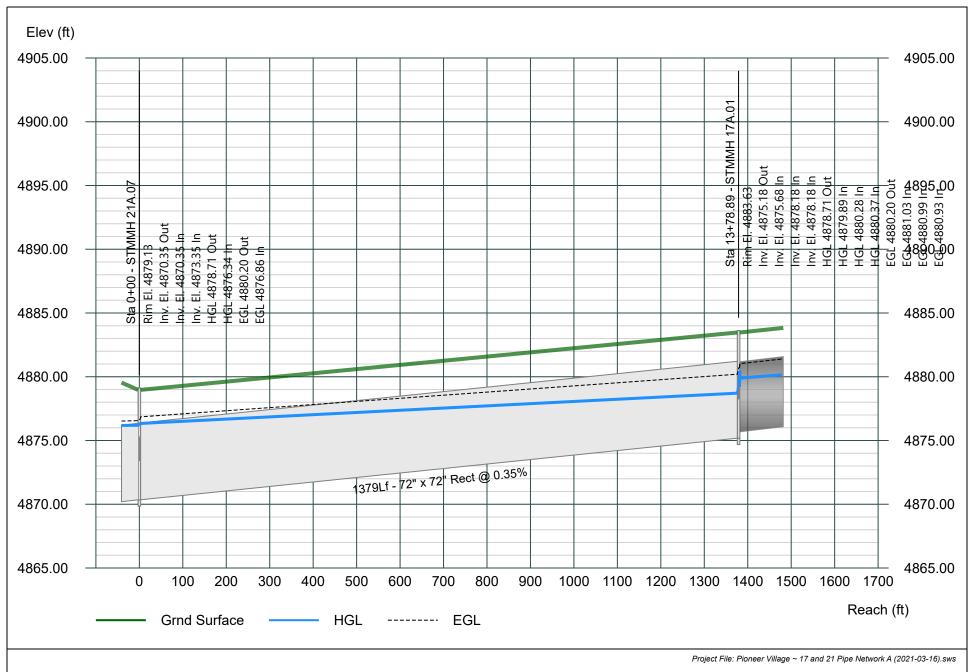
Project Name: Pioneer Village ~ 17 & 21 A Network

03-17-2021



Line 12 - Pipe - (129) (1) (1) (PA 21A NETWORK)

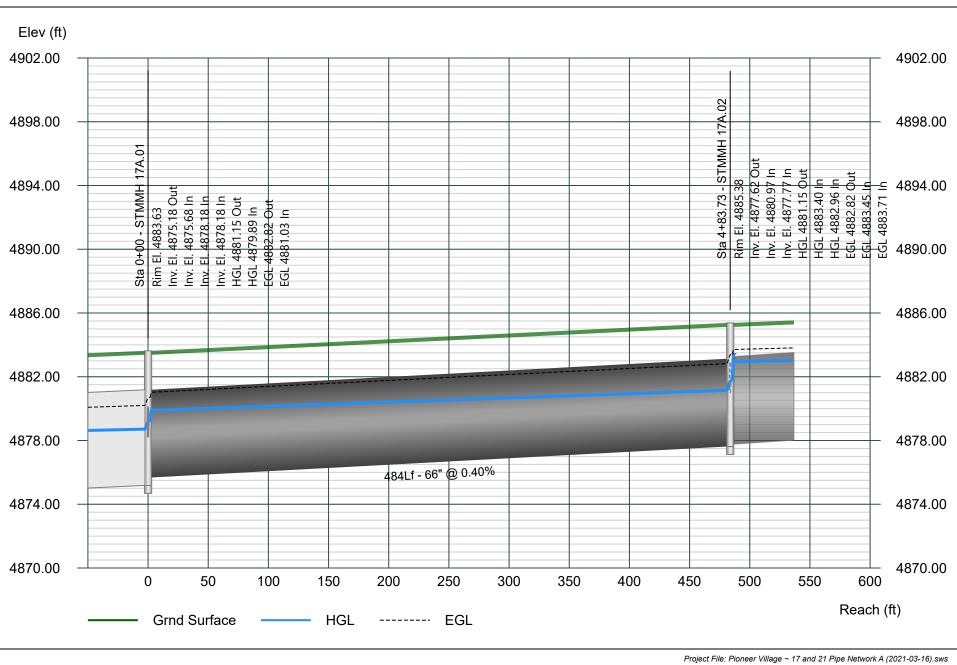
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village ~ 17 & 21 A Network

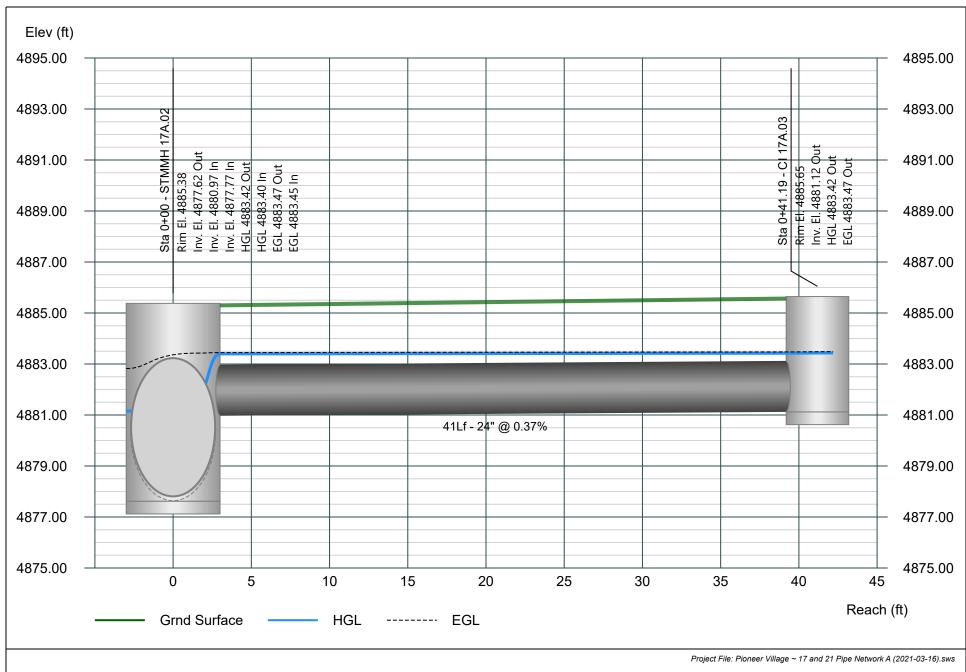
Line 13 - Pipe - (129) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



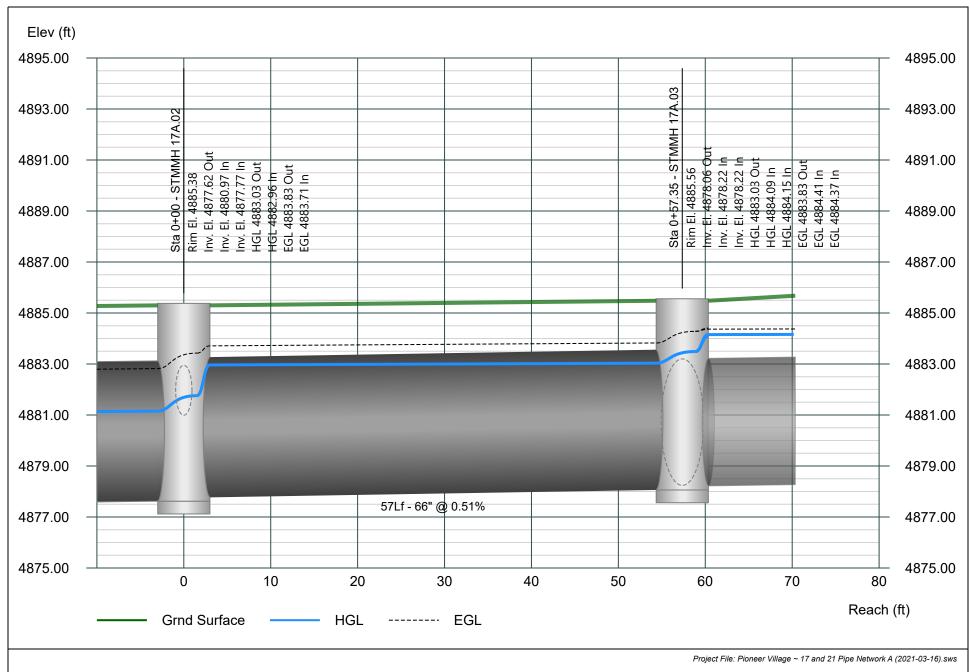
Line 14 - Pipe - (399) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



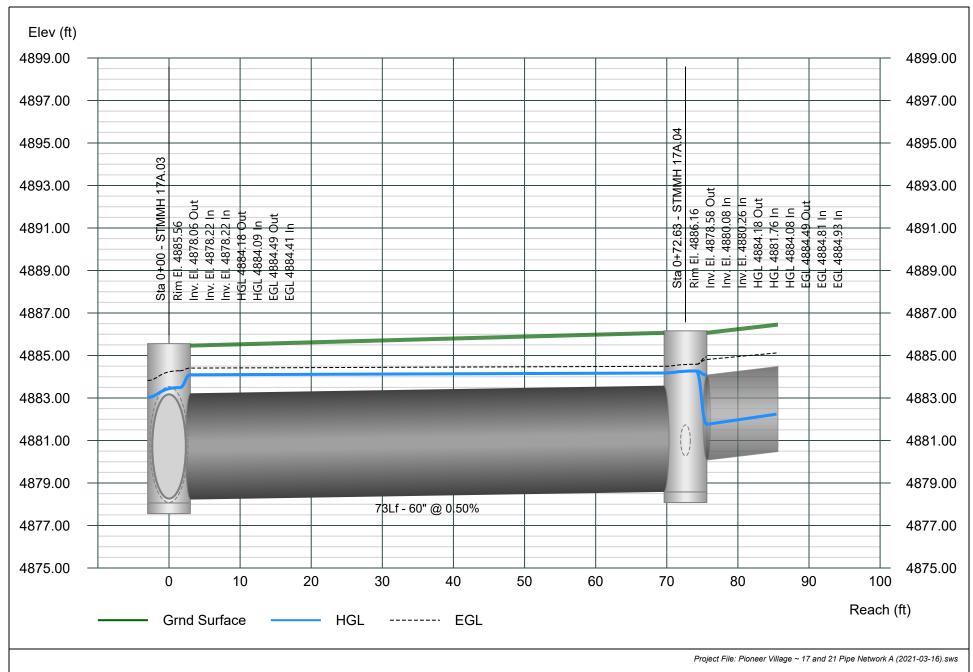
Line 15 - Pipe - (128) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



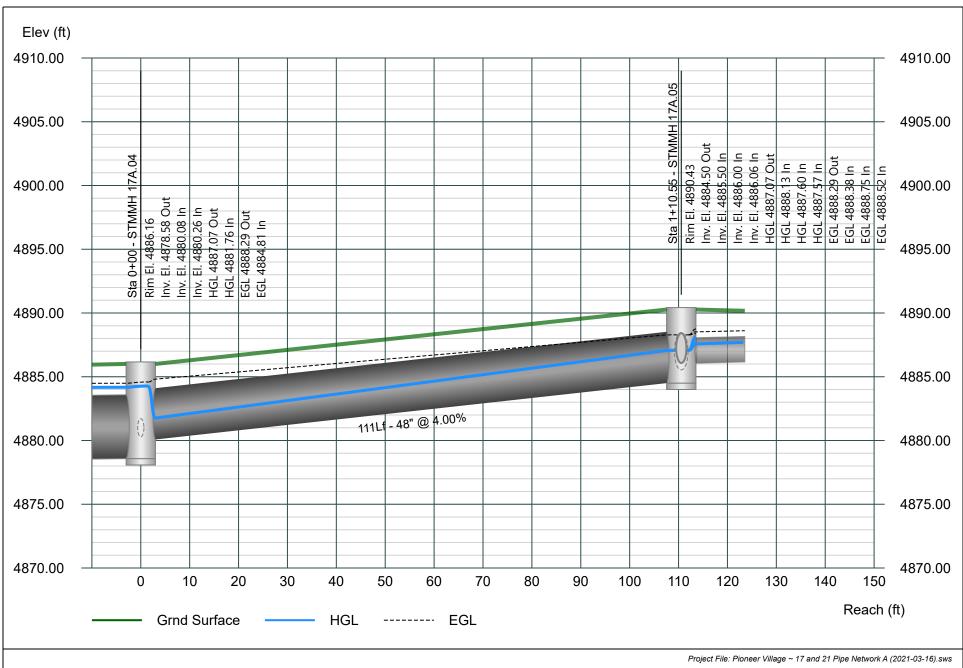
Line 16 - Pipe - (127) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



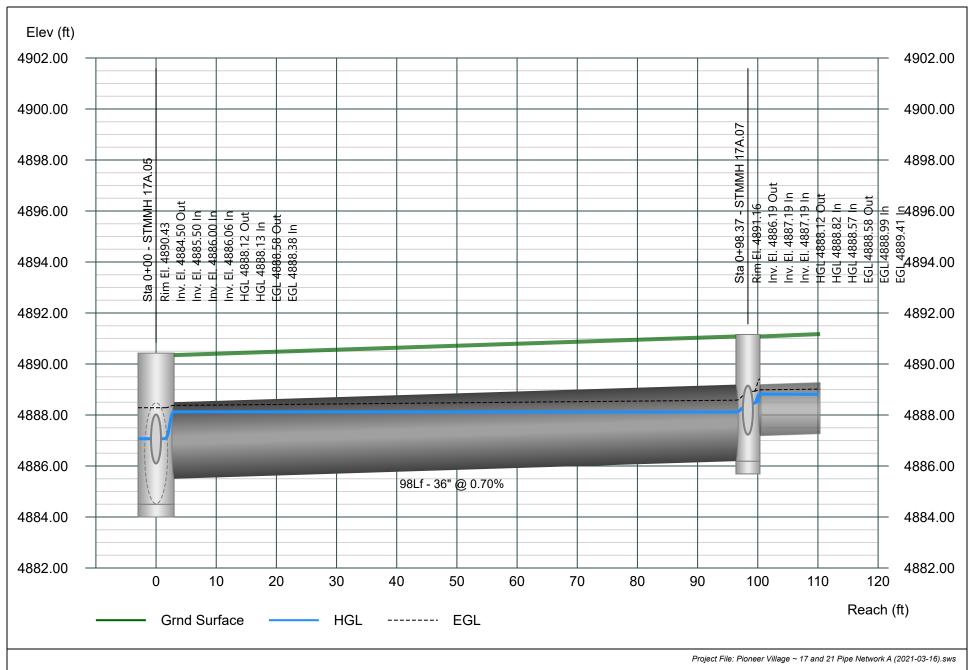
Line 17 - Pipe - (126)(0) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



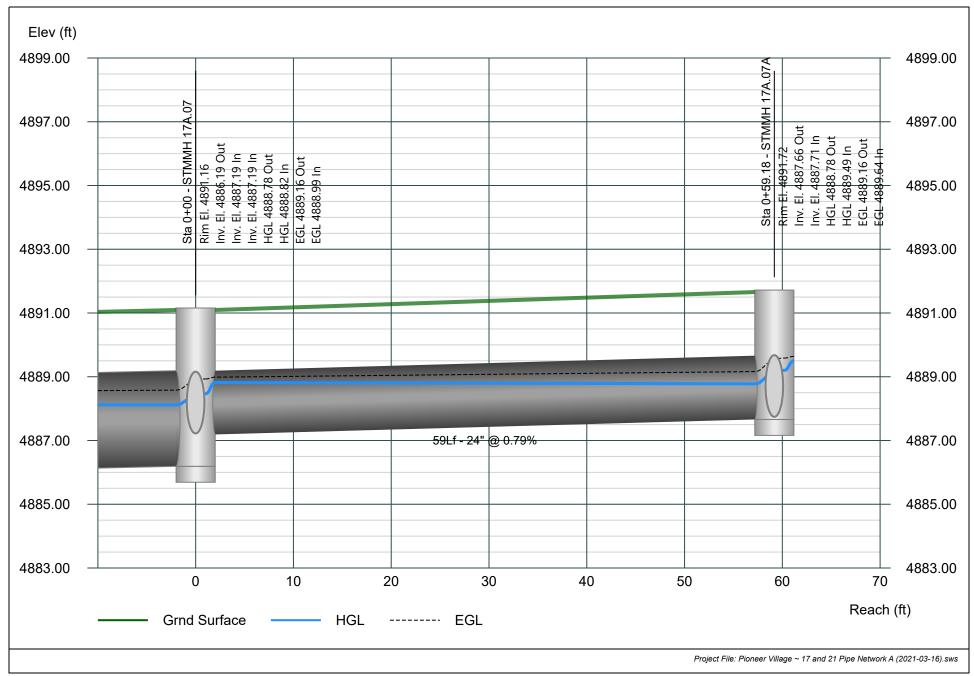
Line 18 - Pipe - (591) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 19 - Pipe - (604) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



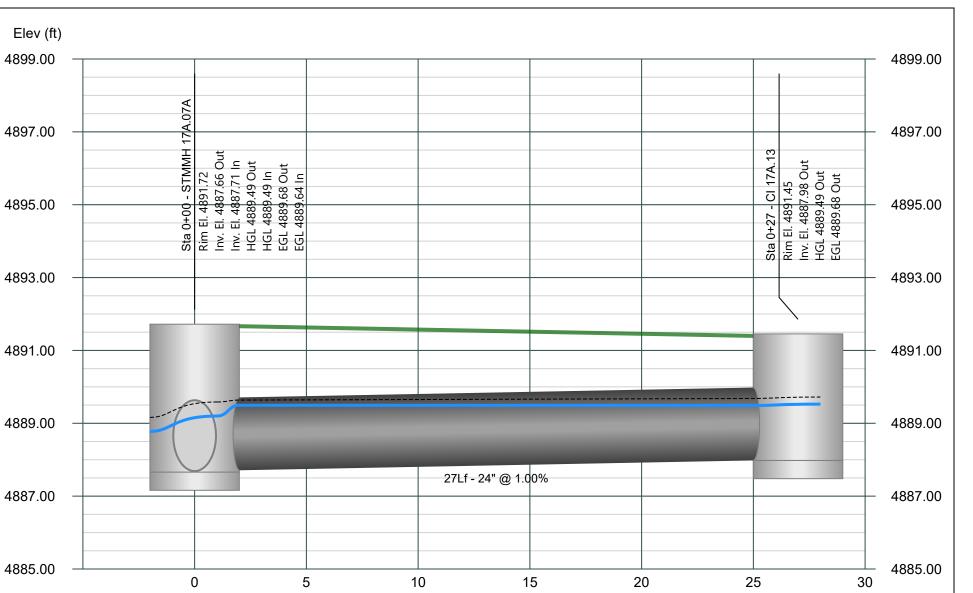
Line 20 - Pipe - (589) (PA 21A NETWORK)

Grnd Surface

HGL

----- EGL

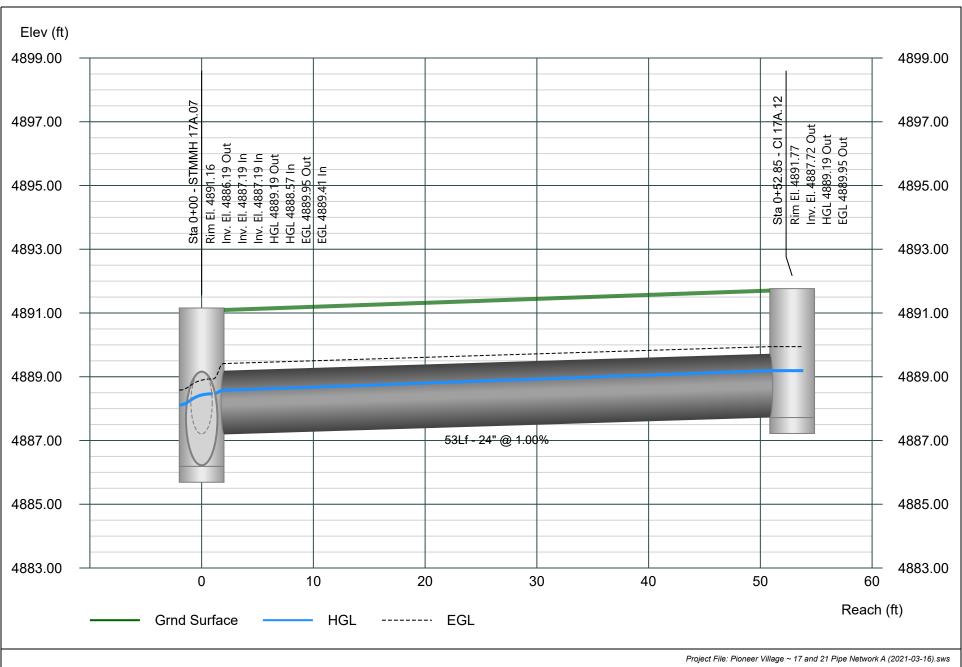
Stormwater Studio 2021 v 3.0.0.24



Project File: Pioneer Village ~ 17 and 21 Pipe Network A (2021-03-16).sws

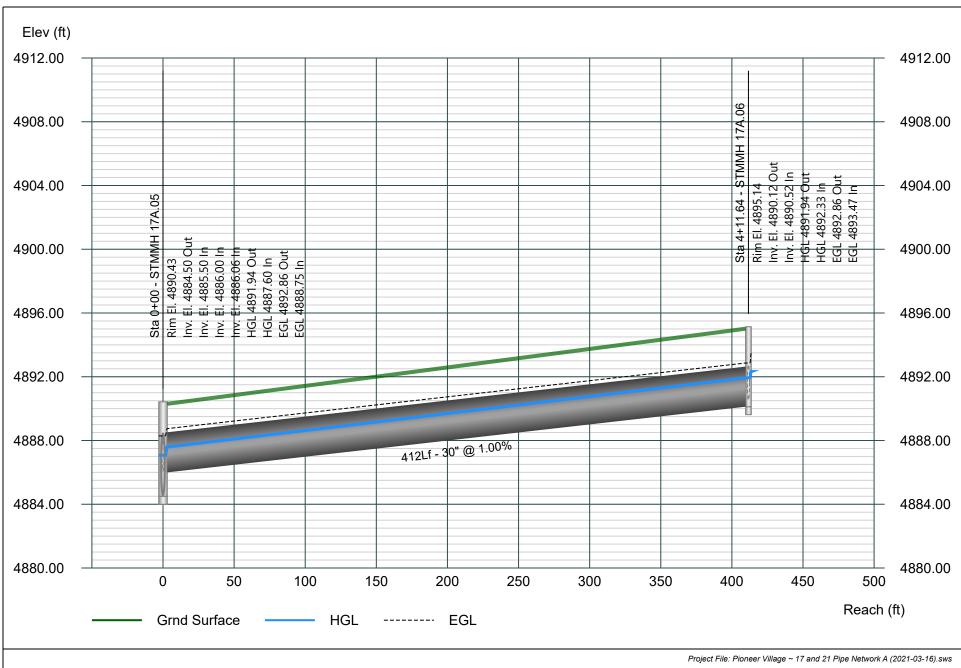
Line 21 - Pipe - (590) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



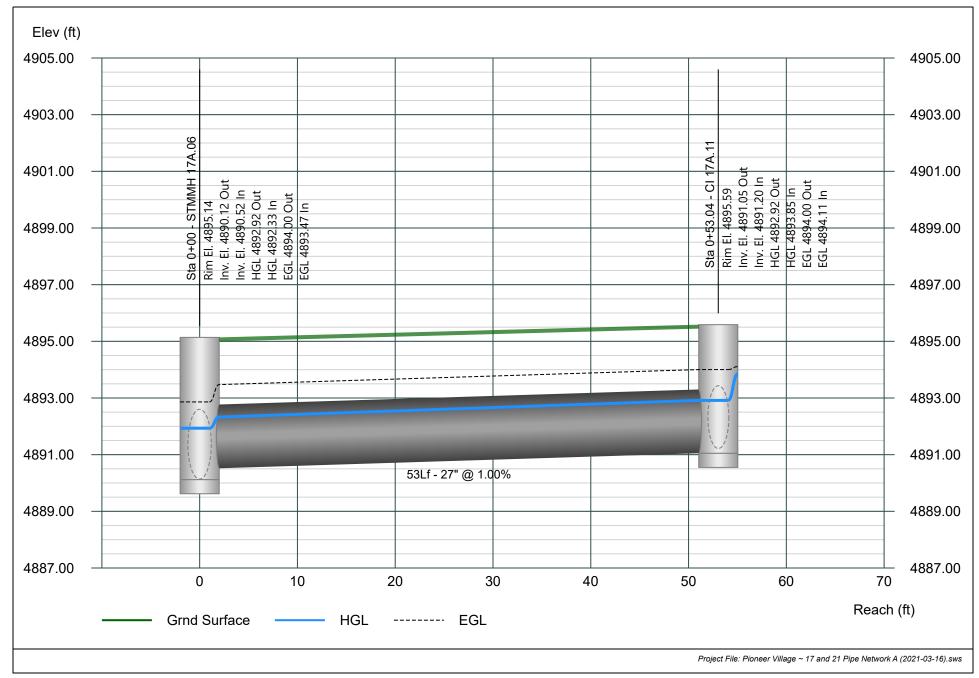
Line 22 - Pipe - (594) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



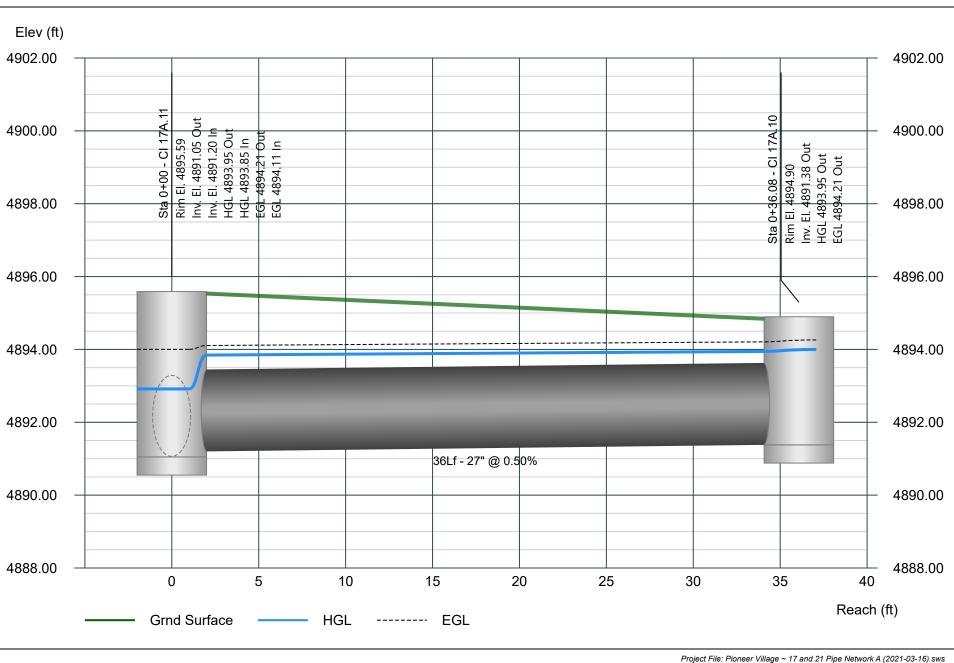
Line 23 - Pipe - (593) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



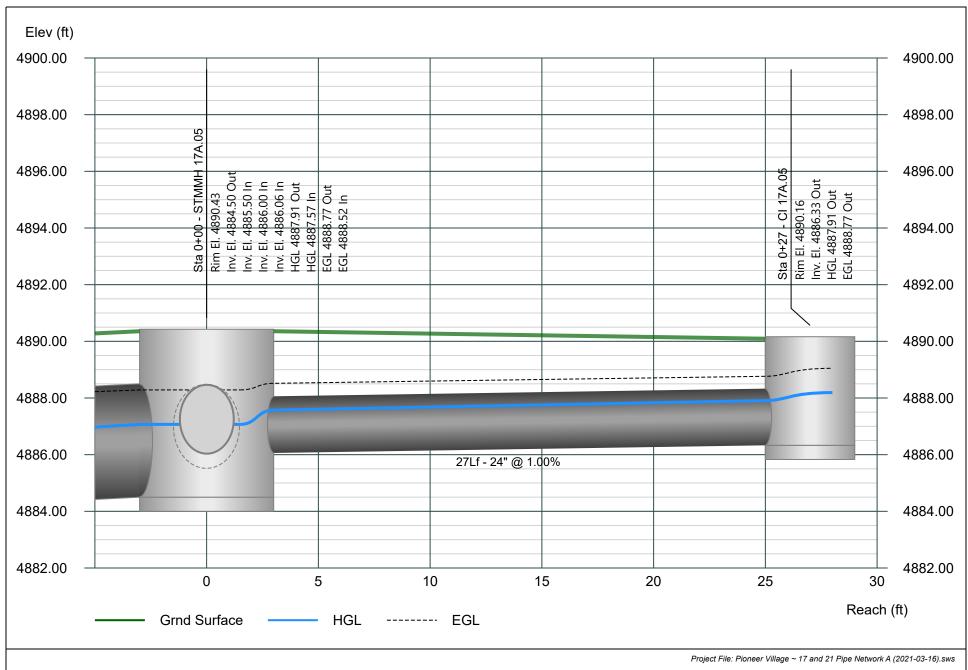
Line 24 - Pipe - (592) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



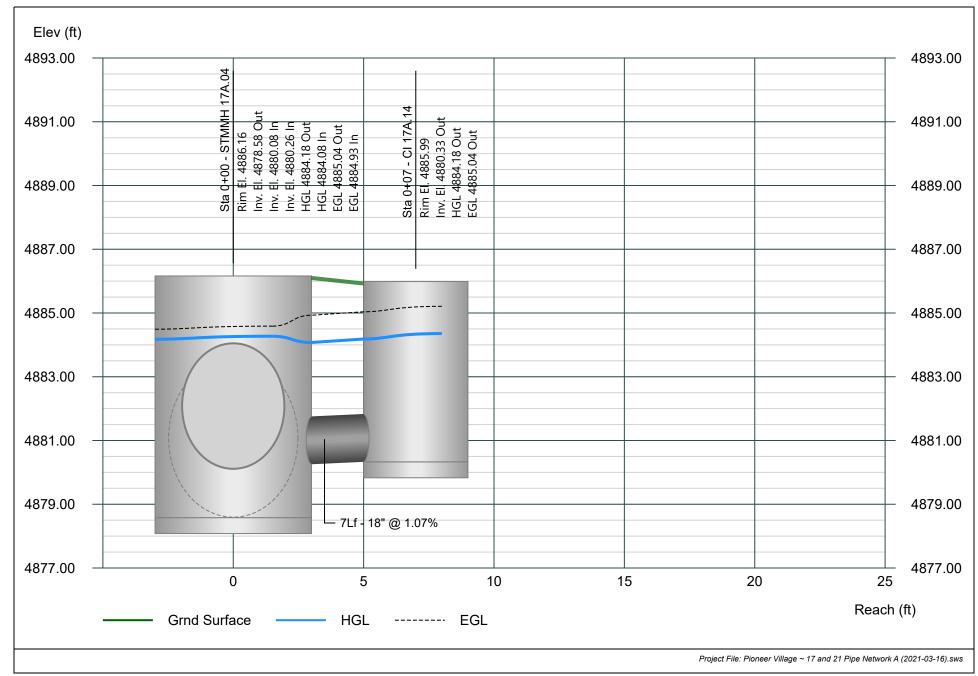
Line 25 - Pipe - (607) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 26 - Pipe - (605) (PA 21A NETWORK)

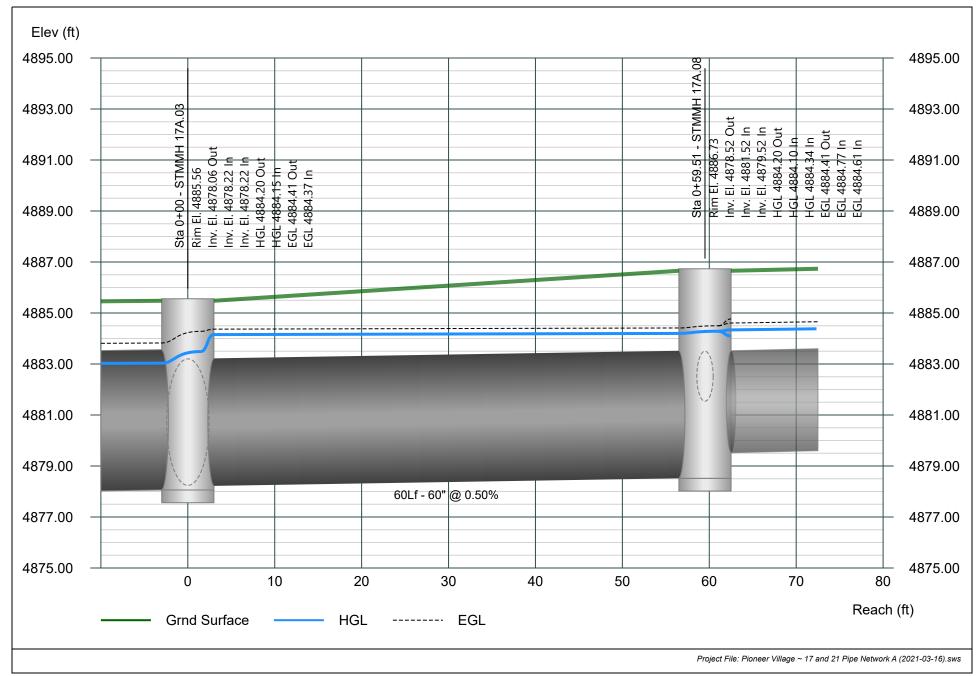
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village ~ 17 & 21 A Network

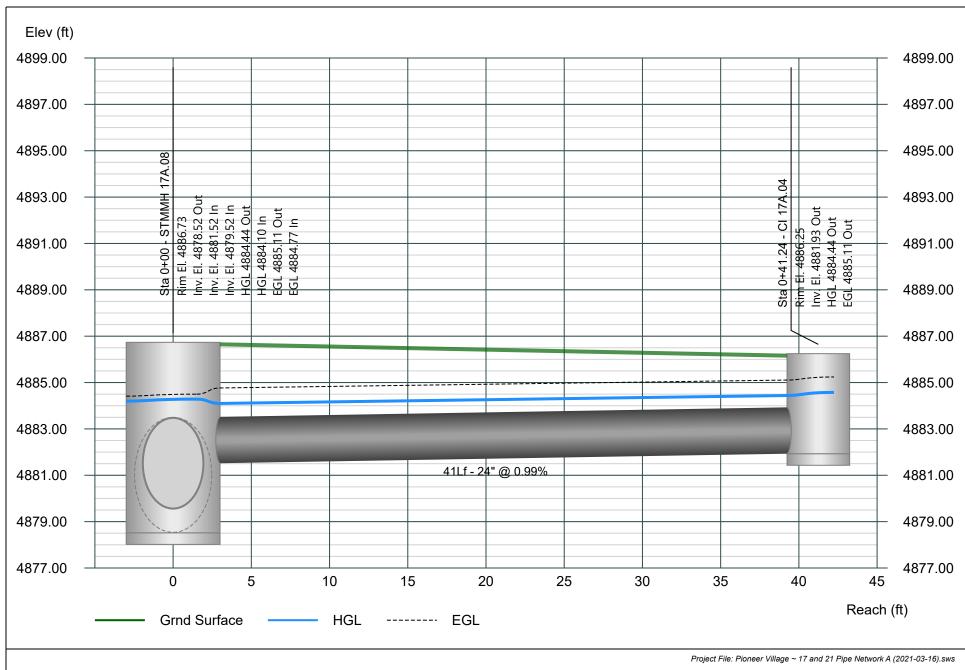
Line 27 - Pipe - (397) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



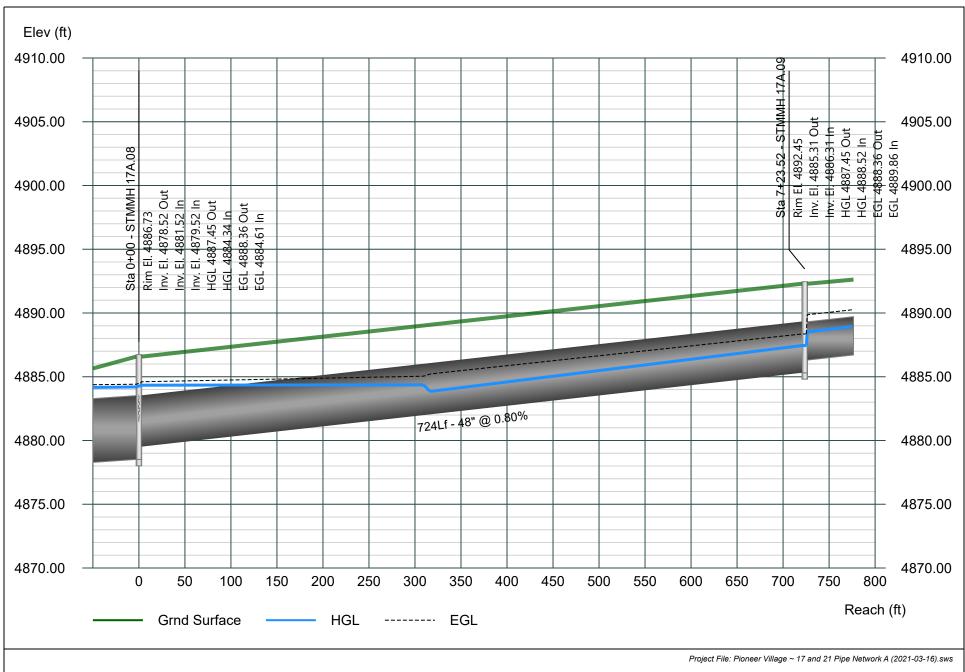
Line 28 - Pipe - (396) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 29 - Pipe - (598) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 30 - Pipe - (597) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24

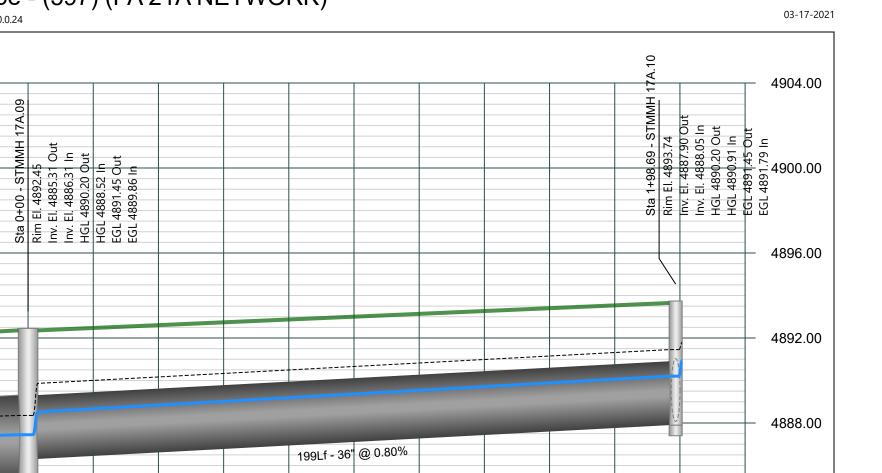
Elev (ft)

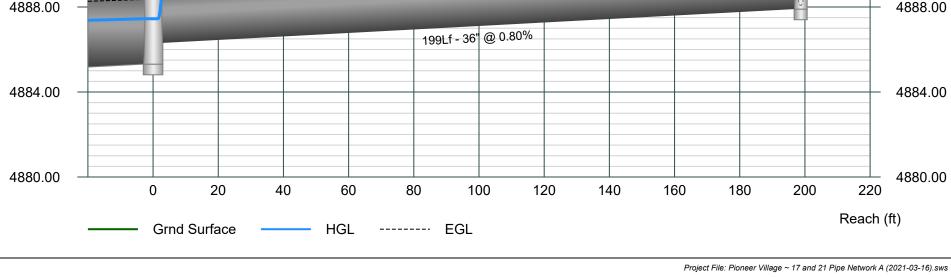
4904.00

4900.00

4896.00

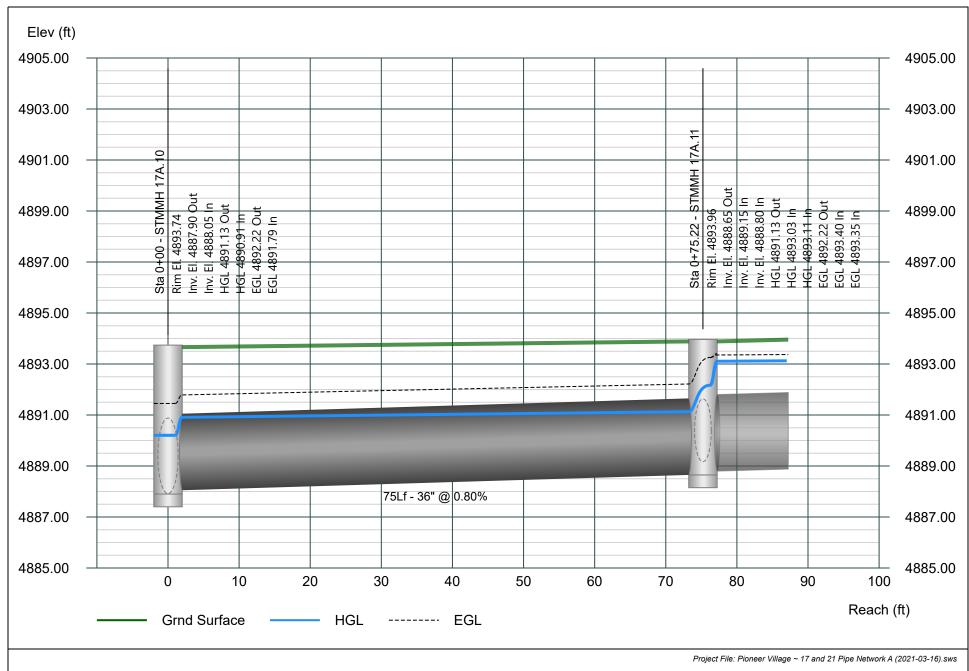
4892.00





Line 31 - Pipe - (596) (1) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village ~ 17 & 21 A Network

Line 32 - Pipe - (603) (PA 21A NETWORK)

0

Grnd Surface

5

HGL

Stormwater Studio 2021 v 3.0.0.24

Elev (ft)

4903.00

4901.00

4899.00

4897.00

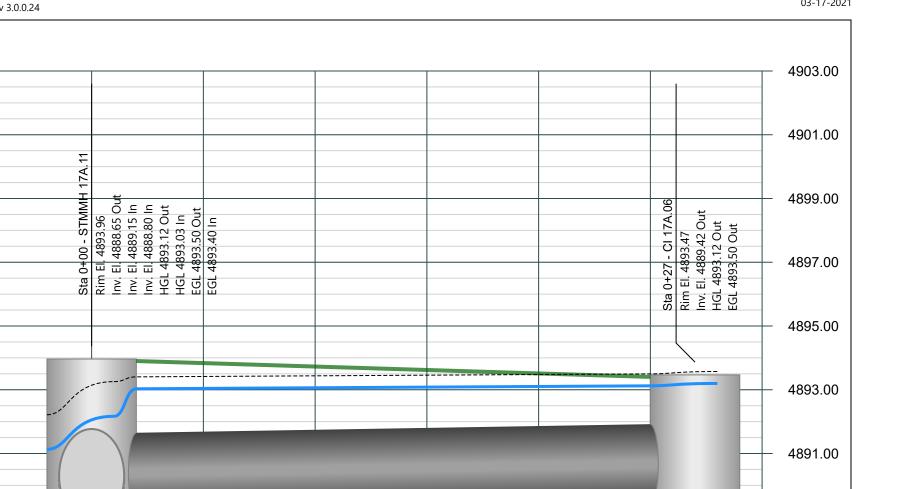
4895.00

4893.00

4891.00

4889.00

4887.00



27Lf - 30" @ 1.00%

15

20

10

----- EGL

Project File: Pioneer Village ~ 17 and 21 Pipe Network A (2021-03-16).sws

25

03-17-2021

4889.00

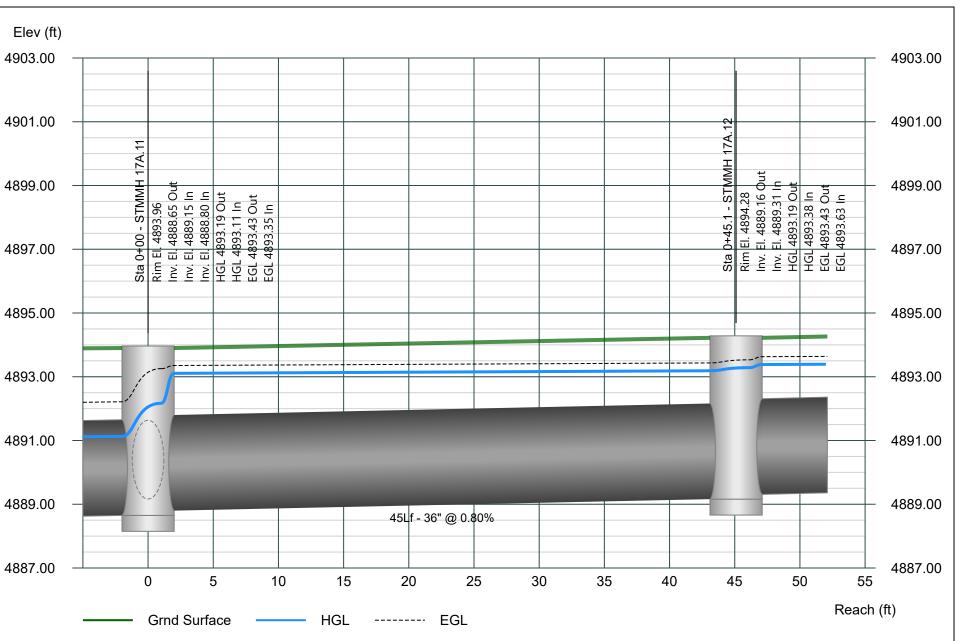
4887.00

30

Reach (ft)

Line 33 - Pipe - (596) (PA 21A NETWORK)

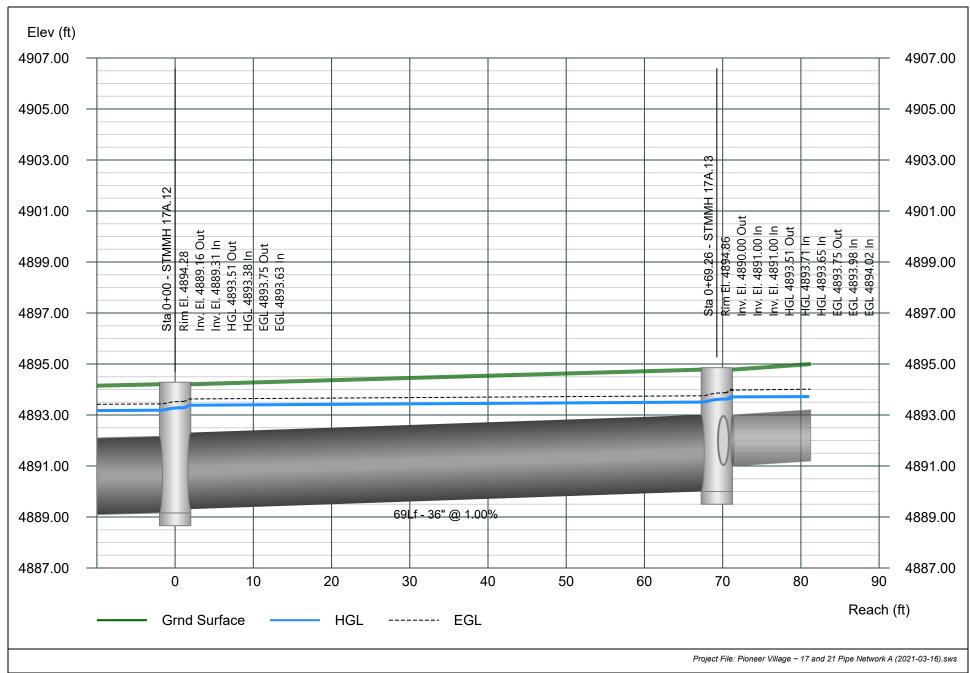
Stormwater Studio 2021 v 3.0.0.24



Project File: Pioneer Village ~ 17 and 21 Pipe Network A (2021-03-16).sws

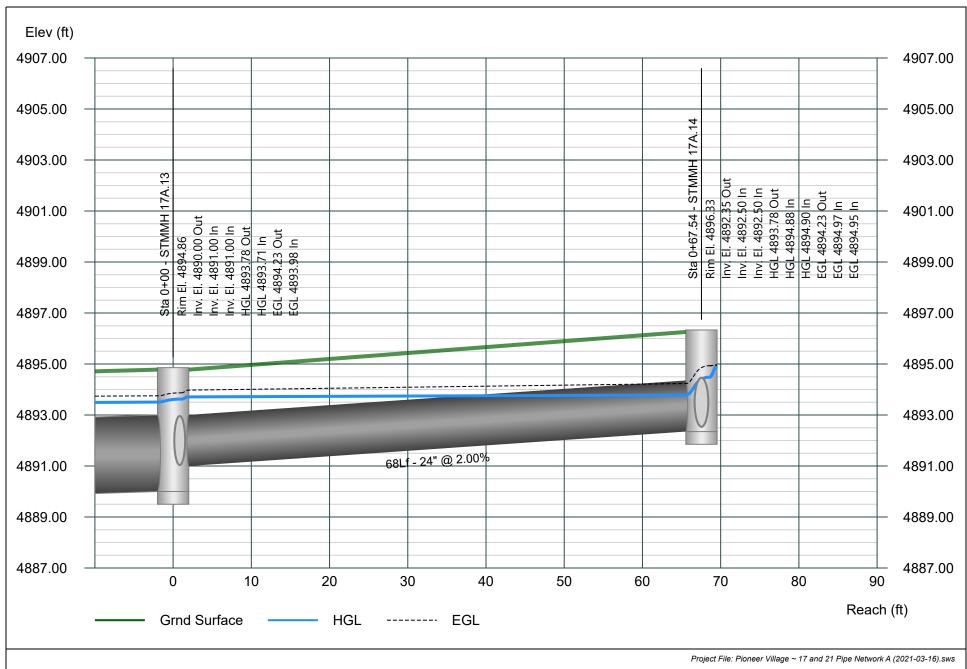
Line 34 - Pipe - (595) (1) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



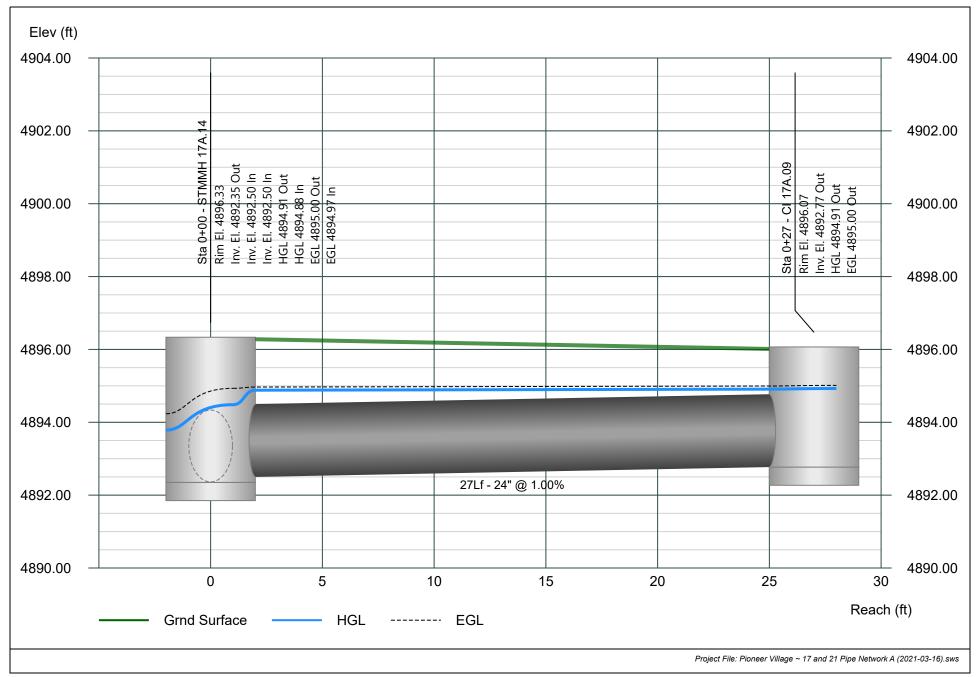
Line 35 - Pipe - (595) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



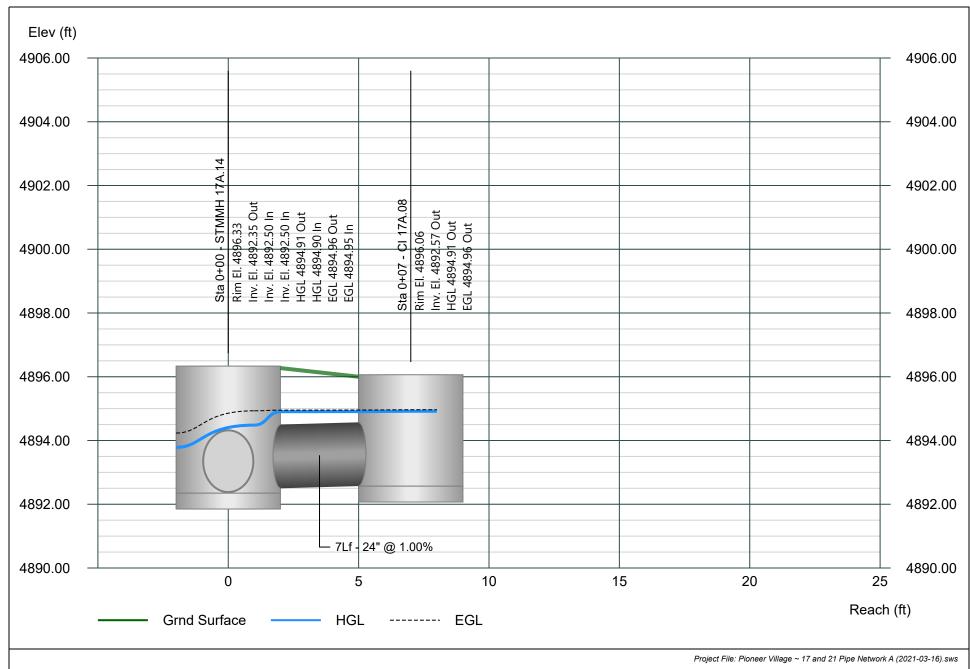
Line 36 - Pipe - (602) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 37 - Pipe - (601) (PA 21A NETWORK)

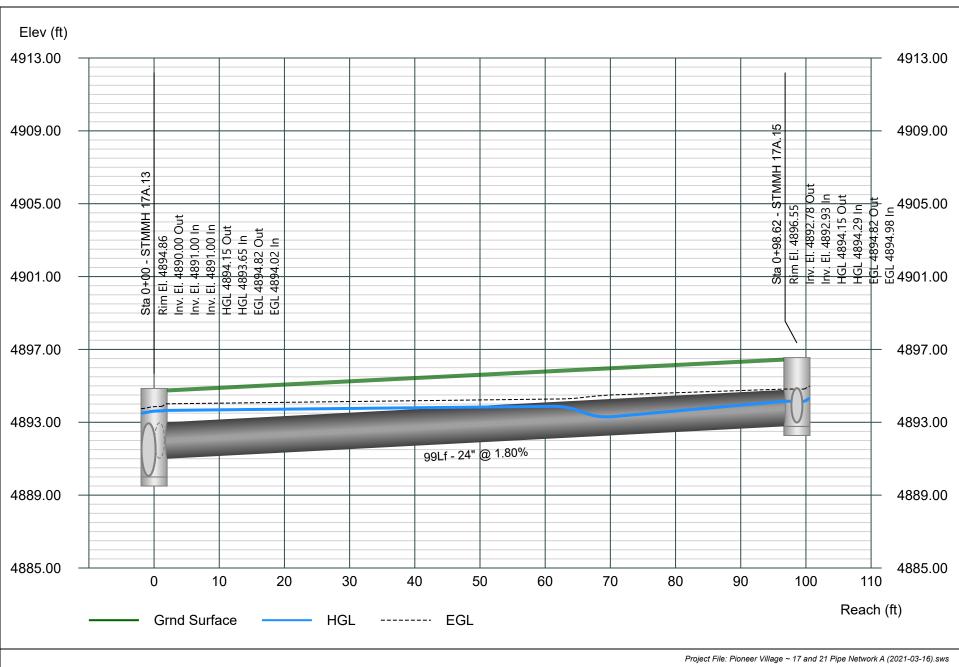
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village ~ 17 & 21 A Network

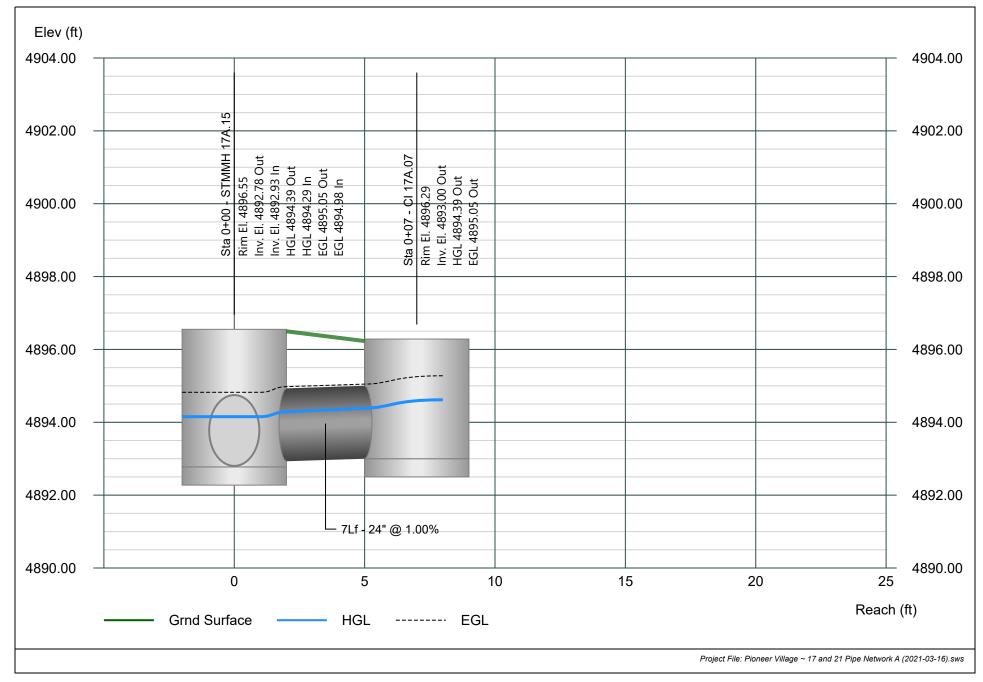
Line 38 - Pipe - (599) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



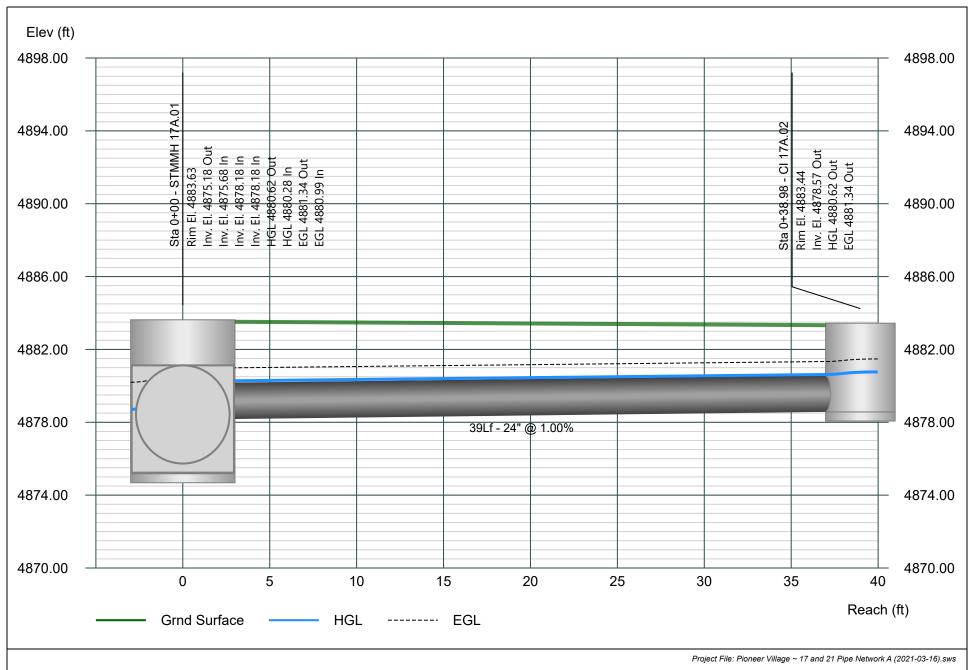
Line 39 - Pipe - (600) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



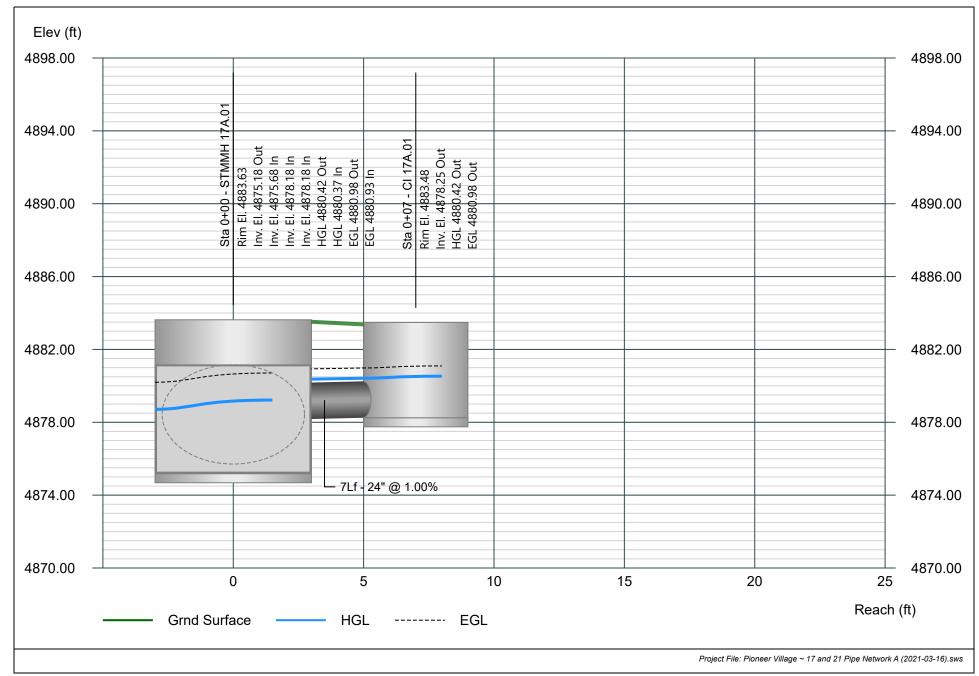
Line 40 - Pipe - (566) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



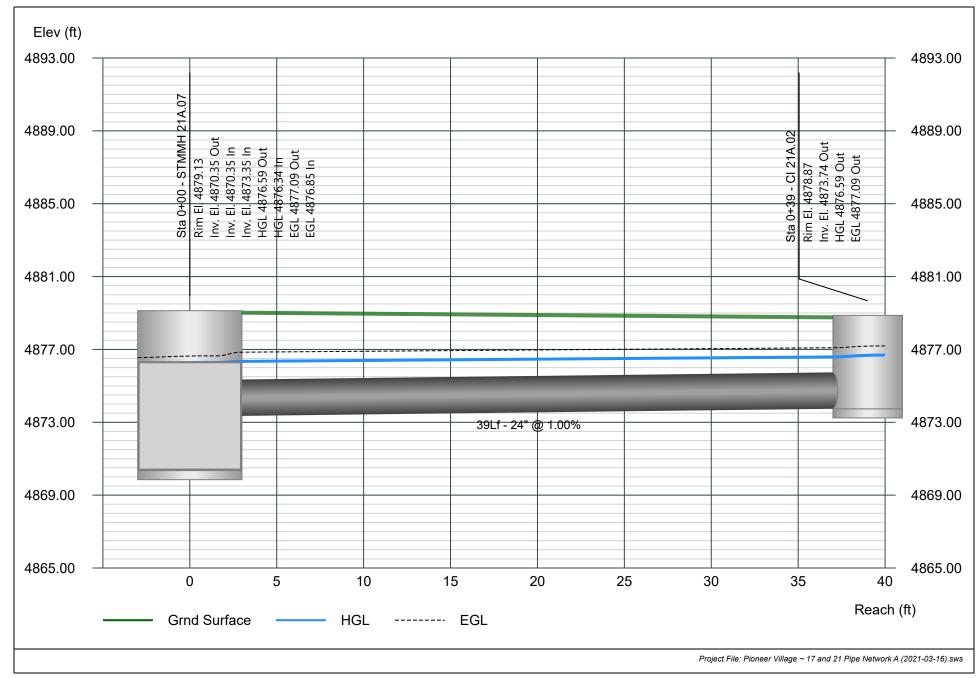
Line 41 - Pipe - (581) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



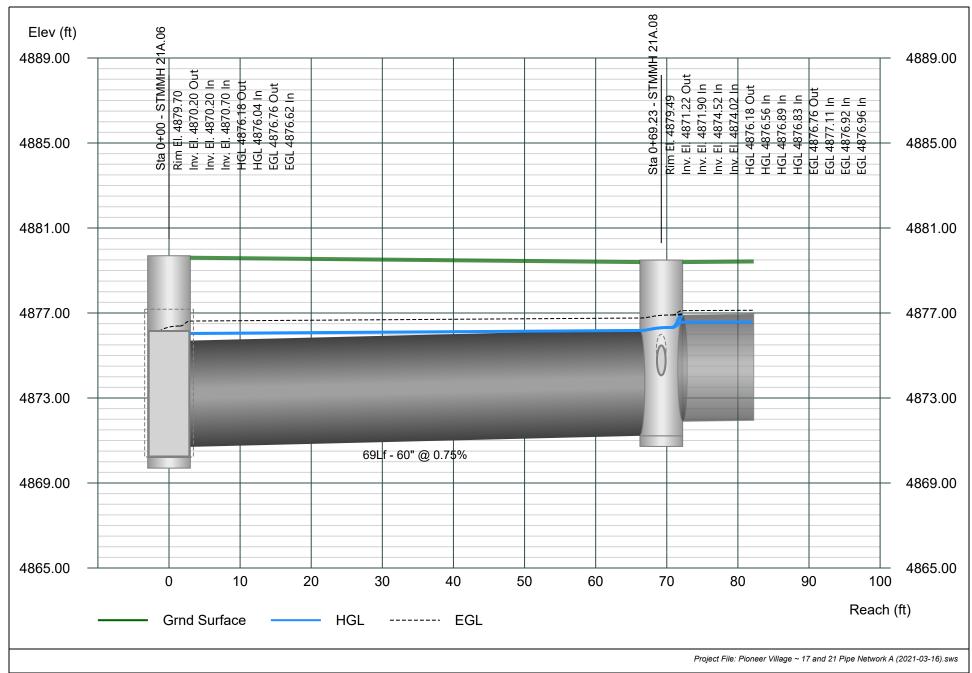
Line 42 - Pipe - (606) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



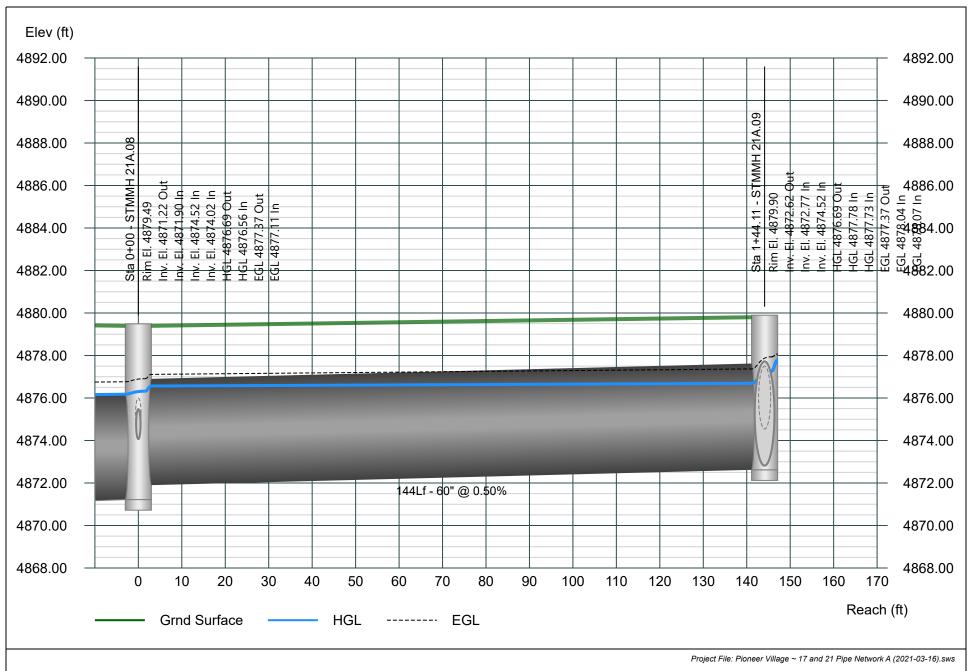
Line 43 - Pipe - (526) (1) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



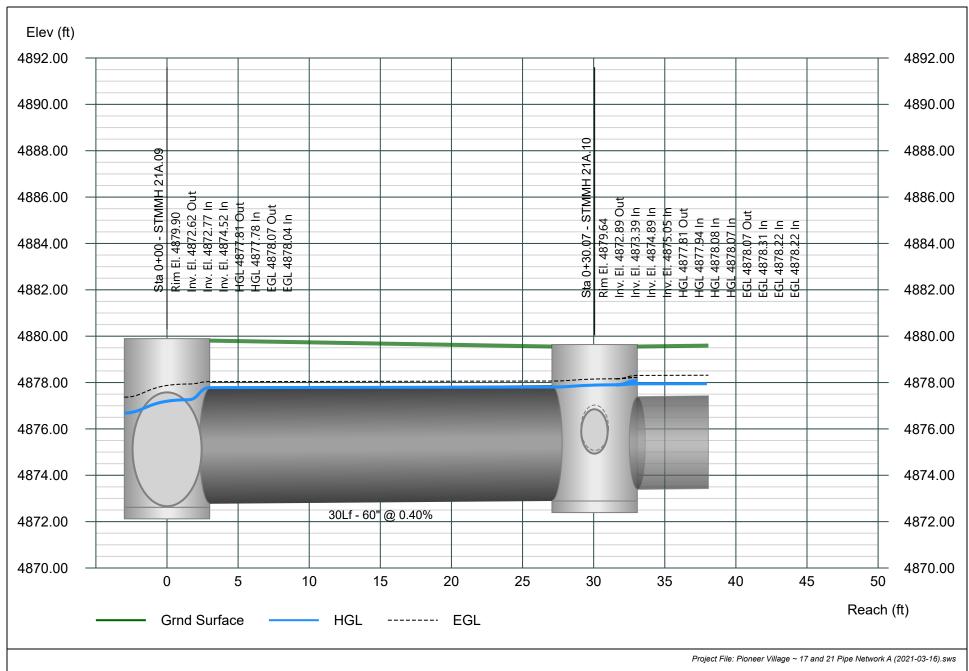
Line 44 - Pipe - (526) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



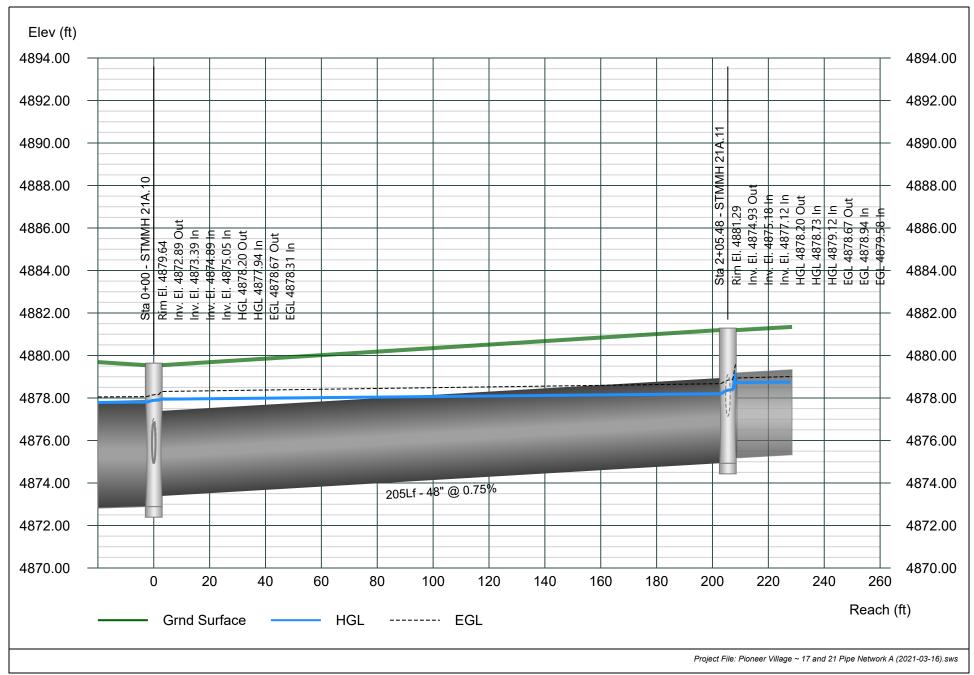
Line 45 - Pipe - (534) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



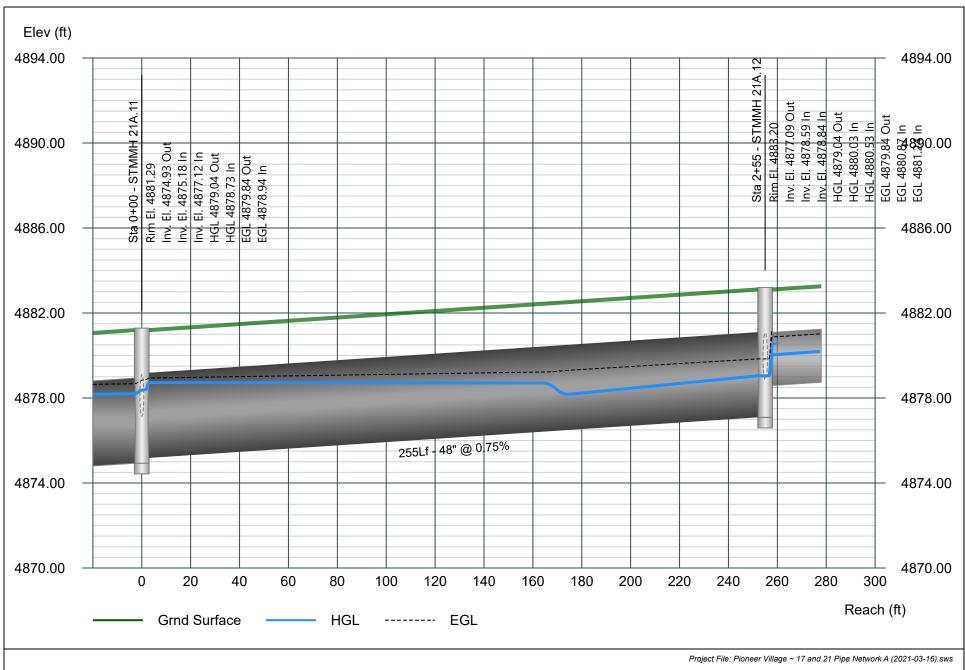
Line 46 - Pipe - (533) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



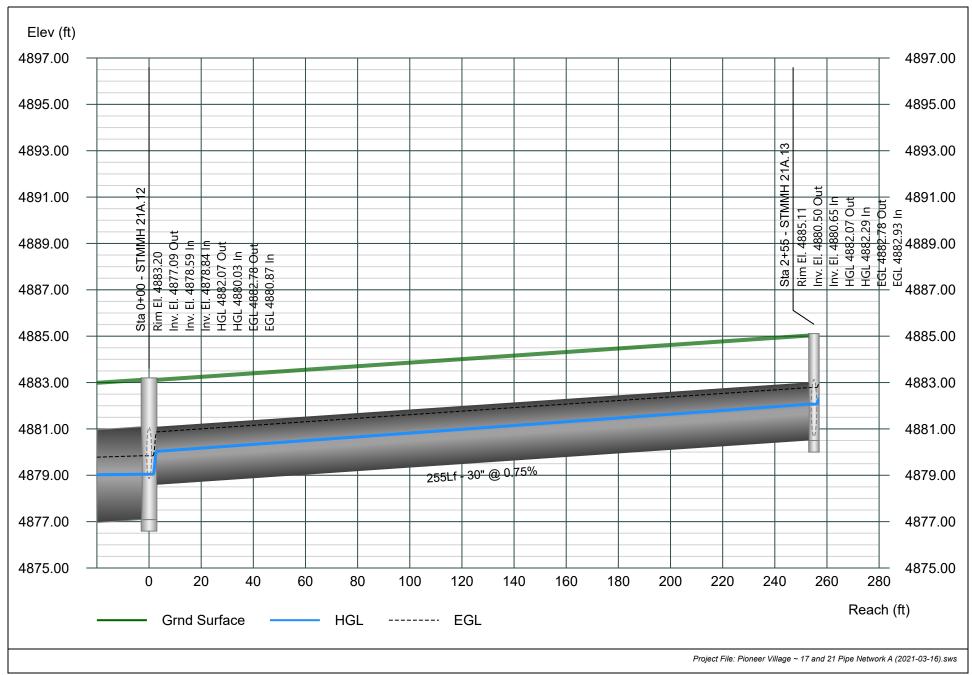
Line 47 - Pipe - (548) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



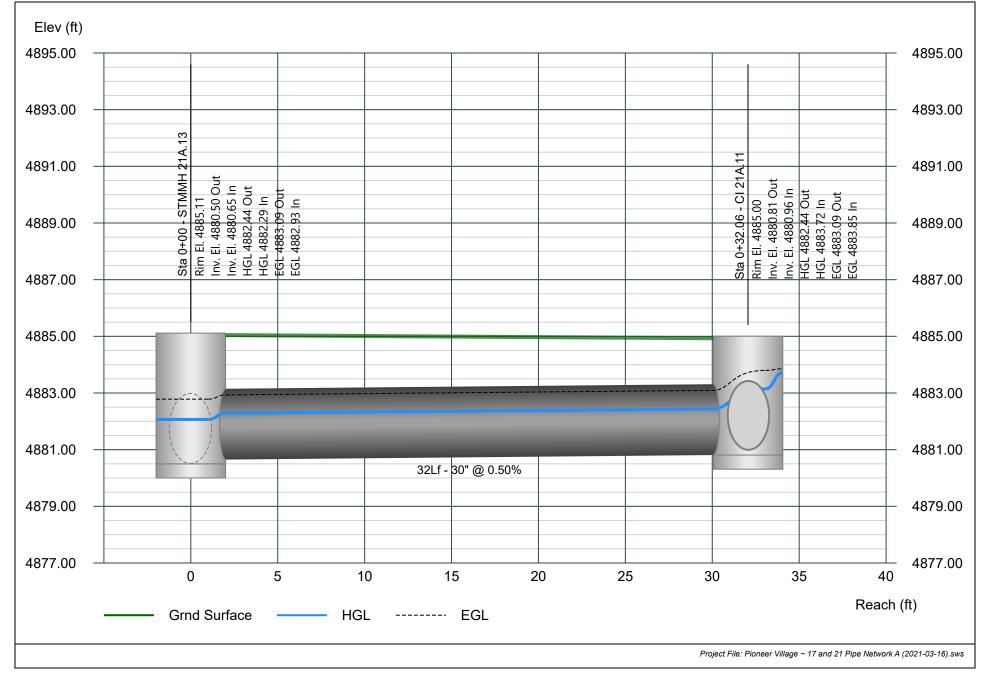
Line 48 - Pipe - (546) (2) (1) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



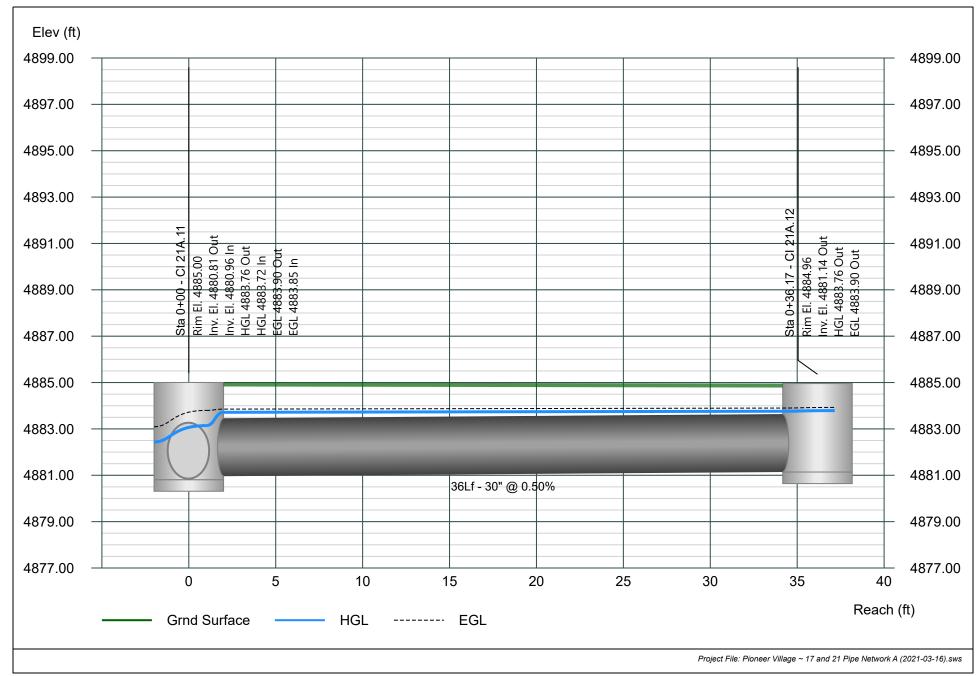
Line 49 - Pipe - (545) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



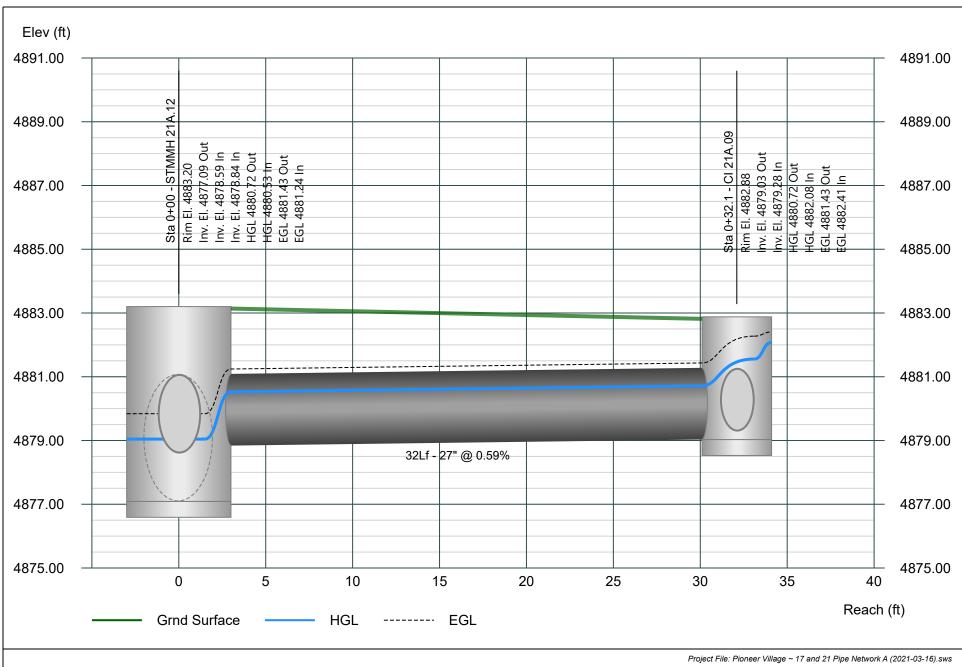
Line 50 - Pipe - (527) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 51 - Pipe - (549) (PA 21A NETWORK)

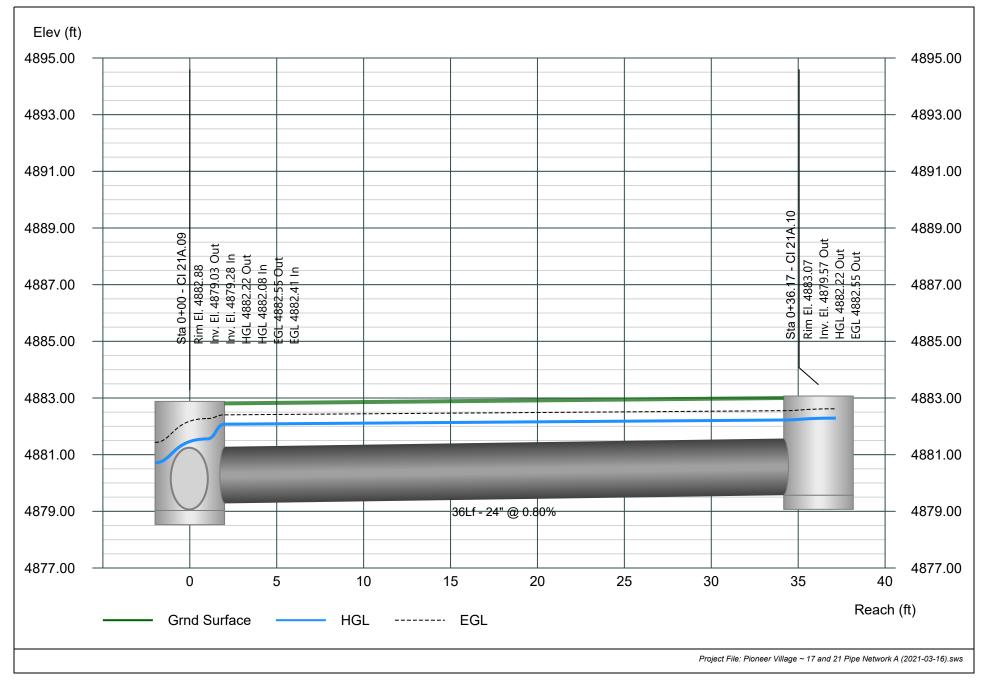
Stormwater Studio 2021 v 3.0.0.24



Line 52 - Pipe - (529) (PA 21A NETWORK)

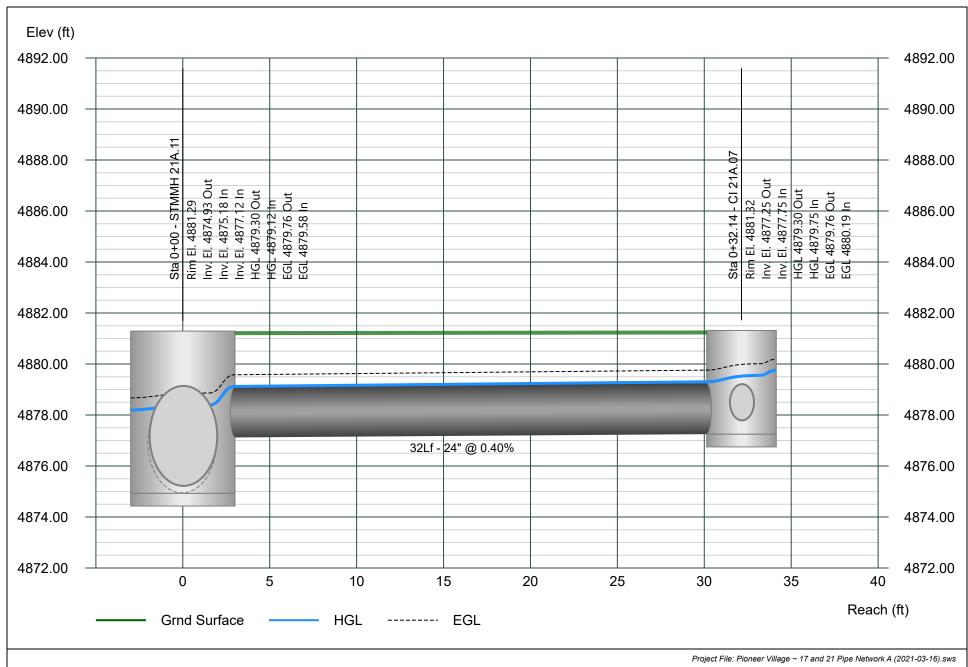
Stormwater Studio 2021 v 3.0.0.24





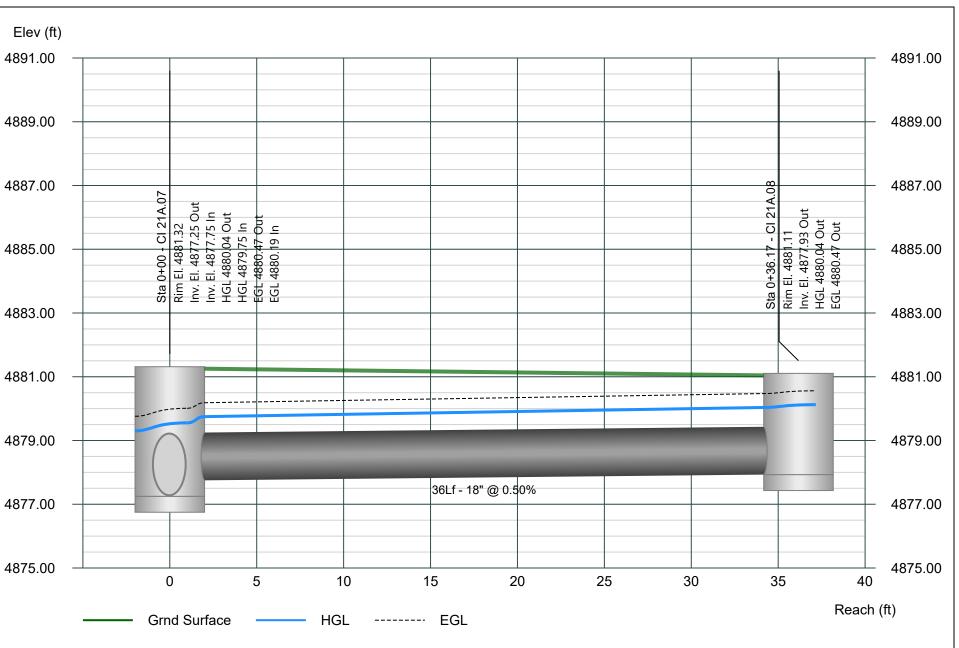
Line 53 - Pipe - (532)(0) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 54 - Pipe - (531) (PA 21A NETWORK)

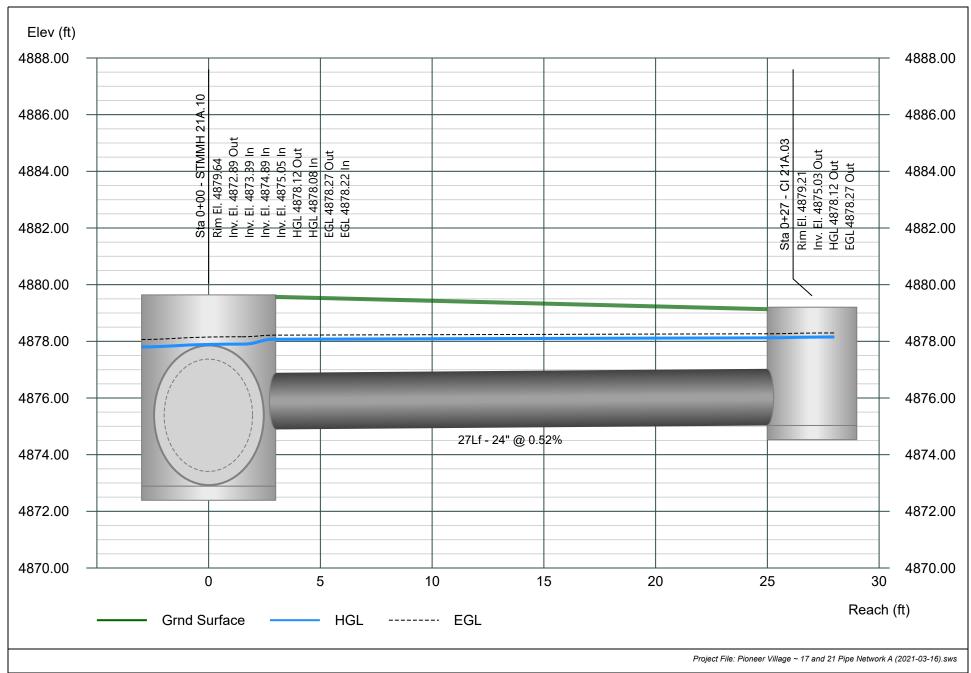
Stormwater Studio 2021 v 3.0.0.24



Project File: Pioneer Village ~ 17 and 21 Pipe Network A (2021-03-16).sws

Line 55 - Pipe - (536) (PA 21A NETWORK)

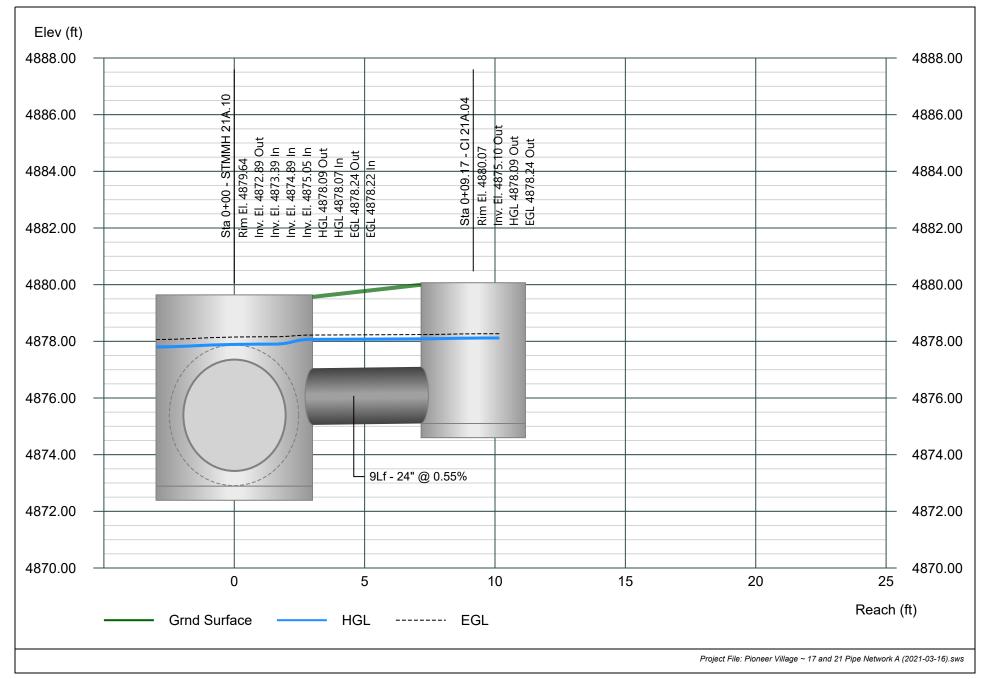
Stormwater Studio 2021 v 3.0.0.24



Line 56 - Pipe - (535) (PA 21A NETWORK)

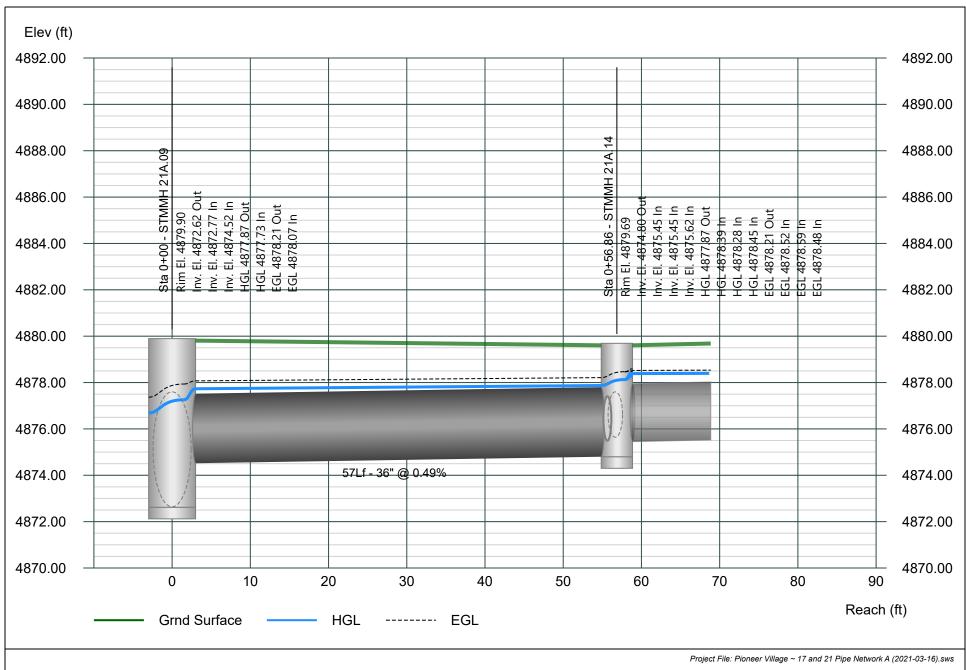
Stormwater Studio 2021 v 3.0.0.24





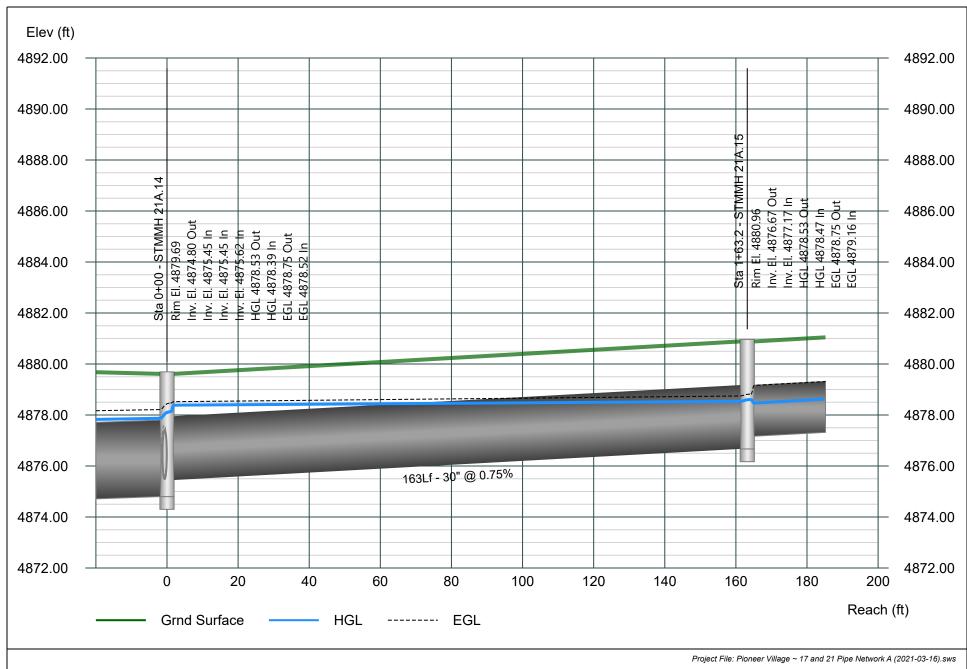
Line 57 - Pipe - (525) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



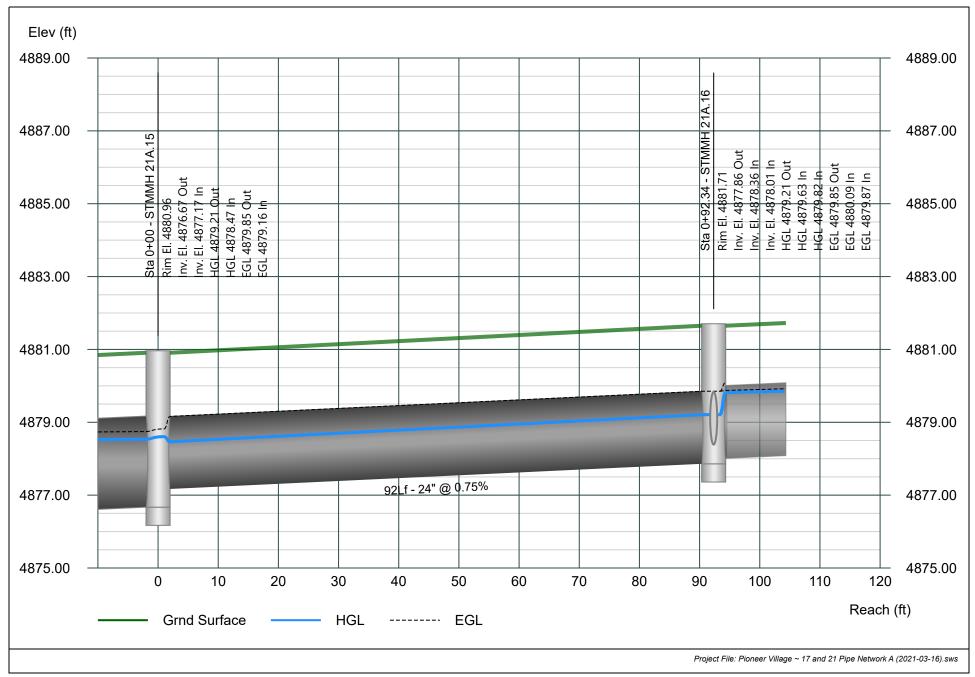
Line 58 - Pipe - (559) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 59 - Pipe - (556) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 60 - Pipe - (560) (PA 21A NETWORK)

A.16

5

- STMMH

Sta 0+00

0

Grnd Surface

Rim El. 4881.71

377.86 Out 378.36 In

Ξ Ξ

HGL

5

10

----- EGL

HGL

5.

48 428

5. 5.

Stormwater Studio 2021 v 3.0.0.24

Elev (ft)

4889.00

4887.00

4885.00

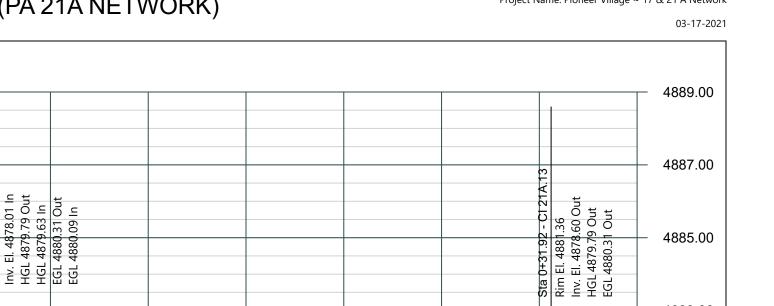
4883.00

4881.00

4879.00

4877.00

4875.00



32Lf - 18" @ 0.75%

15

20

25

Project File: Pioneer Village ~ 17 and 21 Pipe Network A (2021-03-16).sws

30



4883.00

4881.00

4879.00

4877.00

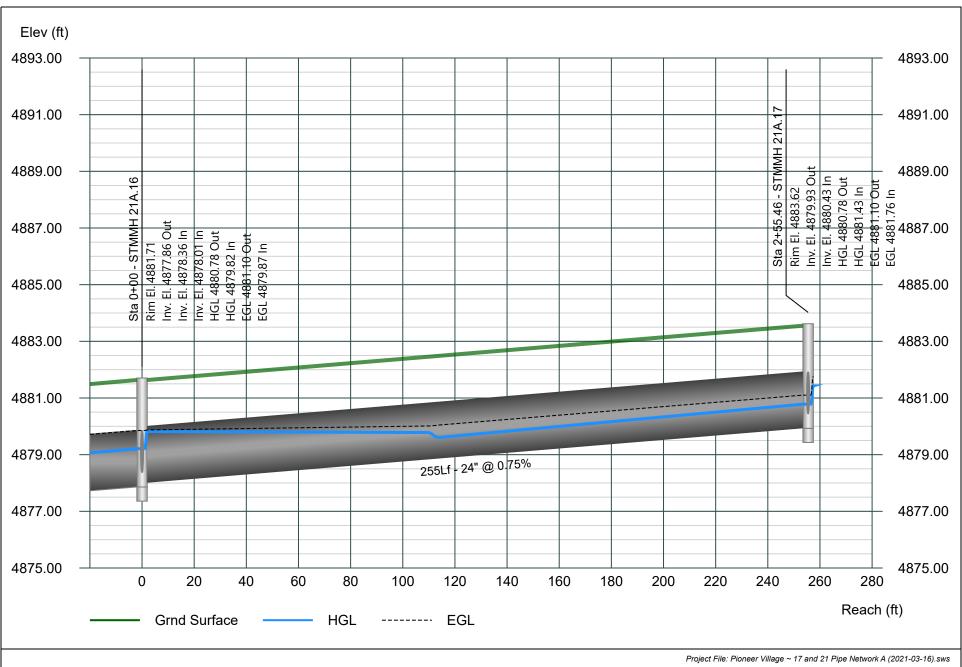
4875.00

35

Reach (ft)

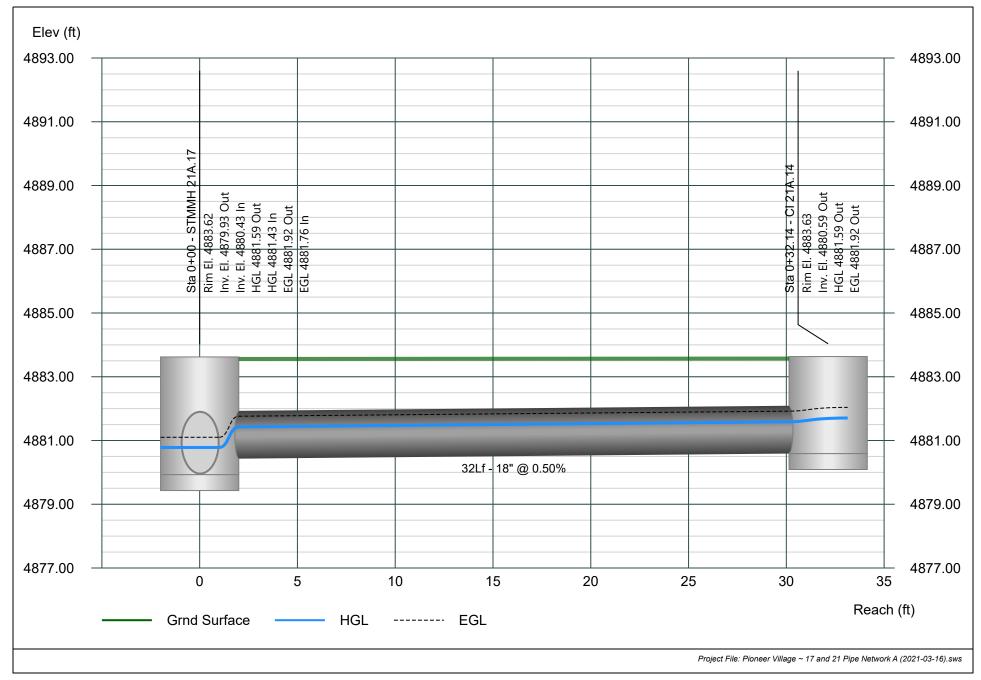
Line 61 - Pipe - (555) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



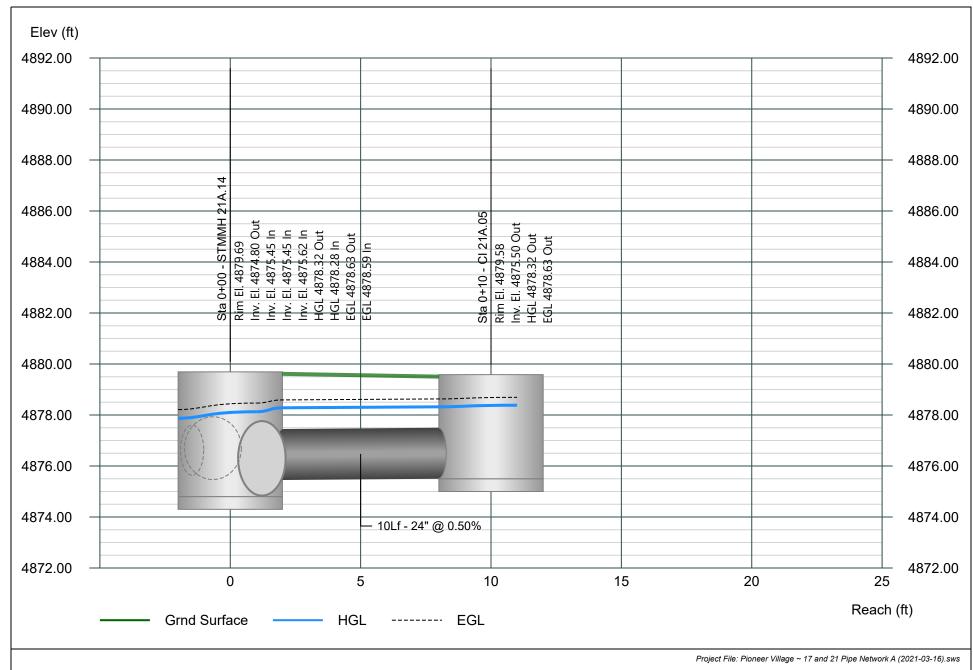
Line 62 - Pipe - (554) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



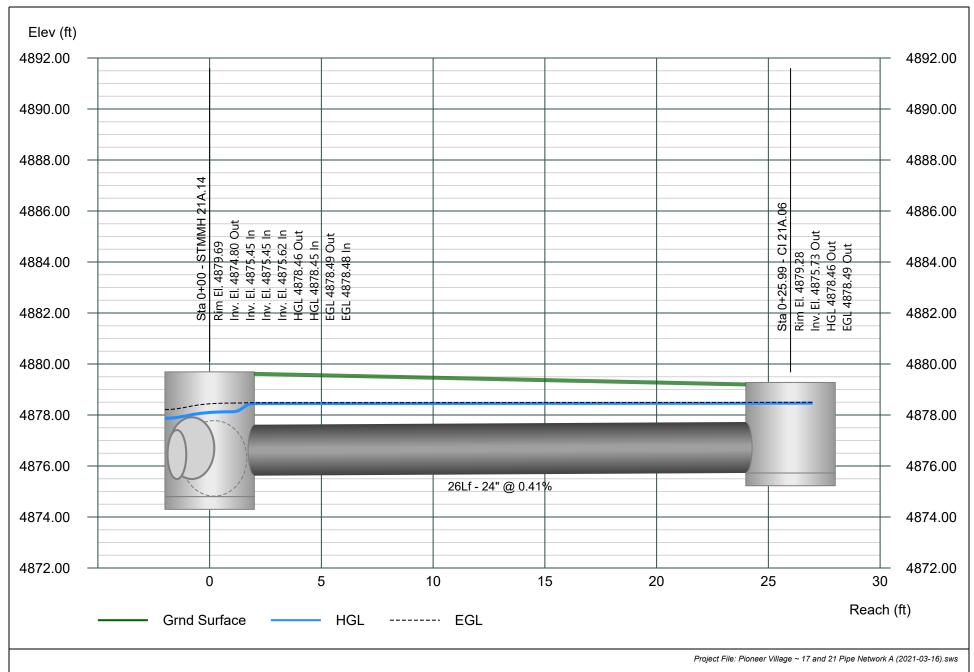
Line 63 - Pipe - (524) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



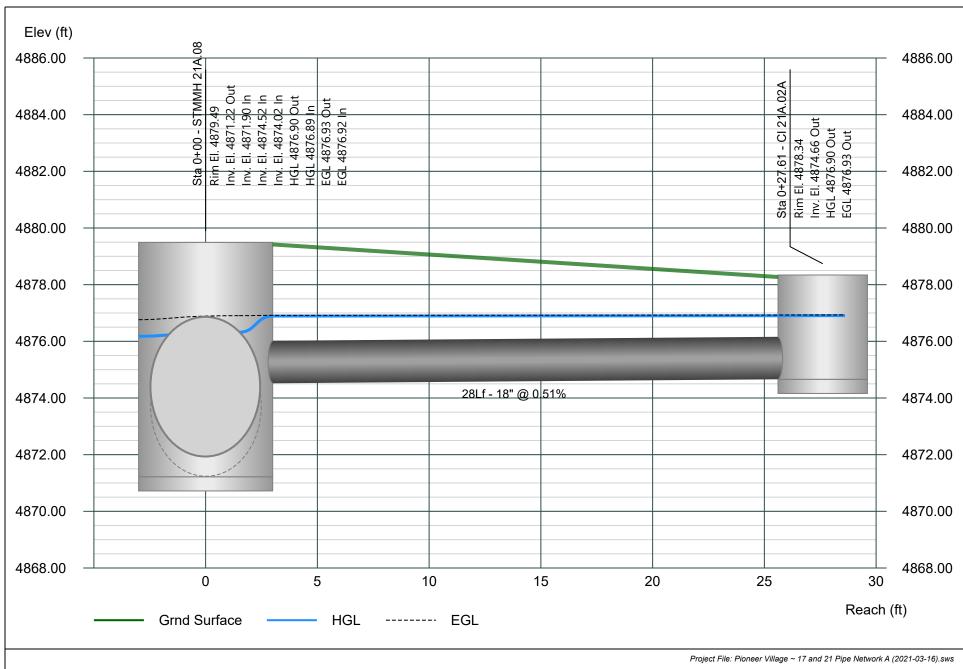
Line 64 - Pipe - (537) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



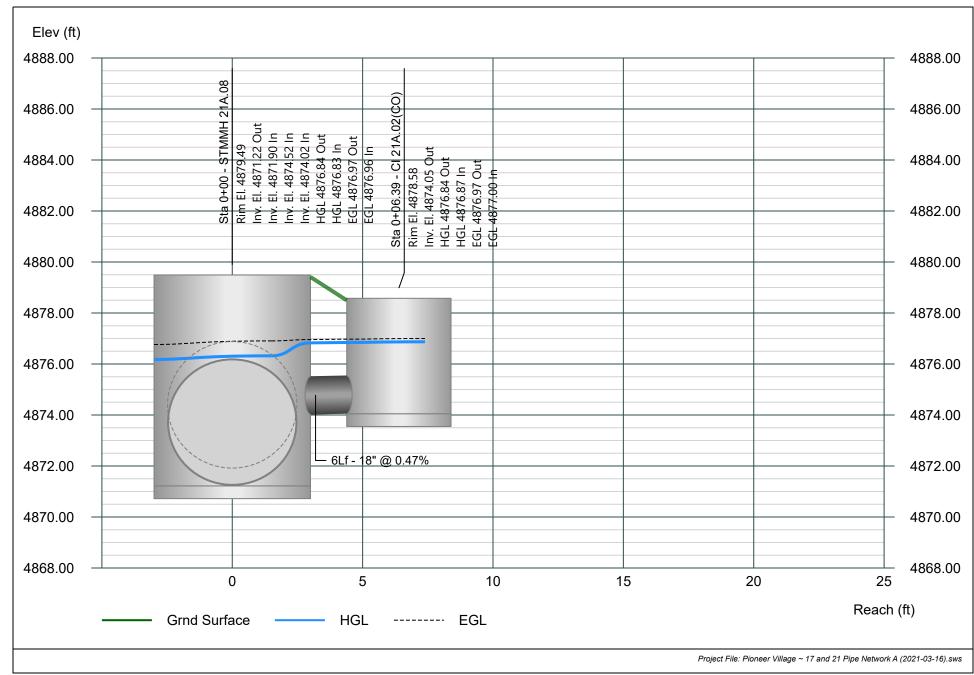
Line 65 - Pipe - (542) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Line 66 - Pipe - (541) (PA 21A NETWORK)

Stormwater Studio 2021 v 3.0.0.24



Storm Sewer Tabulation

	Line ID	Length	Drng	Area	Rational	C >	(A	т	c	Intensity	Total Q	Capacity	Velocity	Lir	ne	Inver	t Elev	HGL	Elev	Surfac	e Elev	Line No
		Ľ	Incr	Total	Rat	Incr	Total	Inlet	Syst	Inte	P	Сар	Vel	Size	Slope	Up	Dn	Up	Dn	Up	Dn	
		(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
Pip	e - (136) (PA 21A NETWOR	t K3)9.13	0.000	0.000	0.00	0.00	0.00	0.0	11.08	8.65	385.60	715.69	6.36	84x108r	0.40	4864.56	4864.00	4871.05	4871.00	4873.40	0.00	1
Pip	e - (135) (PA 21A NETWOR	R 7 ¥.38	0.000	0.000	0.00	0.00	0.00	0.0	10.88	8.70	385.60	718.33	6.12	84x108r	0.40	4865.01	4864.71	4872.00	4871.94	4877.05	4873.40	2
Pip	e - (134) (PA 21A NETWOR	R72.79	0.000	0.000	0.00	0.00	0.00	0.0	10.68	8.76	385.60	714.20	6.12	84x108r	0.40	4865.45	4865.16	4872.44	4872.42	4877.99	4877.05	3
Pip	e - (133) (PA 21A NETWOR	240) 7.38	0.000	0.000	0.00	0.00	0.00	0.0	10.14	8.92	385.60	715.64	6.33	84x108r	0.40	4866.43	4865.60	4872.99	4872.86	4875.62	4877.99	4
Pip	e - (389) (PA 21A NETWOR	K6)5.48	0.000	0.000	0.00	0.00	0.00	0.0	0.04	10.85	9.51	16.00	3.03	24	0.50	4871.76	4871.43	4874.22	4874.10	4876.35	4875.62	5
Pip	e - (390) (PA 21A NETWOR	K7).01	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	9.51	22.58	3.03	24	1.00	4871.98	4871.91	4874.40	4874.39	4875.50	4876.35	6
Pip	e - (388) (PA 21A NETWOR	₩ 2.22	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	19.40	22.62	6.18	24	1.00	4870.85	4870.43	4874.14	4873.83	4875.41	4875.62	7
Pip	e - (132) (PA 21A NETWOR	₩ 8.68	0.000	0.000	0.00	0.00	0.00	0.0	9.99	8.96	356.69	715.81	5.66	84x108r	0.40	4866.63	4866.43	4873.94	4873.89	4875.76	4875.62	8
Pip	e - (400) (PA 21A NETWOR	K7).85	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	11.19	22.85	3.56	24	1.02	4870.21	4870.13	4874.45	4874.43	4875.68	4875.76	9
Pipe -	(130) (1)(0) (PA 21A NETW	8972KG 6	0.000	0.000	0.00	0.00	0.00	0.0	7.82	9.68	345.50	715.62	6.85	84x108r	0.40	4870.20	4866.63	4874.87	4874.27	4879.70	4875.76	10
Pipe - (1	29) (1) (1) (1) (PA 21A NET	V310/B (K)	0.000	0.000	0.00	0.00	0.00	0.0	7.69	9.72	225.13	496.80	4.76	72x96r	0.40	4870.35	4870.20	4876.19	4876.18	4879.13	4879.70	11
Pipe -	(129) (1) (1) (PA 21A NETV	1 0178 K\$9	0.000	0.000	0.00	0.00	0.00	0.0	4.73	10.85	207.23	319.19	7.77	72x72r	0.35	4875.18	4870.35	4878.71	4876.34	4883.63	4879.13	12
Pip	e - (129) (PA 21A NETWOR	#48) 3.73	0.000	0.000	0.00	0.00	0.00	0.0	3.88	10.85	167.05	212.69	9.46	66	0.40	4877.62	4875.68	4881.15	4879.89	4885.38	4883.63	13
Pip	e - (399) (PA 21A NETWOR	⊯4) 1.19	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	5.71	13.73	1.82	24	0.37	4881.12	4880.97	4883.42	4883.40	4885.65	4885.38	14
Pip	e - (128) (PA 21A NETWOR	KS7 .35	0.000	0.000	0.00	0.00	0.00	0.0	3.75	10.85	161.34	238.84	7.04	66	0.51	4878.06	4877.77	4883.03	4882.96	4885.56	4885.38	15
Pip	e - (127) (PA 21A NETWOR	R72.63	0.000	0.000	0.00	0.00	0.00	0.0	1.41	10.85	88.54	183.34	4.51	60	0.50	4878.58	4878.22	4884.18	4884.09	4886.16	4885.56	16
Pipe	- (126)(0) (PA 21A NETWO	fr:140) .55	0.000	0.000	0.00	0.00	0.00	0.0	1.17	10.85	75.44	287.22	11.96	48	4.00	4884.50	4880.08	4887.07	4881.76	4890.43	4886.16	17
Pip	e - (591) (PA 21A NETWOR	19)8.37	0.000	0.000	0.00	0.00	0.00	0.0	0.38	10.85	26.22	55.86	4.73	36	0.70	4886.19	4885.50	4888.12	4888.13	4891.16	4890.43	18
Pip	e - (604) (PA 21A NETWOR	156)9.18	0.000	0.000	0.00	0.00	0.00	0.0	0.14	10.85	8.98	20.16	4.13	24	0.79	4887.66	4887.19	4888.78	4888.82	4891.72	4891.16	19
Pip	e - (589) (PA 21A NETWOR	187.00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	8.98	22.62	3.29	24	1.00	4887.98	4887.71	4889.49	4889.49	4891.45	4891.72	20
Pip	e - (590) (PA 21A NETWOR	K5 12.85	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	17.24	22.66	7.20	24	1.00	4887.72	4887.19	4889.19	4888.57	4891.77	4891.16	21
Pip	e - (594) (PA 21A NETWOR	# €1) 1.64	0.000	0.000	0.00	0.00	0.00	0.0	0.25	10.85	29.47	41.03	8.32	30	1.00	4890.12	4886.00	4891.94	4887.60	4895.14	4890.43	22
	Notes: IDF File = SampleI	DF.idf, F	Return P	eriod = 1	00-yrs.	r = recta	angular e	e = ellipt	ical a = a	arch							Project	File: Pioneer \	/illage ~ 17 aı	nd 21 Pipe Ne	twork A (2021	-03-16).sws

Storm Sewer Tabulation

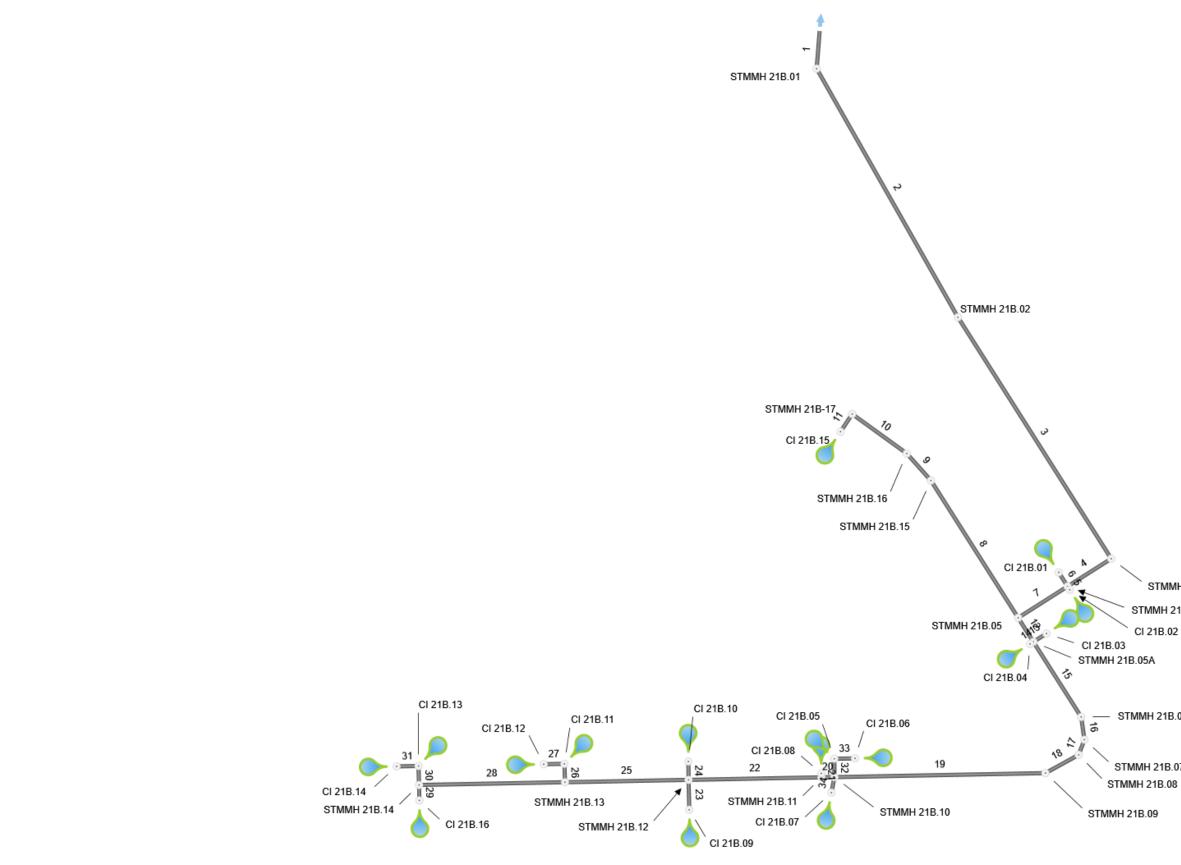
	Line ID	Length	ength	Drng	Area	Rational	CxA		Т	с	Intensity	Total Q	Capacity	Velocity	Line		Invert Elev		HGL Elev		Surface Elev		Line No
		Ľ	Incr	Total	Rat	Incr	Total	Inlet	Syst	Inte	4	Сар	Ve	Size	Slope	Up	Dn	Up	Dn	Up	Dn		
		(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)		
Pip	e - (593) (PA 21A NETWOR	RKS)₿.04	0.000	0.000	0.00	0.00	0.00	0.0	0.15	10.85	29.47	30.96	8.49	27	1.00	4891.05	4890.52	4892.92	4892.33	4895.59	4895.14	23	
Pip	e - (592) (PA 21A NETWOR	RKS)6.08	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	16.35	21.85	4.11	27	0.50	4891.38	4891.20	4893.95	4893.85	4894.90	4895.59	24	
Pip	e - (607) (PA 21A NETWOR	RK27.00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	19.75	22.62	7.59	24	1.00	4886.33	4886.06	4887.91	4887.57	4890.16	4890.43	25	
Pip	e - (605) (PA 21A NETWOR	RK7).00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	13.10	10.88	7.41	18	1.07	4880.33	4880.26	4884.18	4884.08	4885.99	4886.16	26	
Pip	e - (397) (PA 21A NETWOR	RKS)9.51	0.000	0.000	0.00	0.00	0.00	0.0	3.48	10.85	72.80	184.13	3.71	60	0.50	4878.52	4878.22	4884.20	4884.15	4886.73	4885.56	27	
Pip	e - (396) (PA 21A NETWOR	R IA)1.24	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	20.58	22.56	6.55	24	0.99	4881.93	4881.52	4884.44	4884.10	4886.25	4886.73	28	
Pip	e - (598) (PA 21A NETWOR	8 17(2) 3.52	0.000	0.000	0.00	0.00	0.00	0.0	1.43	10.85	52.22	128.50	5.90	48	0.80	4885.31	4879.52	4887.45	4884.34	4892.45	4886.73	29	
Pip	e - (597) (PA 21A NETWOR	8 1K9 8.69	0.000	0.000	0.00	0.00	0.00	0.0	1.06	10.85	52.22	59.66	9.16	36	0.80	4887.90	4886.31	4890.20	4888.52	4893.74	4892.45	30	
Pipe	- (596) (1) (PA 21A NETWO	D RK)22	0.000	0.000	0.00	0.00	0.00	0.0	0.91	10.85	52.22	59.57	7.94	36	0.80	4888.65	4888.05	4891.13	4890.91	4893.96	4893.74	31	
Pip	e - (603) (PA 21A NETWOR	RK27.00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	24.09	41.01	4.91	30	1.00	4889.42	4889.15	4893.12	4893.03	4893.47	4893.96	32	
Pip	e - (596) (PA 21A NETWOR	R I4)5.10	0.000	0.000	0.00	0.00	0.00	0.0	0.72	10.85	28.13	59.61	3.98	36	0.80	4889.16	4888.80	4893.19	4893.11	4894.28	4893.96	33	
Pipe	- (595) (1) (PA 21A NETWO	RB (26	0.000	0.000	0.00	0.00	0.00	0.0	0.43	10.85	28.13	66.57	3.98	36	1.00	4890.00	4889.31	4893.51	4893.38	4894.86	4894.28	34	
Pip	e - (595) (PA 21A NETWOR	RK677.54	0.000	0.000	0.00	0.00	0.00	0.0	0.19	10.85	12.97	31.98	4.75	24	2.00	4892.35	4891.00	4893.78	4893.71	4896.33	4894.86	35	
Pip	e - (602) (PA 21A NETWOR	RK27.00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	7.39	22.62	2.35	24	1.00	4892.77	4892.50	4894.91	4894.88	4896.07	4896.33	36	
Pip	e - (601) (PA 21A NETWOR	RK7).00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	5.58	22.59	1.78	24	1.00	4892.57	4892.50	4894.91	4894.90	4896.06	4896.33	37	
Pip	e - (599) (PA 21A NETWOR	RK9)8.62	0.000	0.000	0.00	0.00	0.00	0.0	0.02	10.85	15.16	30.34	5.69	24	1.80	4892.78	4891.00	4894.15	4893.65	4896.55	4894.86	38	
Pip	e - (600) (PA 21A NETWOR	RK7).00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	15.16	22.59	6.60	24	1.00	4893.00	4892.93	4894.39	4894.29	4896.29	4896.55	39	
Pip	e - (566) (PA 21A NETWOR	RK8)8.98	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	21.26	22.61	6.77	24	1.00	4878.57	4878.18	4880.62	4880.28	4883.44	4883.63	40	
Pip	e - (581) (PA 21A NETWOR	RK7).00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	18.92	22.59	6.02	24	1.00	4878.25	4878.18	4880.42	4880.37	4883.48	4883.63	41	
Pip	e - (606) (PA 21A NETWOR	RKS)9.00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	17.90	22.62	5.70	24	1.00	4873.74	4873.35	4876.59	4876.34	4878.87	4879.13	42	
Pipe	- (526) (1) (PA 21A NETWO	RB .23	0.000	0.000	0.00	0.00	0.00	0.0	3.08	10.85	120.37	225.75	6.14	60	0.75	4871.22	4870.70	4876.18	4876.04	4879.49	4879.70	43	
Pip	e - (526) (PA 21A NETWOR	R K4) 4.11	0.000	0.000	0.00	0.00	0.00	0.0	2.70	10.85	113.10	184.14	6.27	60	0.50	4872.62	4871.90	4876.69	4876.56	4879.90	4879.49	44	
	Notes: IDF File = Samplel	DF.idf, F	Return P	eriod = 1	00-yrs.												Project I	File: Pioneer \	/illage ~ 17 ar	nd 21 Pipe Ne	twork A (2021	-03-16).sws	

Storm Sewer Tabulation

	Line ID	Length	Drng	Area	Rational	C	٢A	т	c	Intensity	Total Q	Capacity	Velocity	Li	ne	Inver	t Elev	HGL	Elev	Surfac	e Elev	Line No
		Ľ	Incr	Total	Rat	Incr	Total	Inlet	Syst	Inte	4	Cap	Vel	Size	Slope	Up	Dn	Up	Dn	Up	Dn	
		(ft)	(ac)	(ac)	(C)			(min)	(min)	(in/hr)	(cfs)	(cfs)	(ft/s)	(in)	(%)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
Pip	e - (534) (PA 21A NETWOF	RKS)0.07	0.000	0.000	0.00	0.00	0.00	0.0	2.36	10.85	80.01	164.63	4.08	60	0.40	4872.89	4872.77	4877.81	4877.78	4879.64	4879.90	45
Pip	e - (533) (PA 21A NETWOF	280) 5.48	0.000	0.000	0.00	0.00	0.00	0.0	1.69	10.85	60.70	124.36	5.18	48	0.75	4874.93	4873.39	4878.20	4877.94	4881.29	4879.64	46
Pip	e - (548) (PA 21A NETWOF	285) 5.00	0.000	0.000	0.00	0.00	0.00	0.0	0.91	10.85	43.66	124.31	5.43	48	0.75	4877.09	4875.18	4879.04	4878.73	4883.20	4881.29	47
Pipe -	(546) (2) (1) (PA 21A NETV	/ 23F5k0)0	0.000	0.000	0.00	0.00	0.00	0.0	0.29	10.85	21.96	35.50	7.14	30	0.75	4880.50	4878.59	4882.07	4880.03	4885.11	4883.20	48
Pip	e - (545) (PA 21A NETWOF	RKS)2.06	0.000	0.000	0.00	0.00	0.00	0.0	0.20	10.85	21.96	28.99	6.47	30	0.50	4880.81	4880.65	4882.44	4882.29	4885.00	4885.11	49
Pip	e - (527) (PA 21A NETWOF	RKS)6.17	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	14.59	28.95	2.97	30	0.50	4881.14	4880.96	4883.76	4883.72	4884.96	4885.00	50
Pip	e - (549) (PA 21A NETWOF	RKS)2.10	0.000	0.000	0.00	0.00	0.00	0.0	0.13	10.85	21.70	23.82	6.79	27	0.59	4879.03	4878.84	4880.72	4880.53	4882.88	4883.20	51
Pip	e - (529) (PA 21A NETWOF	RKS)6.17	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	14.45	20.24	4.60	24	0.80	4879.57	4879.28	4882.22	4882.08	4883.07	4882.88	52
Pipe	- (532)(0) (PA 21A NETWO	14 (RS122)	0.000	0.000	0.00	0.00	0.00	0.0	0.11	10.85	17.04	14.32	5.42	24	0.40	4877.25	4877.12	4879.30	4879.12	4881.32	4881.29	53
Pip	e - (531) (PA 21A NETWOF	RKS)6.17	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	9.36	7.41	5.30	18	0.50	4877.93	4877.75	4880.04	4879.75	4881.11	4881.32	54
Pip	e - (536) (PA 21A NETWOF	RK27.00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	9.53	16.27	3.03	24	0.52	4875.03	4874.89	4878.12	4878.08	4879.21	4879.64	55
Pip	e - (535) (PA 21A NETWOF	RK9.17	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	9.78	16.75	3.11	24	0.55	4875.10	4875.05	4878.09	4878.07	4880.07	4879.64	56
Pip	e - (525) (PA 21A NETWOF	RKS)6.86	0.000	0.000	0.00	0.00	0.00	0.0	2.49	10.85	33.09	46.78	4.68	36	0.49	4874.80	4874.52	4877.87	4877.73	4879.69	4879.90	57
Pip	e - (559) (PA 21A NETWOF	R K6) 3.20	0.000	0.000	0.00	0.00	0.00	0.0	1.68	10.85	14.50	35.46	3.32	30	0.75	4876.67	4875.45	4878.53	4878.39	4880.96	4879.69	58
Pip	e - (556) (PA 21A NETWOF	RK9)2.34	0.000	0.000	0.00	0.00	0.00	0.0	1.43	10.85	14.50	19.55	6.59	24	0.75	4877.86	4877.17	4879.21	4878.47	4881.71	4880.96	59
Pip	e - (560) (PA 21A NETWOF	RKS)1.92	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	8.72	9.11	5.63	18	0.75	4878.60	4878.36	4879.79	4879.63	4881.36	4881.71	60
Pip	e - (555) (PA 21A NETWOF	2 83 5.46	0.000	0.000	0.00	0.00	0.00	0.0	0.12	10.85	5.78	19.61	3.24	24	0.75	4879.93	4878.01	4880.78	4879.82	4883.62	4881.71	61
Pip	e - (554) (PA 21A NETWOF	RKS)2.14	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	5.78	7.40	4.63	18	0.50	4880.59	4880.43	4881.59	4881.43	4883.63	4883.62	62
Pip	e - (524) (PA 21A NETWOF	RM()0.00	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	14.02	15.96	4.46	24	0.50	4875.50	4875.45	4878.32	4878.28	4879.58	4879.69	63
Pip	e - (537) (PA 21A NETWOF	RI\$5.99	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	4.57	14.44	1.45	24	0.41	4875.73	4875.62	4878.46	4878.45	4879.28	4879.69	64
Pip	e - (542) (PA 21A NETWOF	RK27.61	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	2.17	7.48	1.23	18	0.51	4874.66	4874.52	4876.90	4876.89	4878.34	4879.49	65
Pip	e - (541) (PA 21A NETWOF	RK6).39	0.000	0.000	0.00	0.00	0.00	0.0	0.00	10.85	5.10	7.17	2.89	18	0.47	4874.05	4874.02	4876.84	4876.83	4878.58	4879.49	66
	Notes: IDF File = SampleI	DF.idf, F	Return P	eriod = 1	100-yrs.												Project	File: Pioneer \	/illage ~ 17 ai	nd 21 Pipe Ne	twork A (2021	-03-16).sws

Plan View

Stormwater Studio 2021 v 3.0.0.24



03-15-2021

STMMH 2

STMMH 21B.(

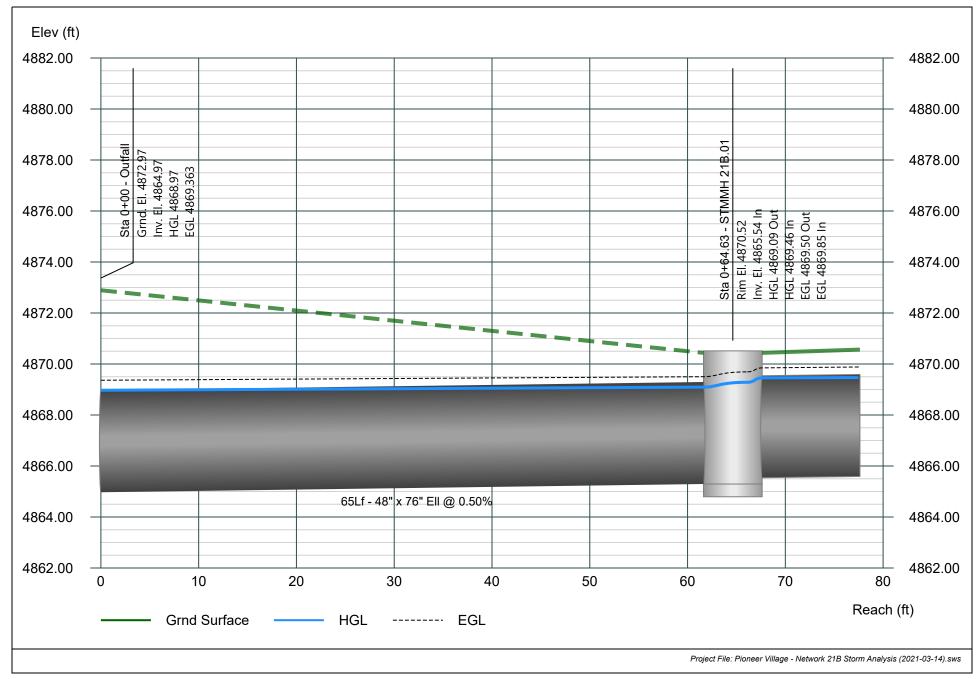
CI 21B.02

— STMMH 21B.06

STMMH 21B.07

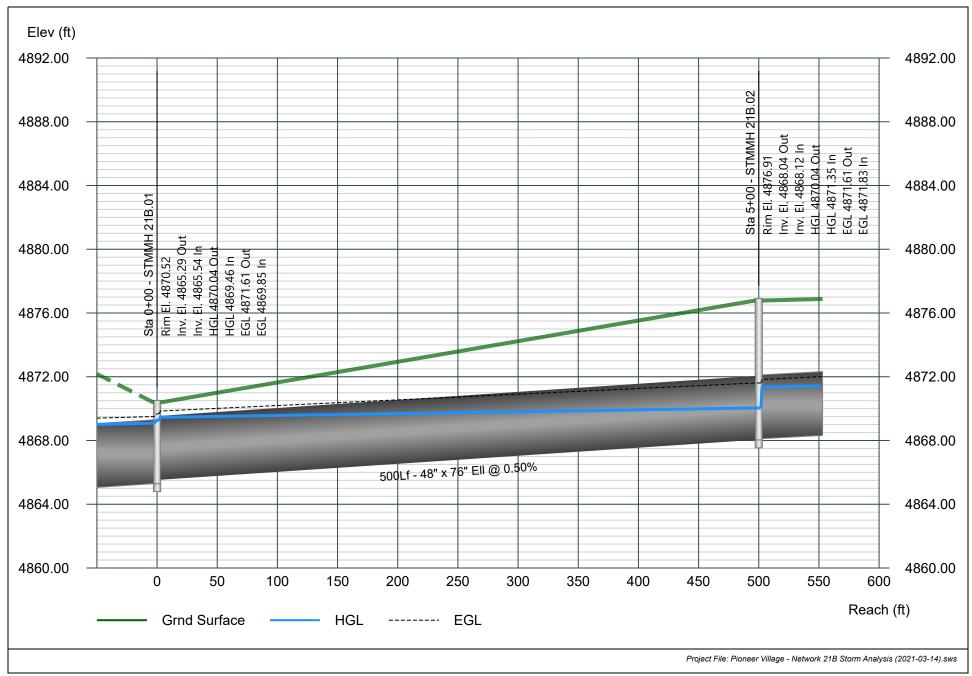
Line 1 - Pipe - (500)

Stormwater Studio 2021 v 3.0.0.24



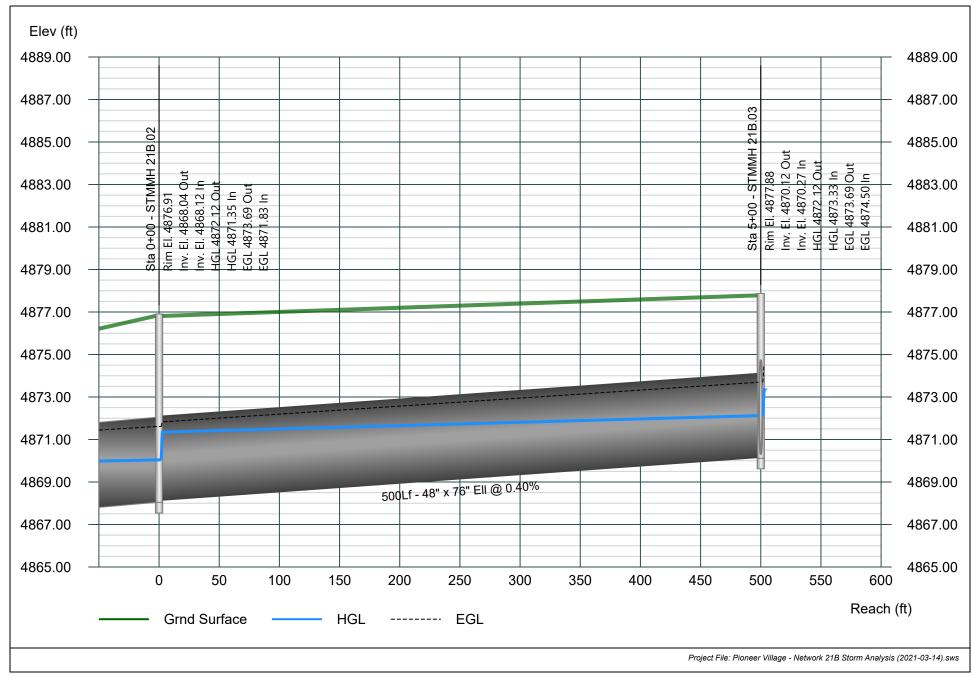
Line 2 - Pipe - (499) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



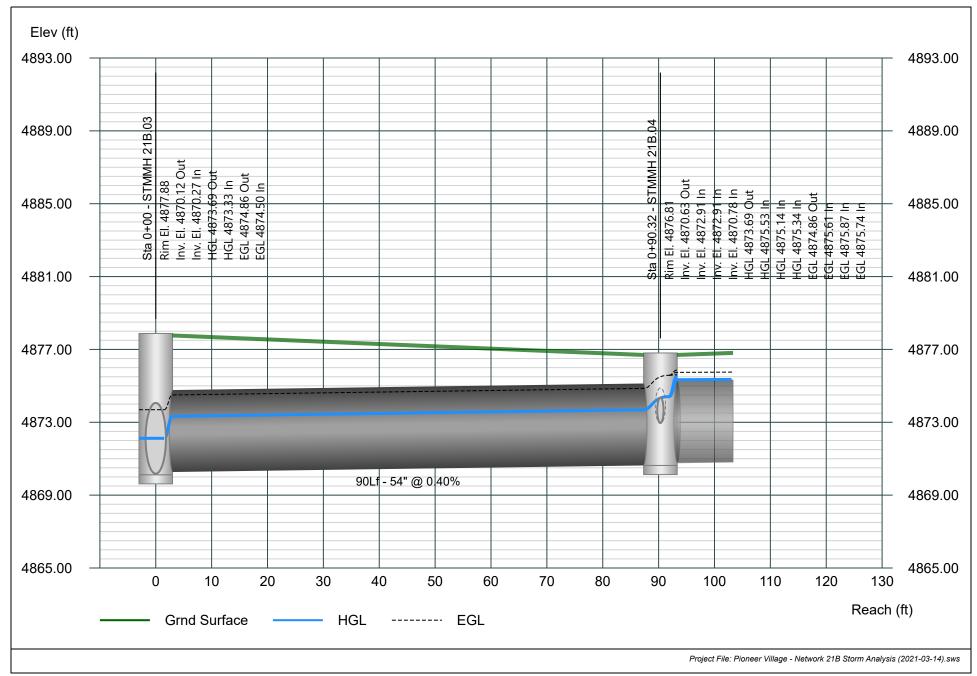
Line 3 - Pipe - (498) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



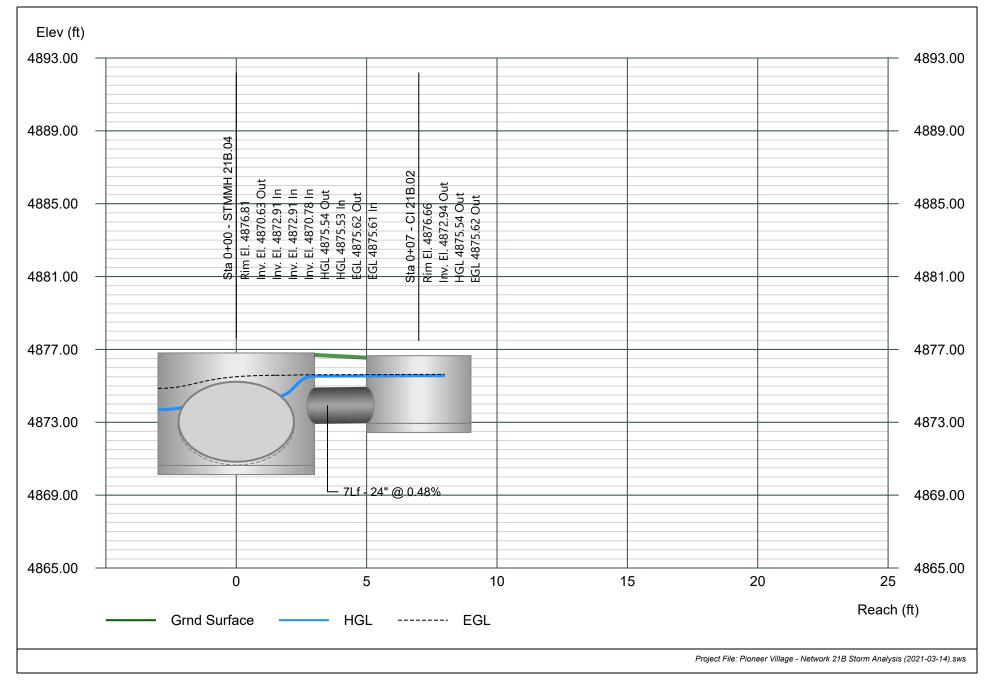
Line 4 - Pipe - (497) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



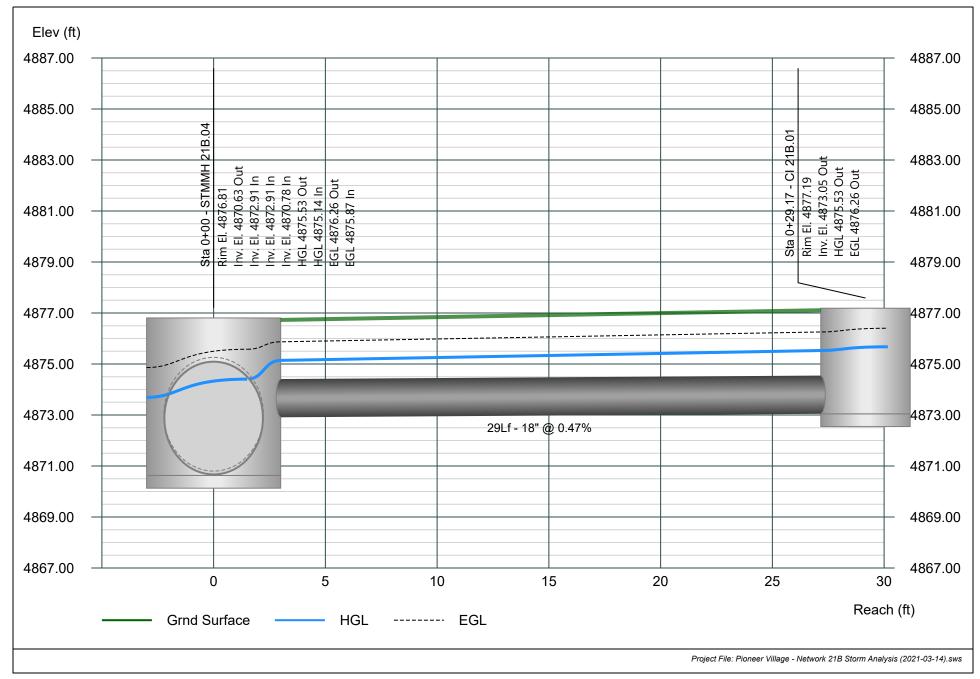
Line 5 - Pipe - (515) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



Line 6 - Pipe - (513) (Storm Sewer - 21 B Network)

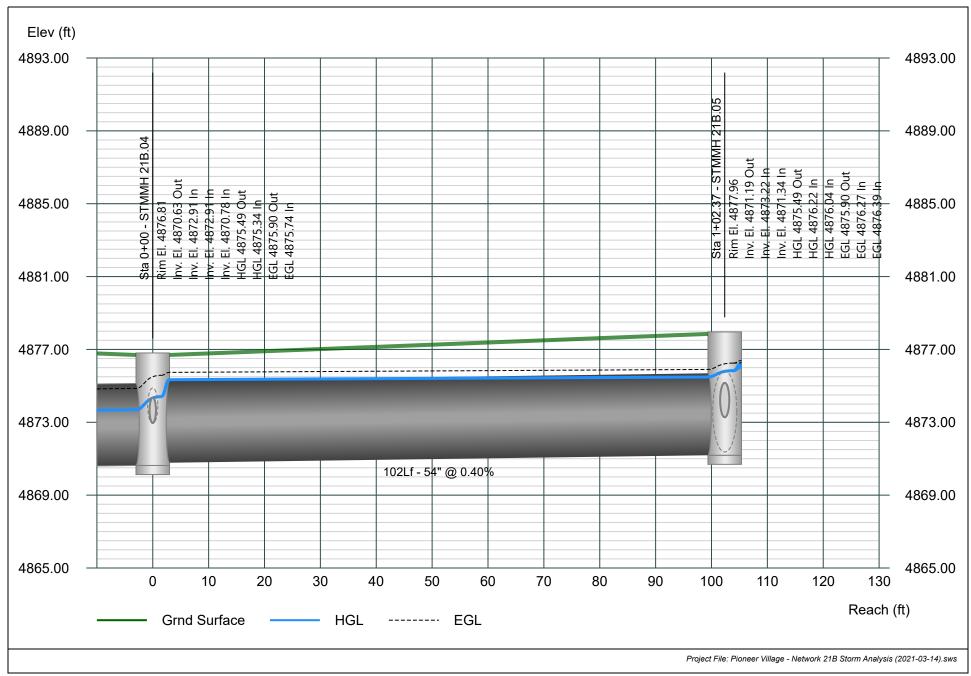
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village Storm Network 21B

Line 7 - Pipe - (496) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24

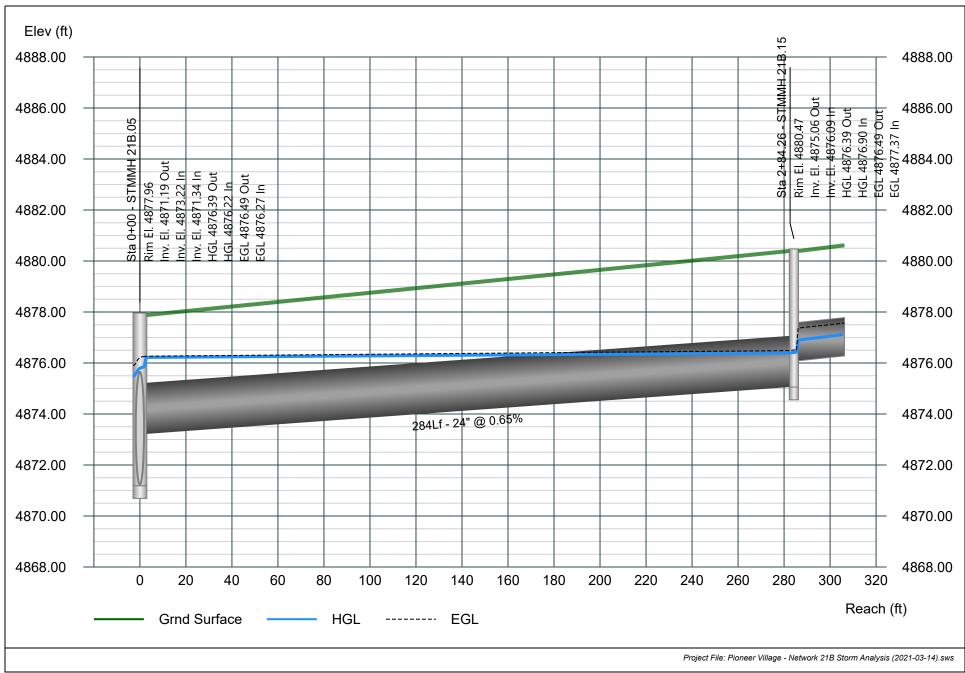


Line 8 - Pipe - (507) (1) (Storm Sewer - 21 B Network)

Project Name: Pioneer Village Storm Network 21B

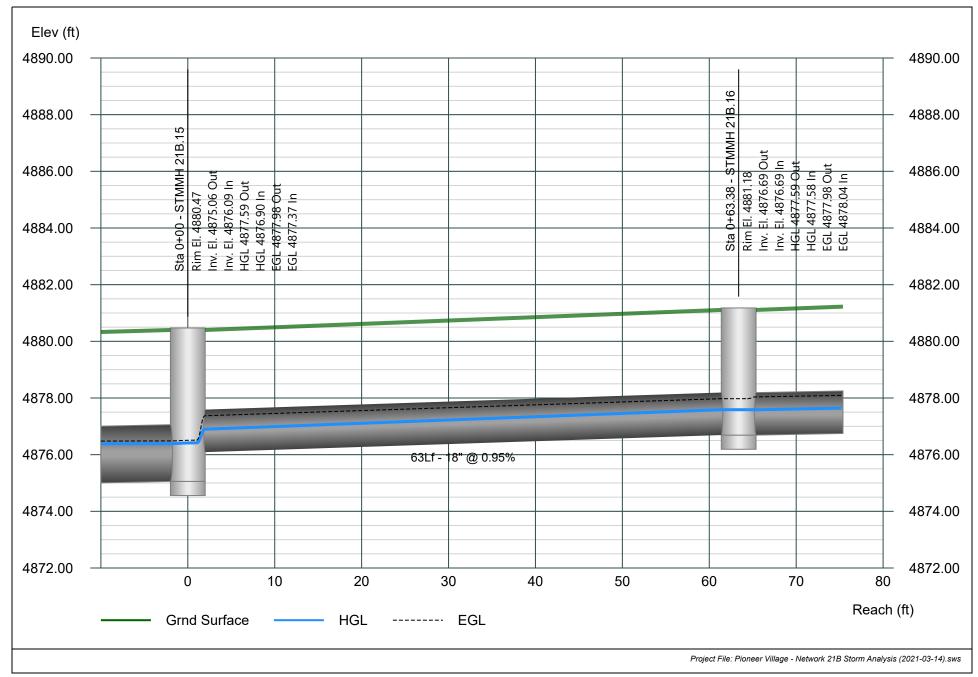
03-15-2021

Stormwater Studio 2021 v 3.0.0.24



Line 9 - Pipe - (506) (Storm Sewer - 21 B Network)

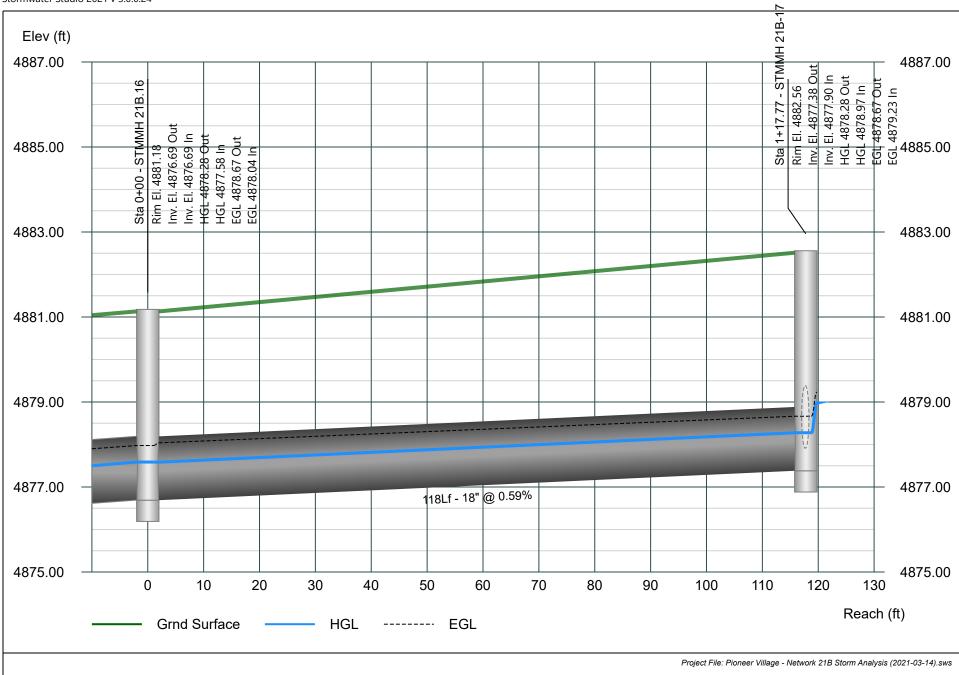
Stormwater Studio 2021 v 3.0.0.24



Line 10 - Pipe - (505) (Storm Sewer - 21 B Network)

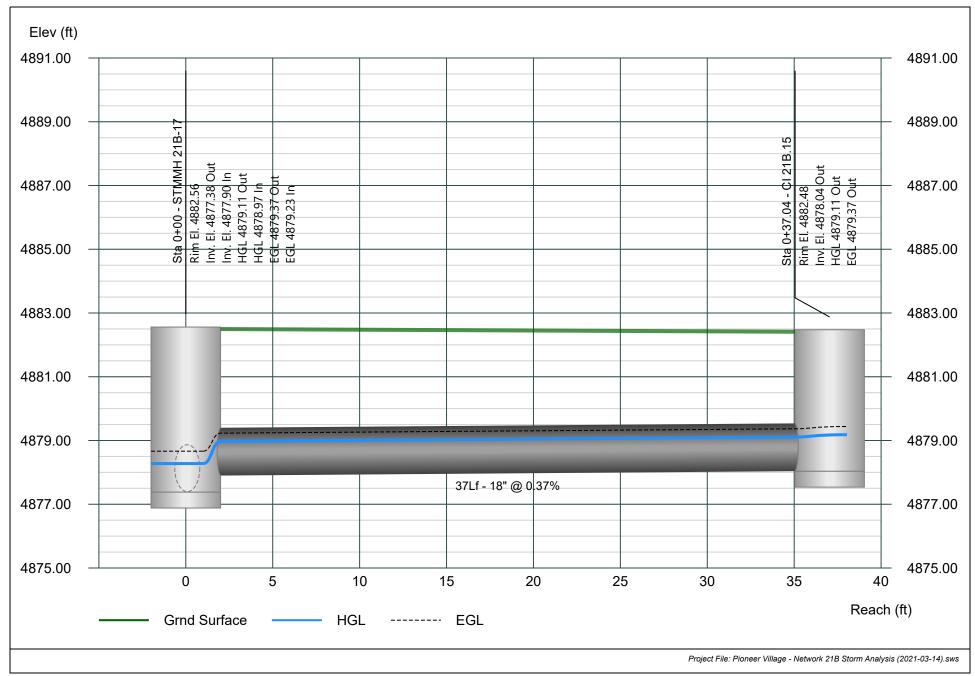
03-15-2021

Stormwater Studio 2021 v 3.0.0.24



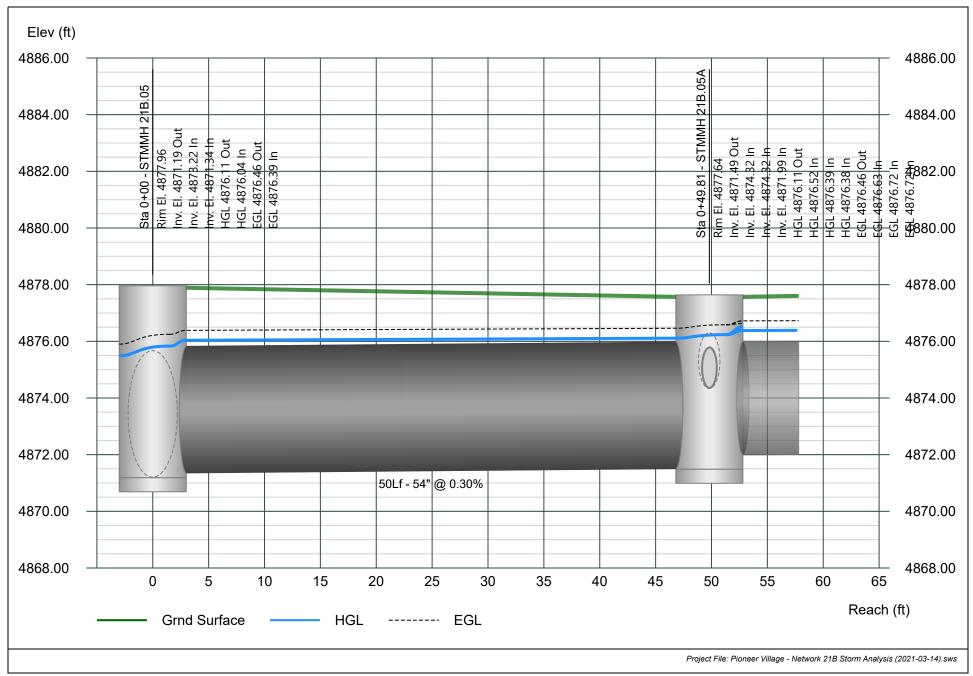
Line 11 - Pipe - (503) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



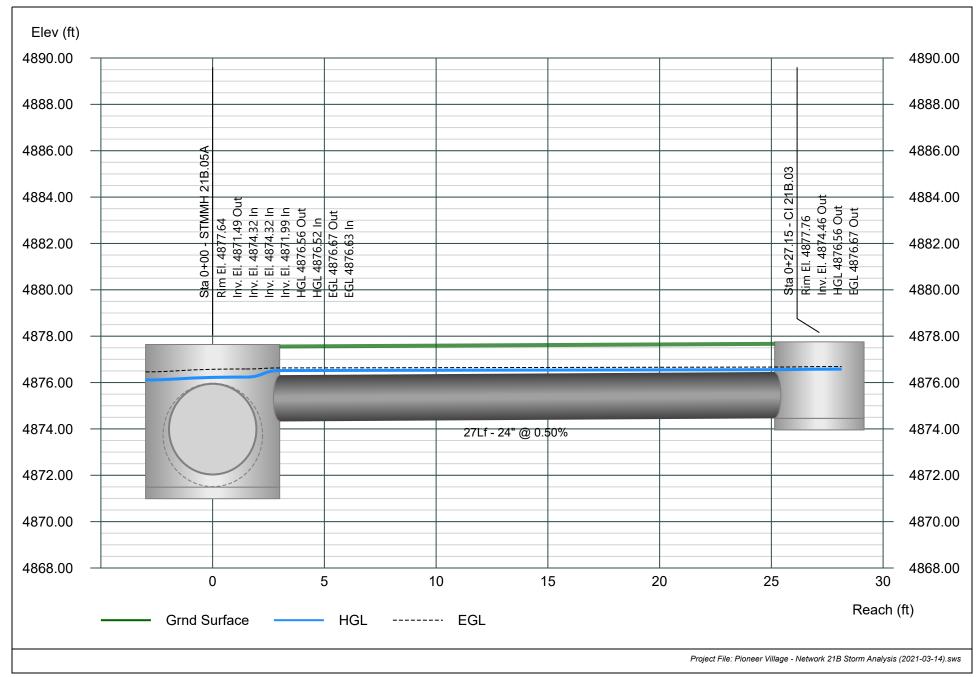
Line 12 - Pipe - (510) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



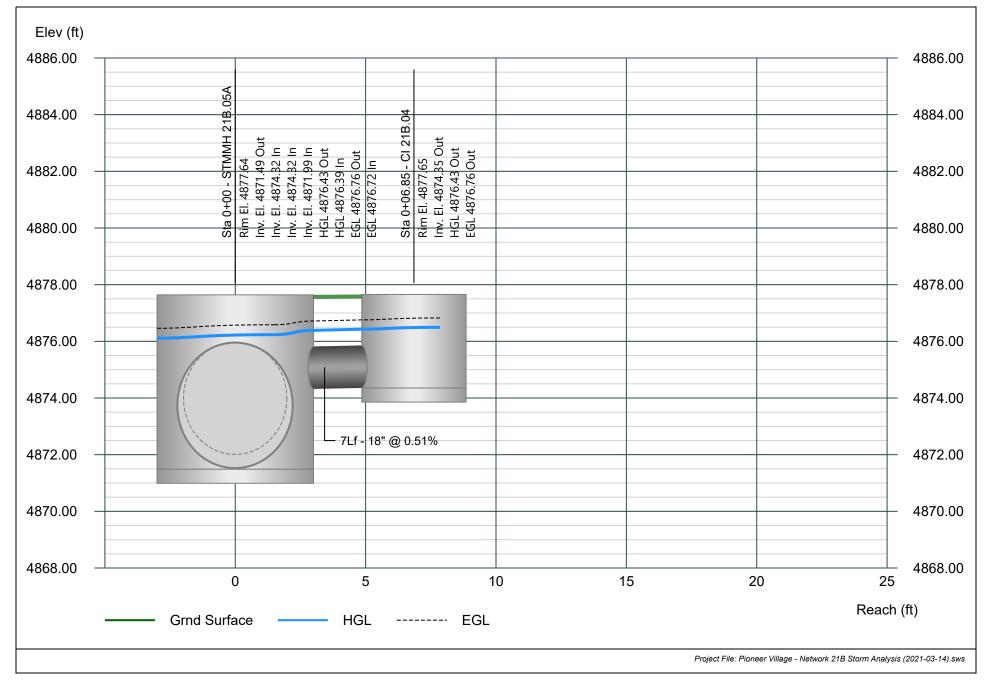
Line 13 - Pipe - (565) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



Line 14 - Pipe - (511) (Storm Sewer - 21 B Network)

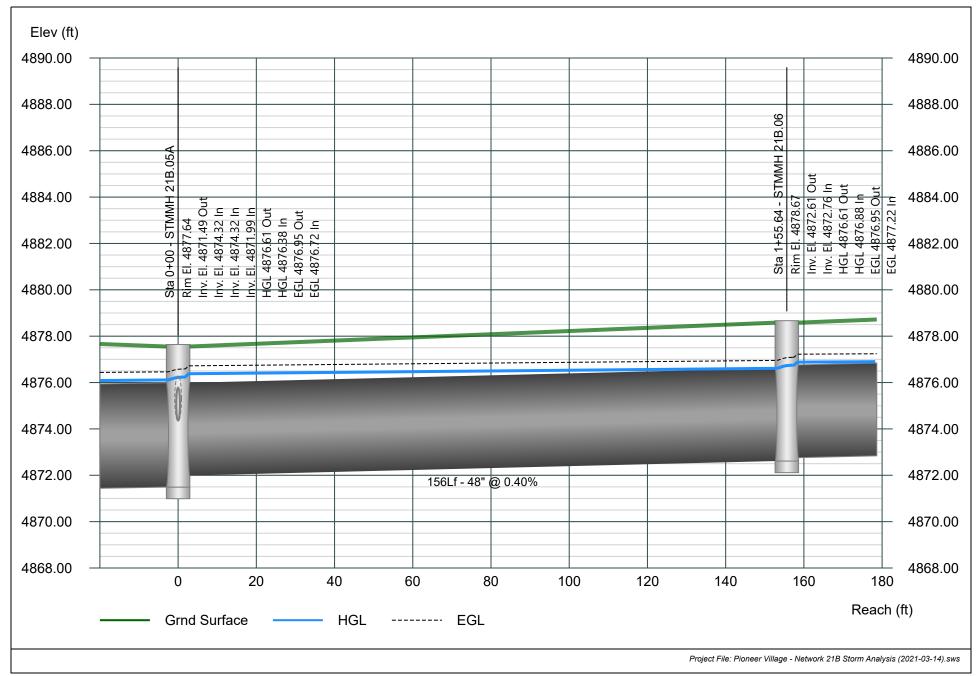
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village Storm Network 21B

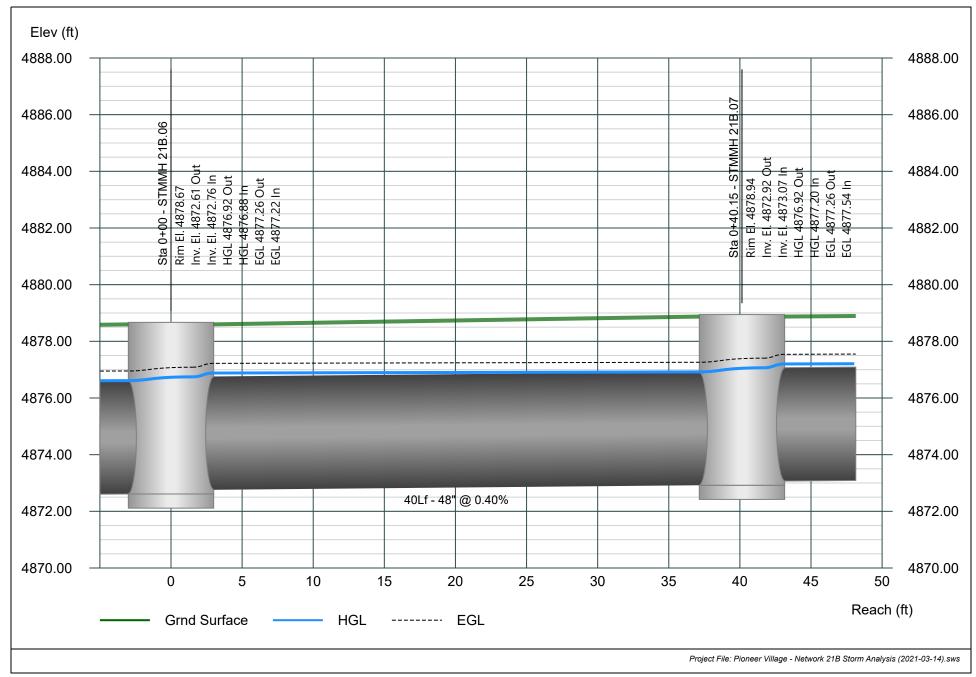
Line 15 - Pipe - (564) (1) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



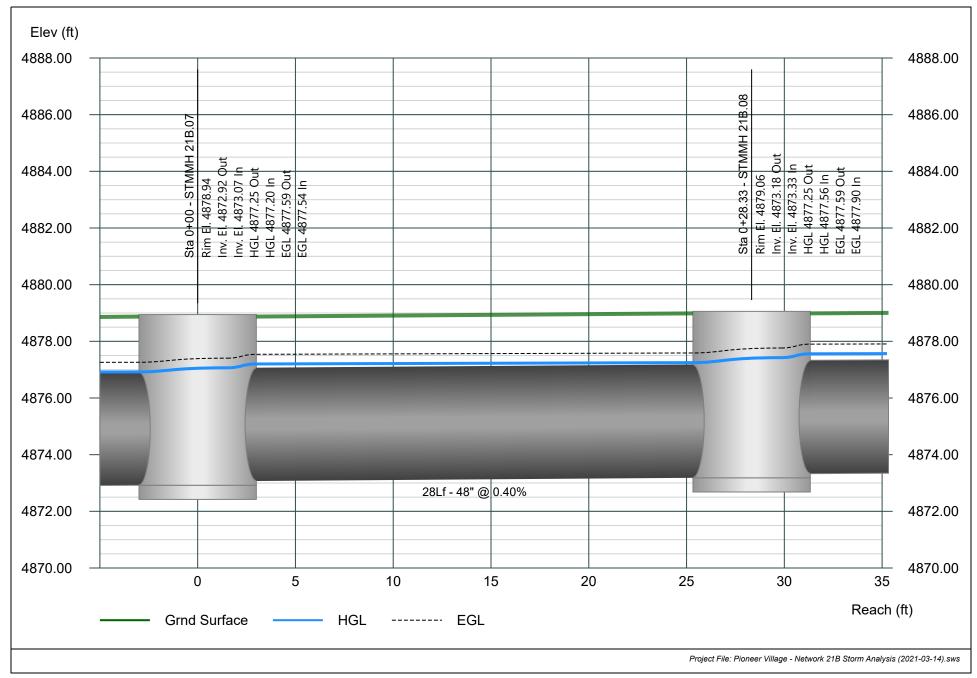
Line 16 - Pipe - (564) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



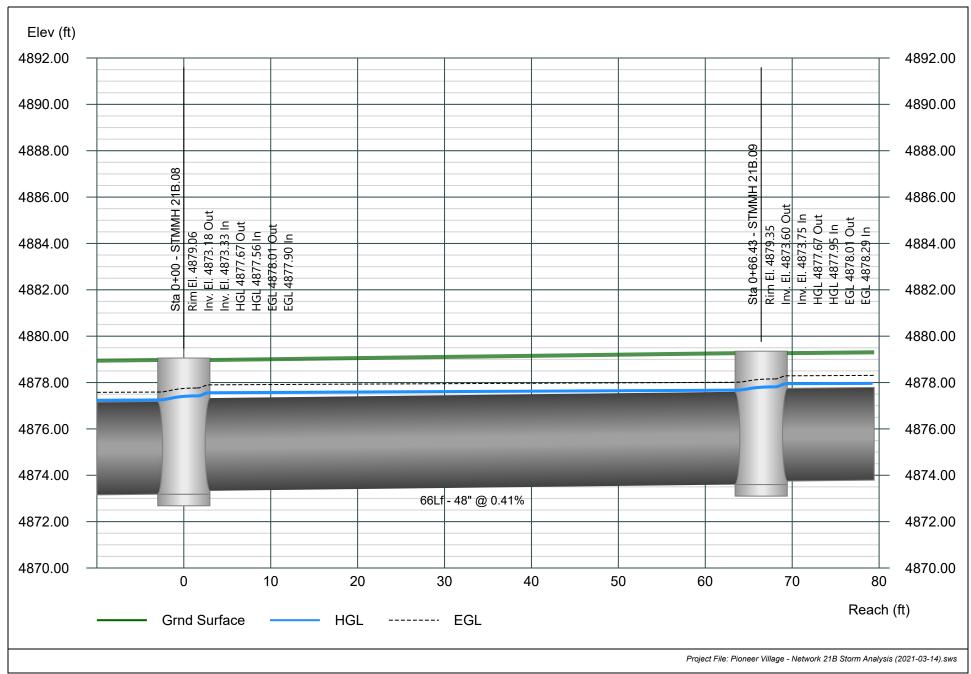
Line 17 - Pipe - (493) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



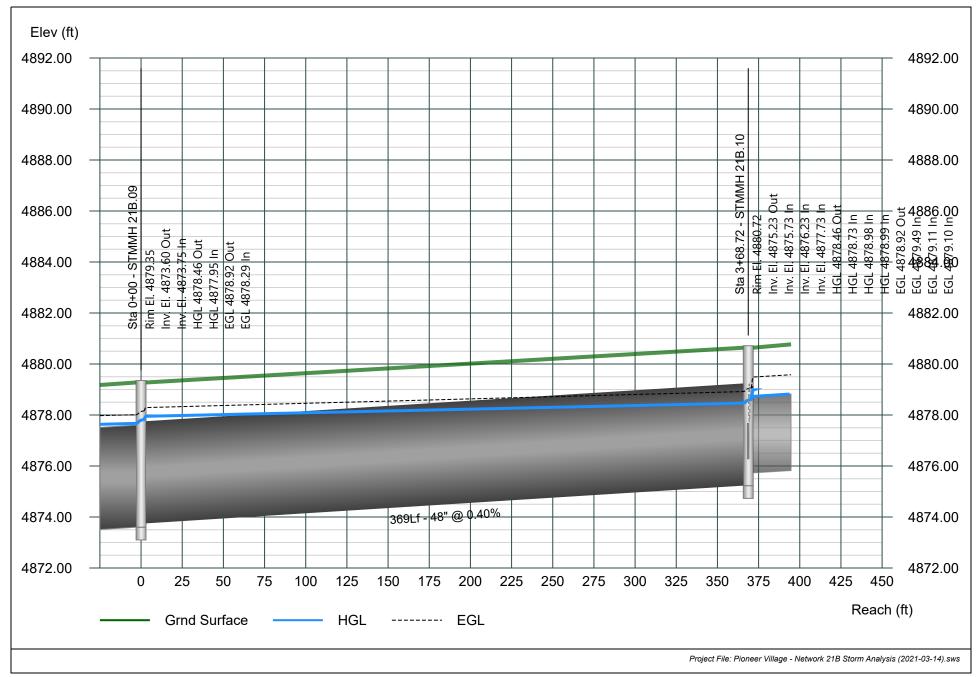
Line 18 - Pipe - (492) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



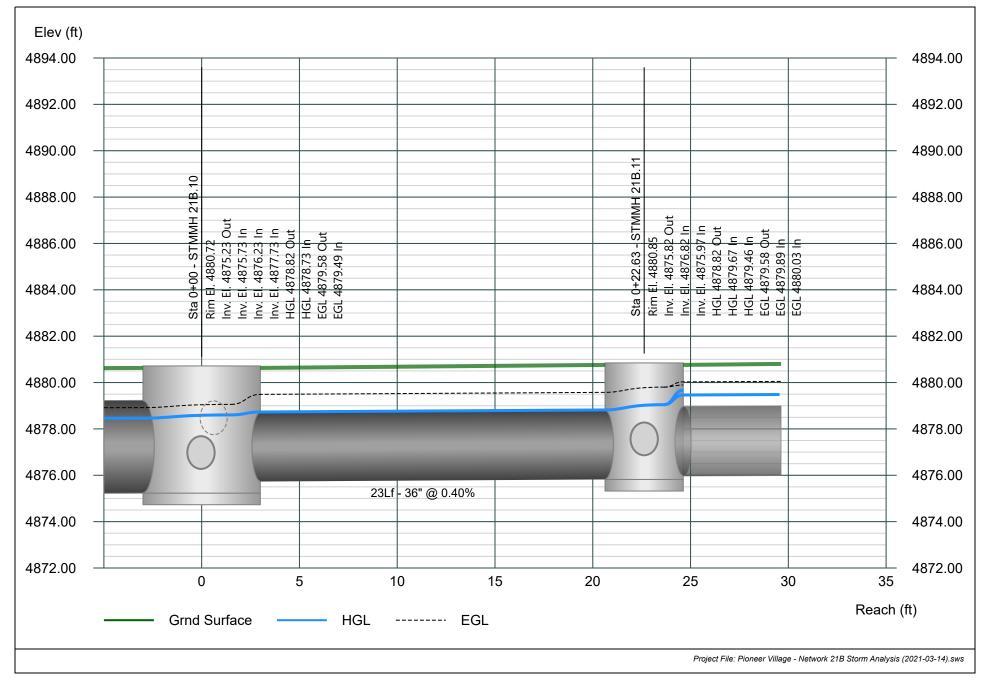
Line 19 - Pipe - (571) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



Line 20 - Pipe - (570) (Storm Sewer - 21 B Network)

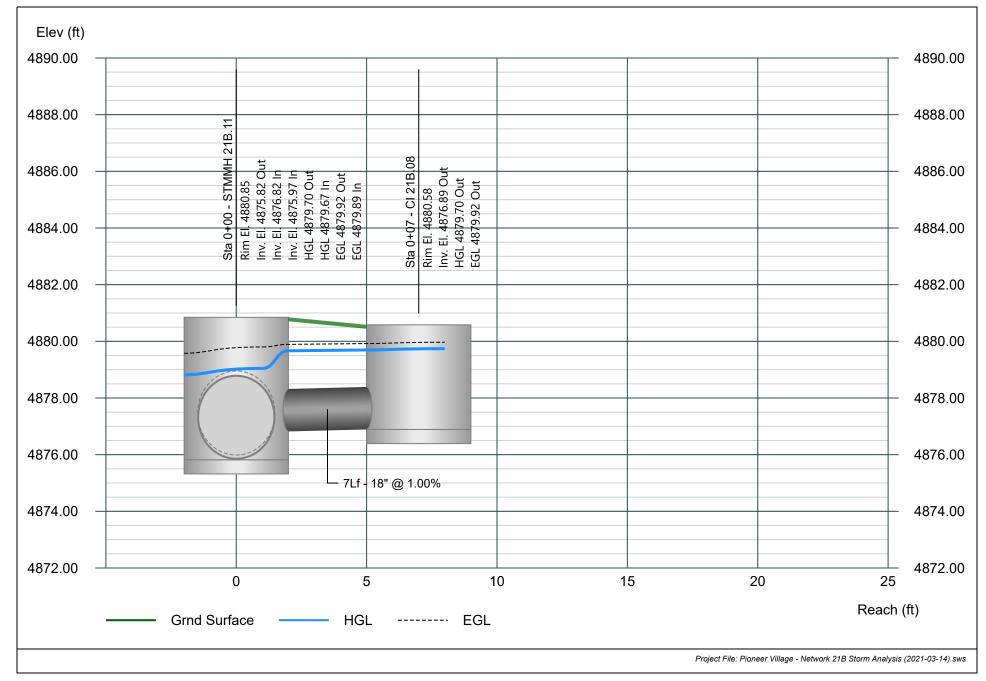
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village Storm Network 21B

Line 21 - Pipe - (518) (Storm Sewer - 21 B Network)

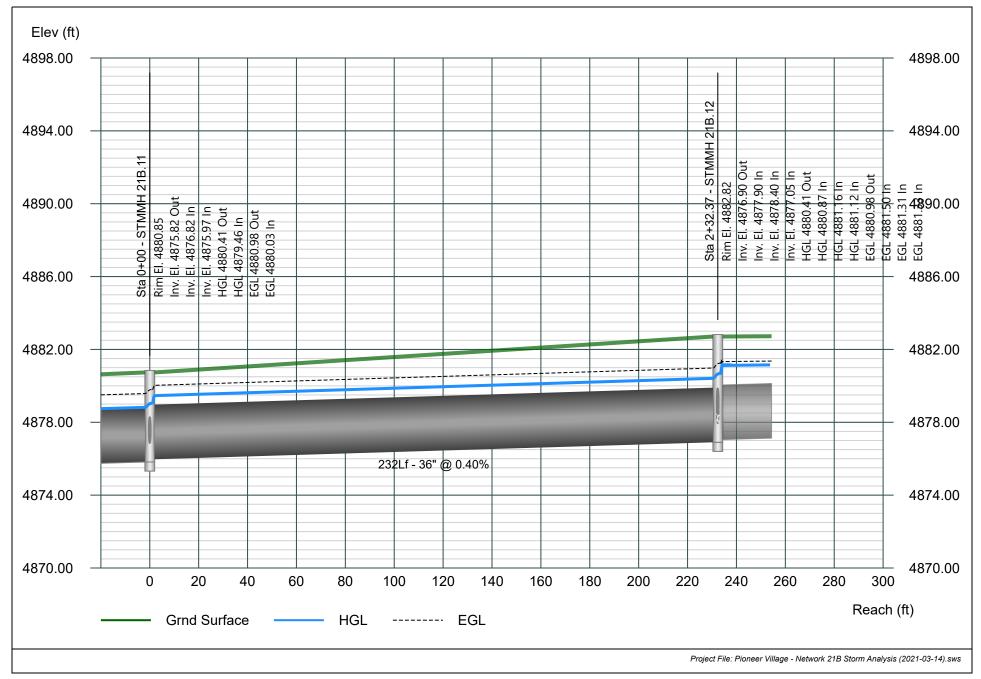
Stormwater Studio 2021 v 3.0.0.24



Project Name: Pioneer Village Storm Network 21B

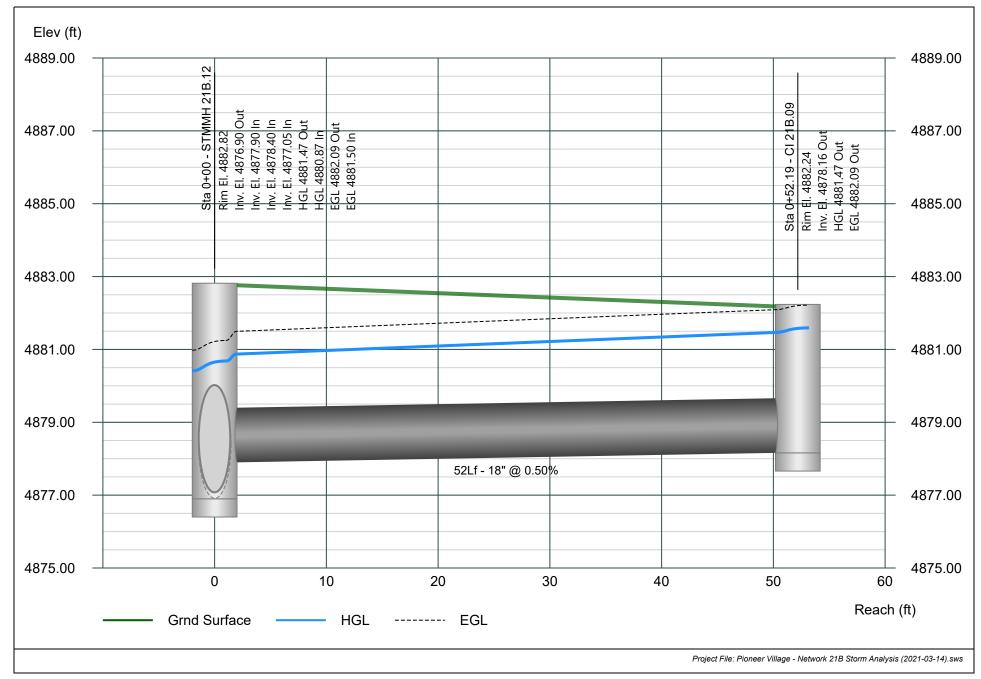
Line 22 - Pipe - (488) (1) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



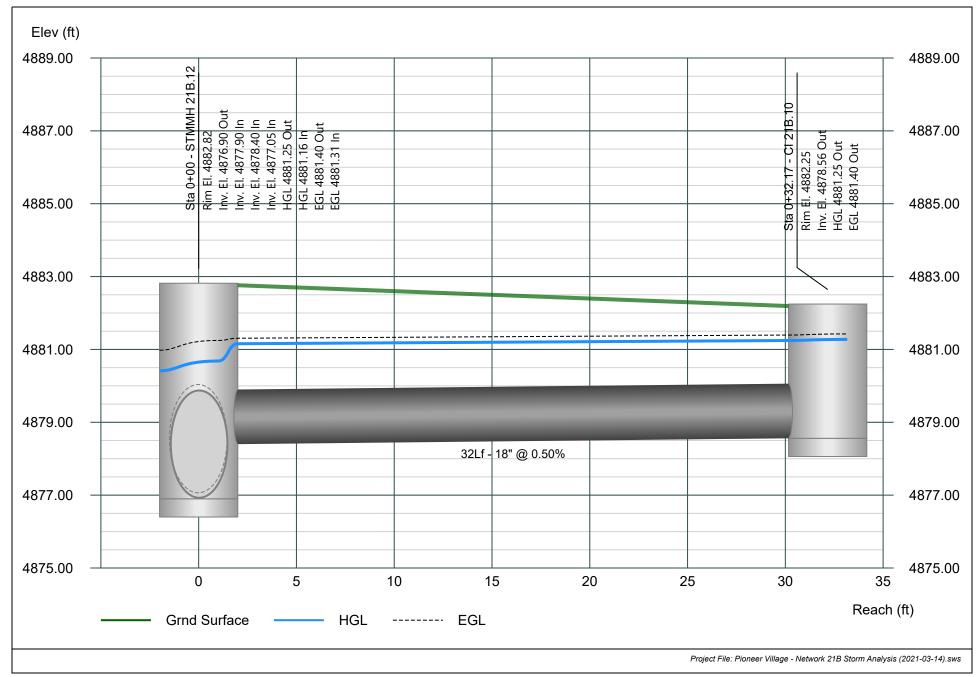
Line 23 - Pipe - (585) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24

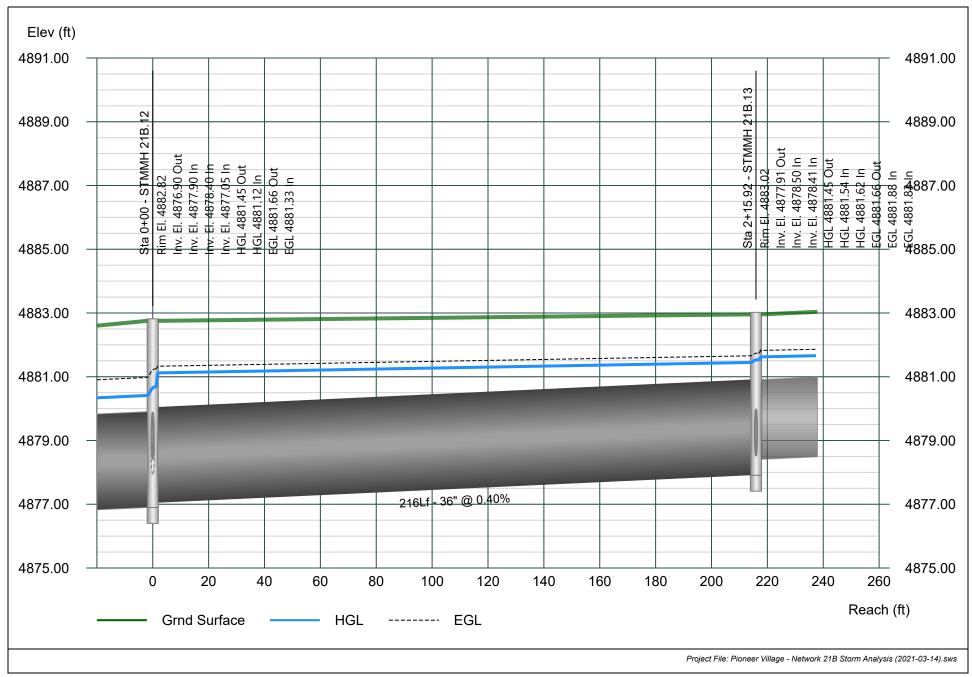


Line 24 - Pipe - (519) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24

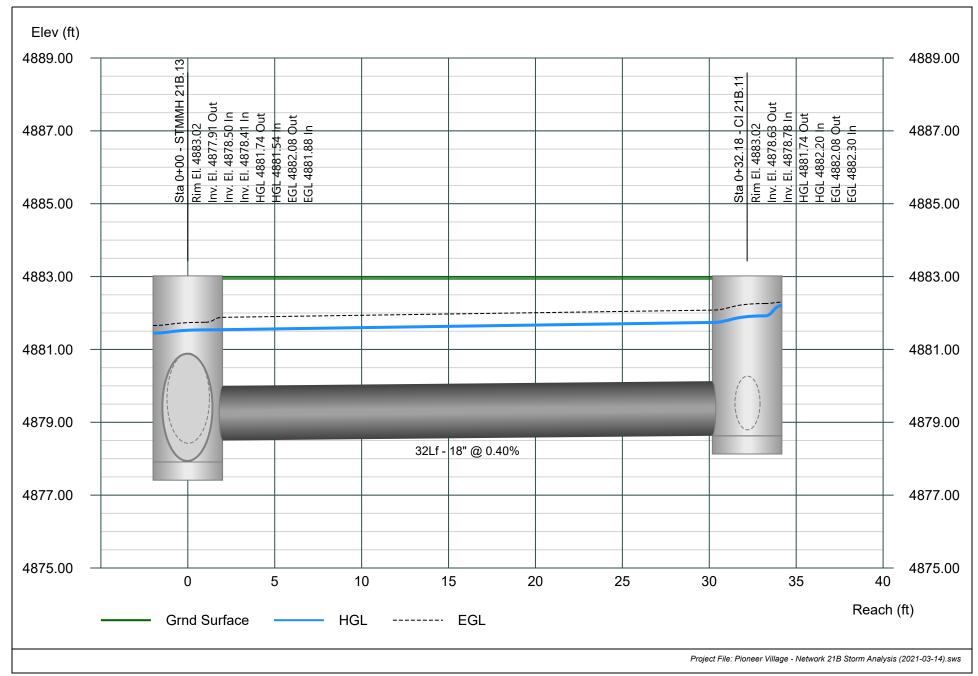


Line 25 - Pipe - (487) (Storm Sewer - 21 B Network)

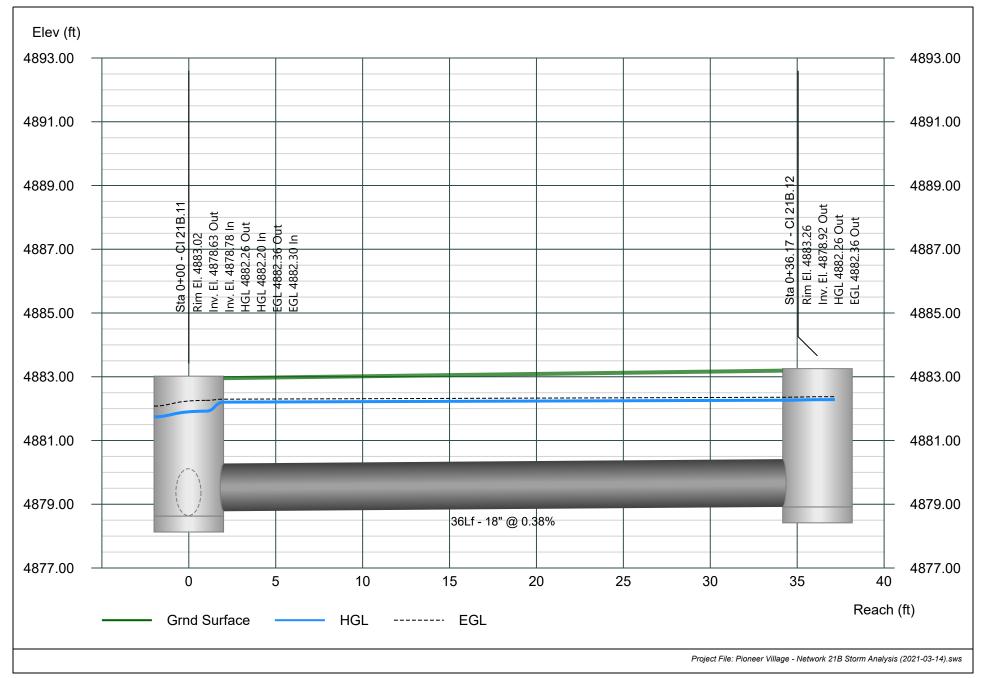


Line 26 - Pipe - (486) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24

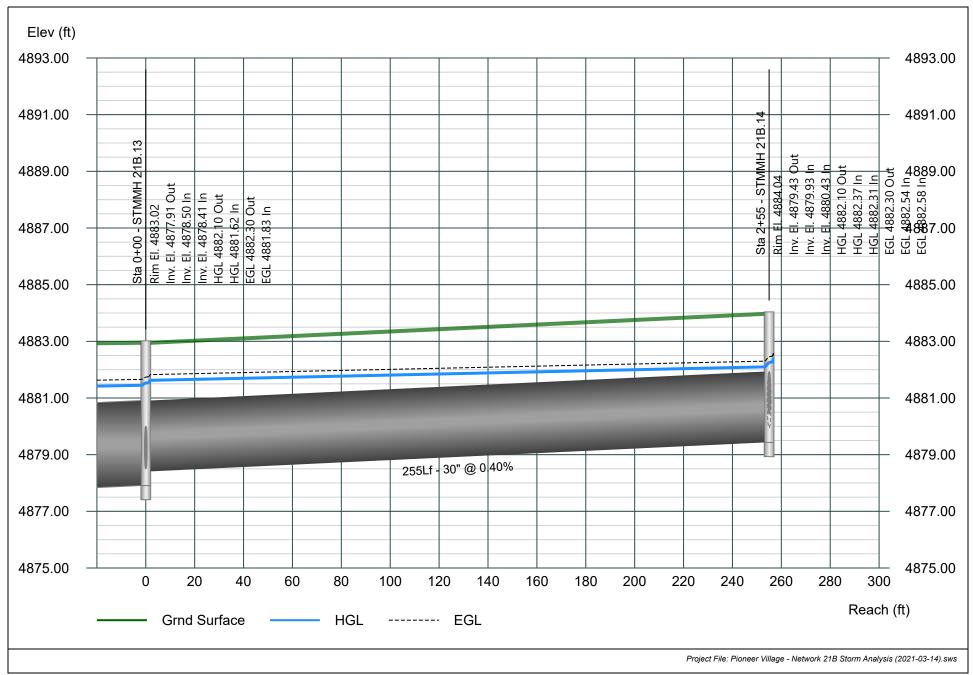


Line 27 - Pipe - (485) (Storm Sewer - 21 B Network)



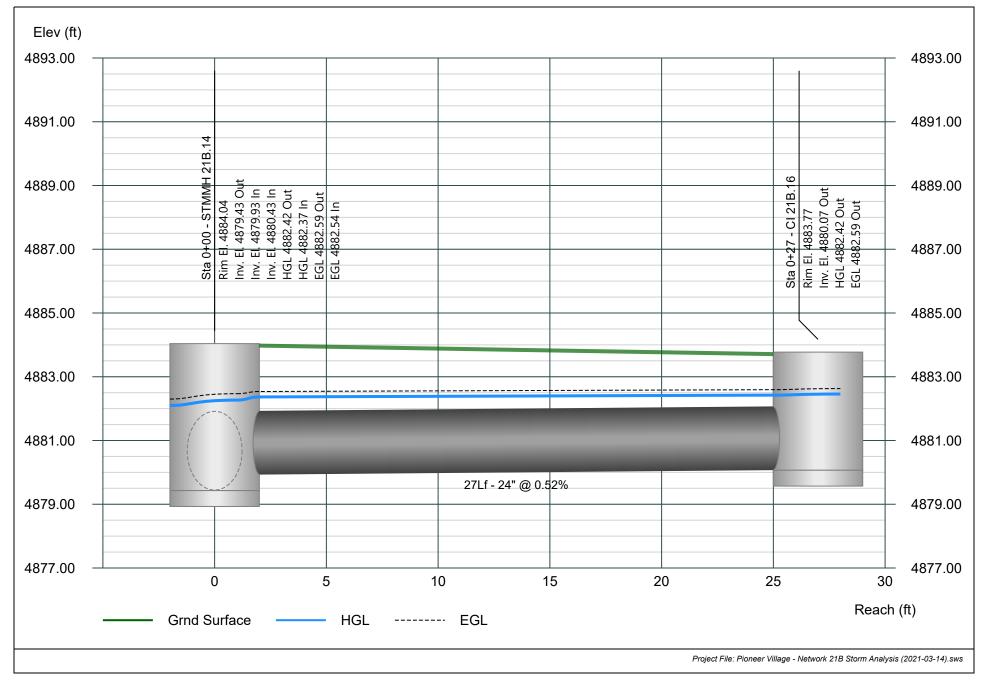
Line 28 - Pipe - (580) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24

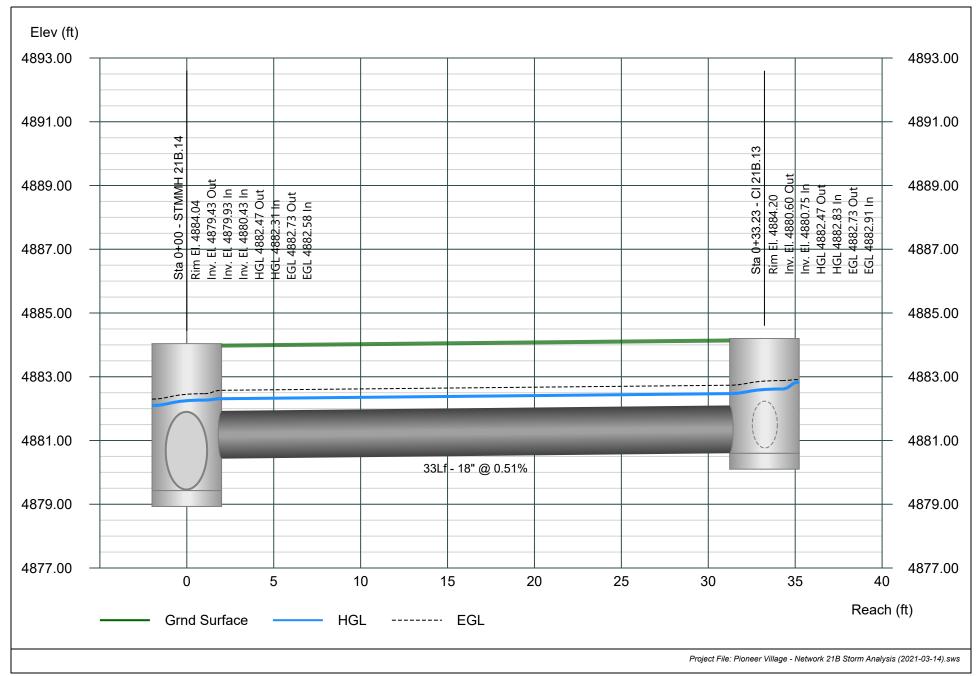


Line 29 - Pipe - (587) (Storm Sewer - 21 B Network)

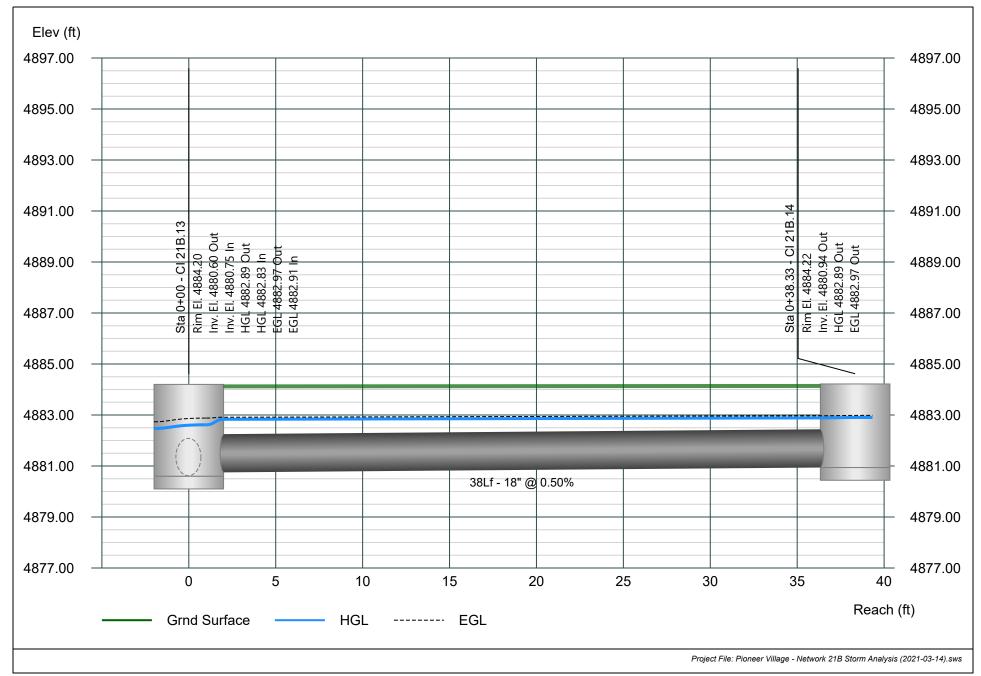
Stormwater Studio 2021 v 3.0.0.24



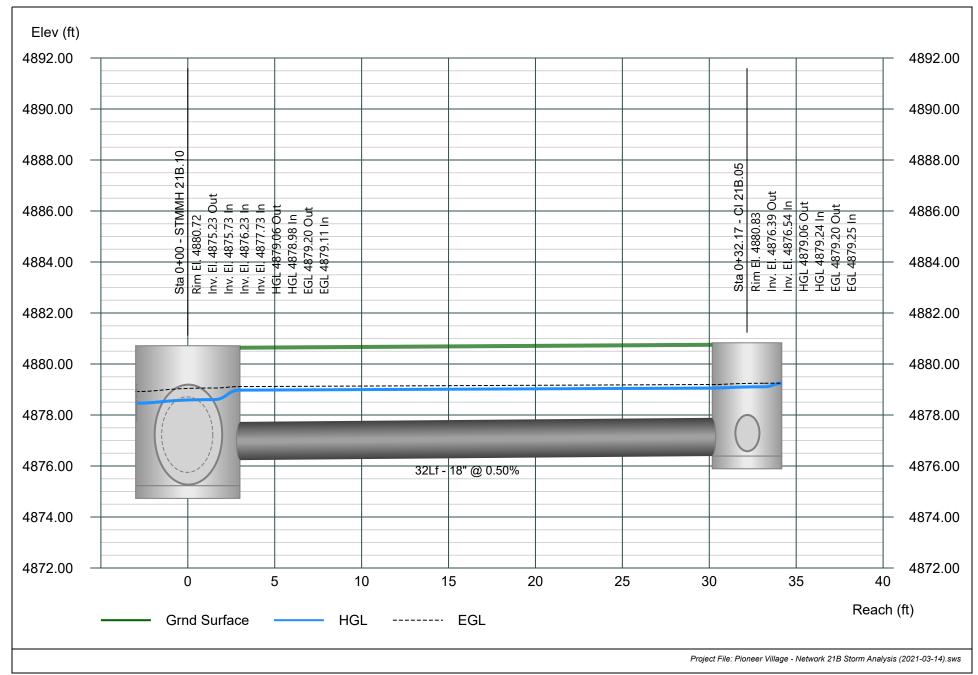
Line 30 - Pipe - (579) (Storm Sewer - 21 B Network)



Line 31 - Pipe - (578) (Storm Sewer - 21 B Network)

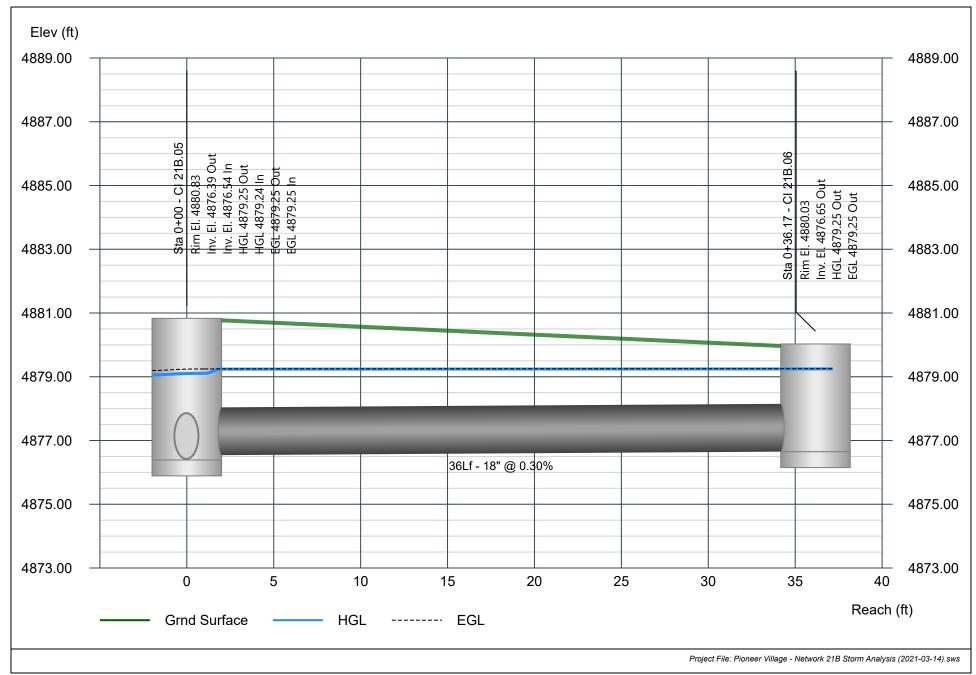


Line 32 - Pipe - (586)(0) (Storm Sewer - 21 B Network)



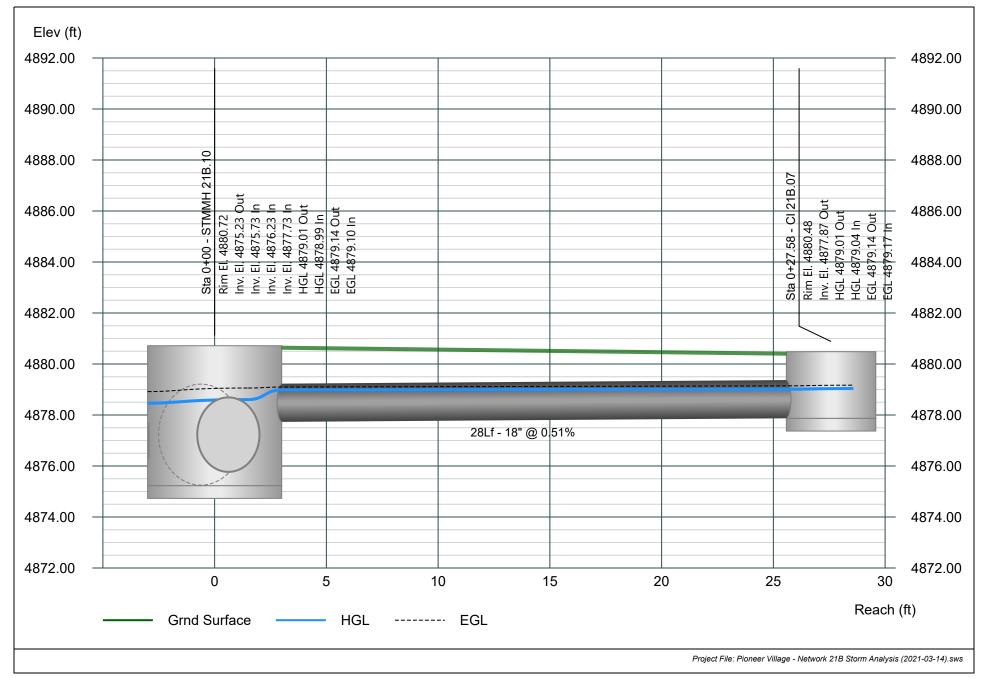
Line 33 - Pipe - (584)(0) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



Line 34 - Pipe - (517) (Storm Sewer - 21 B Network)

Stormwater Studio 2021 v 3.0.0.24



Energy Grade Line Calculations

03-15-2021

Line	Line Size	_			Do	ownstrea	m			gth	Upstream							Pi	ре		Junction		
No		Q	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	Len	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	n Value	Enrgy Loss	HGLa Elev	EGLa Elev	Enrgy Loss	
	(in)	(cfs)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)		(ft)	(ft)	(ft)	(ft)	
1	48x76e	99.96	4864.97	4.00	19.90	4868.97	5.02	0.39	4869.36	64.63	4865.29	3.80	19.50	4869.09	5.13	0.41	4869.50	0.013	0.139	4869.28	4869.69	0.19	
2	48x76e	99.96	4865.54	3.92	19.90	4869.46	5.02	0.39	4869.85	500.00	4868.04	2.00	9.95	4870.04	10.05	1.57	4871.61	0.013	1.762	4870.04	4871.61	0.00	
3	48x76e	99.96	4868.12	3.23	17.95	4871.35	5.57	0.48	4871.83	500.00	4870.12	2.00	9.95	4872.12	10.05	1.57	4873.69	0.013	1.861	4872.12	4873.69	0.00	
4	54	99.96	4870.27	3.06 ³	11.52	4873.33	8.68	1.17	4874.50	90.32	4870.63	3.06	11.52	4873.69	8.68	1.17	4874.86	0.013	0.360	4874.41	4875.58	0.72	
5	24	6.96	4872.91	2.00	3.14	4875.53	2.22	0.08	4875.61	7.00	4872.94	2.00	3.14	4875.54	2.22	0.08	4875.62	0.013	0.007	4875.56	4875.63	0.02	
6	18	12.09	4872.91	1.50 ³	1.77	4875.14	6.84	0.73	4875.87	29.17	4873.05	1.50	1.77	4875.53	6.84	0.73	4876.26	0.013	0.387	4875.67	4876.40	0.15	
7	54	80.91	4870.78	4.50	15.90	4875.34	5.09	0.40	4875.74	102.37	4871.19	4.30	15.65	4875.49	5.17	0.42	4875.90	0.013	0.162	4875.83	4876.25	0.35	
8	24	5.50	4873.22	2.00	3.14	4876.22	1.75	0.05	4876.27	284.26	4875.06	1.33	2.22	4876.39	2.47	0.10	4876.49	0.013	0.218	4876.42	4876.51	0.03	
9	18	5.50	4876.09	0.81‡	0.97	4876.90	5.66	0.50	4877.37	63.38	4876.69	0.90²	1.10	4877.59	5.00	0.39	4877.98	0.013	0.602	4877.59	4877.98	0.00	
10	18	5.50	4876.69	0.89‡	1.10	4877.58	5.00	0.39	4878.04	117.77	4877.38	0.90²	1.10	4878.28	5.00	0.39	4878.67	0.013	0.626	4878.28	4878.67	0.00	
11	18	5.50	4877.90	1.07³	1.35	4878.97	4.07	0.26	4879.23	37.04	4878.04	1.07	1.35	4879.11	4.07	0.26	4879.37	0.013	0.137	4879.18	4879.44	0.07	
12	54	75.41	4871.34	4.50	15.90	4876.04	4.74	0.35	4876.39	49.81	4871.49	4.50	15.90	4876.11	4.74	0.35	4876.46	0.013	0.073	4876.24	4876.59	0.12	
13	24	8.43	4874.32	2.00	3.14	4876.52	2.68	0.11	4876.63	27.15	4874.46	2.00	3.14	4876.56	2.68	0.11	4876.67	0.013	0.038	4876.58	4876.69	0.02	
14	18	8.13	4874.32	1.50 ³	1.77	4876.39	4.60	0.33	4876.72	6.85	4874.35	1.50	1.77	4876.43	4.60	0.33	4876.76	0.013	0.041	4876.50	4876.82	0.07	
15	48	58.85	4871.99	4.00	12.56	4876.38	4.68	0.34	4876.72	155.64	4872.61	4.00	12.57	4876.61	4.68	0.34	4876.95	0.013	0.231	4876.75	4877.09	0.13	
16	48	58.85	4872.76	4.00	12.56	4876.88	4.68	0.34	4877.22	40.15	4872.92	4.00	12.57	4876.92	4.68	0.34	4877.26	0.013	0.039	4877.07	4877.41	0.14	
17	48	58.85	4873.07	4.00	12.56	4877.20	4.68	0.34	4877.54	28.33	4873.18	4.00	12.57	4877.25	4.68	0.34	4877.59	0.013	0.047	4877.42	4877.76	0.17	
18	48	58.85	4873.33	4.00	12.56	4877.56	4.68	0.34	4877.90	66.43	4873.60	4.00	12.57	4877.67	4.68	0.34	4878.01	0.013	0.111	4877.81	4878.15	0.14	
19	48	58.85	4873.75	4.00	12.56	4877.95	4.68	0.34	4878.29	368.72	4875.23	3.23	10.89	4878.46	5.41	0.45	4878.92	0.013	0.627	4878.60	4879.06	0.14	
20	36	49.37	4875.73	3.00 ³	7.07	4878.73	6.99	0.76	4879.49	22.63	4875.82	3.00	7.07	4878.82	6.98	0.76	4879.58	0.013	0.088	4879.04	4879.80	0.23	
21	18	6.74	4876.82	1.50	1.77	4879.67	3.81	0.23	4879.89	7.00	4876.89	1.50	1.77	4879.70	3.81	0.23	4879.92	0.013	0.029	4879.74	4879.97	0.05	
22	36	42.63	4875.97	3.00	7.07	4879.46	6.03	0.57	4880.03	232.37	4876.90	3.00	7.07	4880.41	6.03	0.57	4880.98	0.013	0.949	4880.68	4881.25	0.27	
Notes:	Return Perio	d = 100-	yrs. ² Critic	al depth	. ³ Norm	al depth. ‡	Superc	ritical. r	= rectang	ular e = e	elliptical a =	arch				Pro	iject File: Pior	neer Villag	e - Networ	k 21B Storm /	Analysis (2021	1-03-14).sws	

Energy Grade Line Calculations

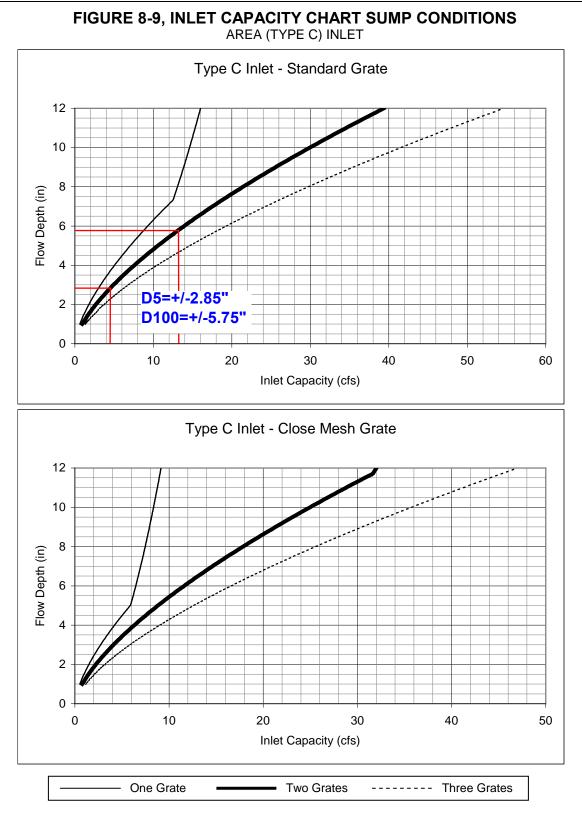
Project Name: Pioneer Village Storm Network 21B

03-15-2021

Line	Line Size		Downstream				Length	Upstream							Pi	ре	Junction					
No		Q	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	Len	Invert Elev	Depth	Area	HGL Elev	Vel	Vel Head	EGL Elev	n Value	Enrgy Loss	HGLa Elev	EGLa Elev	Enrgy Loss
	(in)	(cfs)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft)	(ft)	(sqft)	(ft)	(ft/s)	(ft)	(ft)		(ft)	(ft)	(ft)	(ft)
23	18	11.20	4877.90	1.50 ³	1.77	4880.87	6.34	0.62	4881.50	52.19	4878.16	1.50	1.77	4881.47	6.34	0.62	4882.09	0.013	0.594	4881.59	4882.22	0.13
24	18	5.50	4878.40	1.50	1.77	4881.16	3.11	0.15	4881.31	32.17	4878.56	1.50	1.77	4881.25	3.11	0.15	4881.40	0.013	0.088	4881.28	4881.43	0.03
25	36	25.93	4877.05	3.00	7.07	4881.12	3.67	0.21	4881.33	215.92	4877.91	3.00	7.07	4881.45	3.67	0.21	4881.66	0.013	0.326	4881.54	4881.75	0.09
26	18	8.25	4878.50	1.50 ³	1.77	4881.54	4.67	0.34	4881.88	32.18	4878.63	1.50	1.77	4881.74	4.67	0.34	4882.08	0.013	0.199	4881.92	4882.26	0.18
27	18	4.30	4878.78	1.50	1.77	4882.20	2.43	0.09	4882.30	36.17	4878.92	1.50	1.77	4882.26	2.43	0.09	4882.36	0.013	0.061	4882.28	4882.38	0.02
28	30	17.68	4878.41	2.50	4.91	4881.62	3.60	0.20	4881.83	255.00	4879.43	2.50	4.91	4882.10	3.60	0.20	4882.30	0.013	0.474	4882.27	4882.47	0.17
29	24	10.40	4879.93	2.00	3.14	4882.37	3.31	0.17	4882.54	27.00	4880.07	2.00	3.14	4882.42	3.31	0.17	4882.59	0.013	0.057	4882.46	4882.63	0.03
30	18	7.28	4880.43	1.50	1.77	4882.31	4.12	0.26	4882.58	33.23	4880.60	1.50	1.77	4882.47	4.12	0.26	4882.73	0.013	0.159	4882.62	4882.88	0.15
31	18	4.05	4880.75	1.50	1.77	4882.83	2.29	0.08	4882.91	38.33	4880.94	1.50	1.77	4882.89	2.29	0.08	4882.97	0.013	0.057	4882.90	4882.99	0.02
32	18	5.28	4876.23	1.50	1.77	4878.98	2.99	0.14	4879.11	32.17	4876.39	1.50	1.77	4879.06	2.99	0.14	4879.20	0.013	0.082	4879.11	4879.25	0.05
33	18	1.29	4876.54	1.50	1.77	4879.24	0.73	0.01	4879.25	36.17	4876.65	1.50	1.77	4879.25	0.73	0.01	4879.25	0.013	0.005	4879.25	4879.26	0.00
34	18	4.20	4877.73	1.26	1.58	4878.99	2.66	0.11	4879.10	27.58	4877.87	1.14	1.44	4879.01	2.91	0.13	4879.14	0.013	0.046	4879.04	4879.17	0.03

Type C Inlet #4.02 - Capacity Analysis

Chapter 8. Inlets



Notes:

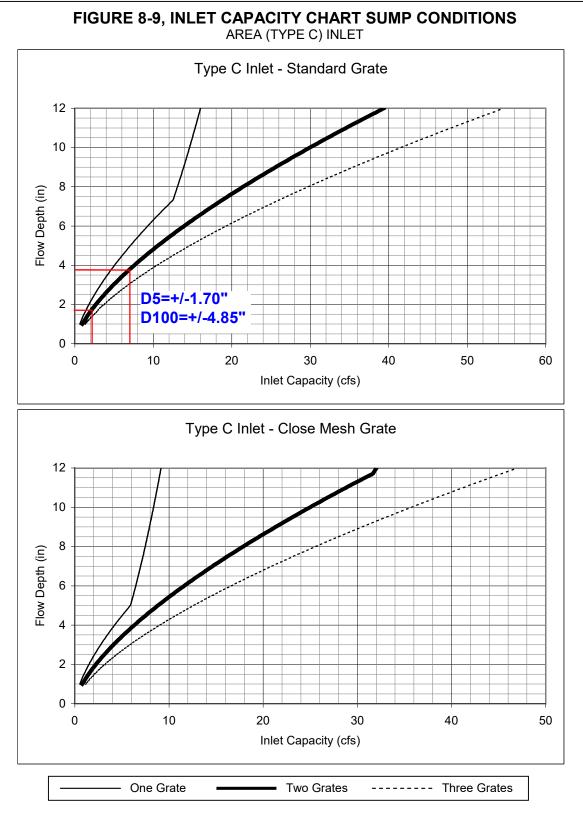
1. SEMSWA standard inlet parameters must apply to use these charts.

SEMSWA Stormwater Management ManualPage 8-15

Inlet #10 will collect runoff from Basins 07 and 07a. Combining the flow rates of each inlet nets a Q_5 of 1.44 and Q_{100} of 2.81 CFS. The ponding depths are provided above.

Type C Inlet #4.03 - Capacity Analysis

Chapter 8. Inlets

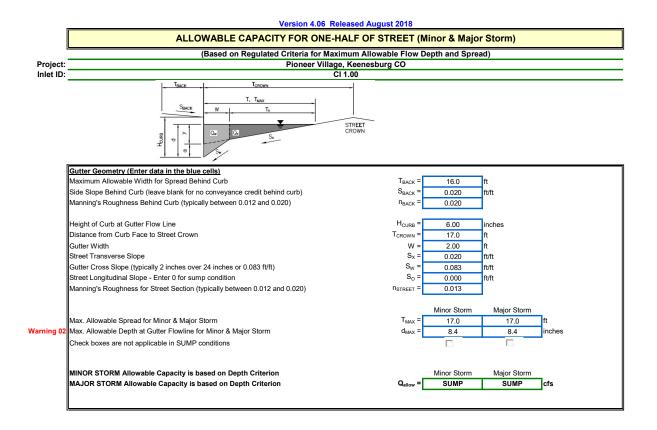


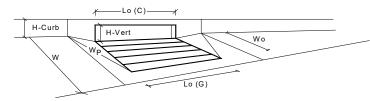
Notes:

1. SEMSWA standard inlet parameters must apply to use these charts.

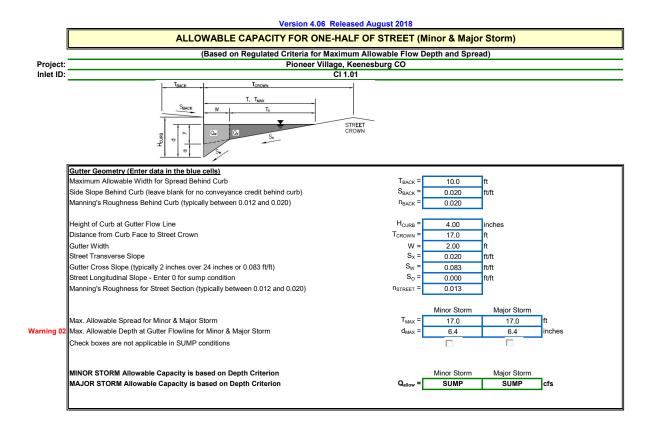
SEMSWA Stormwater Management ManualPage 8-15

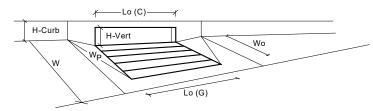
Inlet #10 will collect runoff from Basins 07 and 07a. Combining the flow rates of each inlet nets a Q_5 of 1.44 and Q_{100} of 2.81 CFS. The ponding depths are provided above.



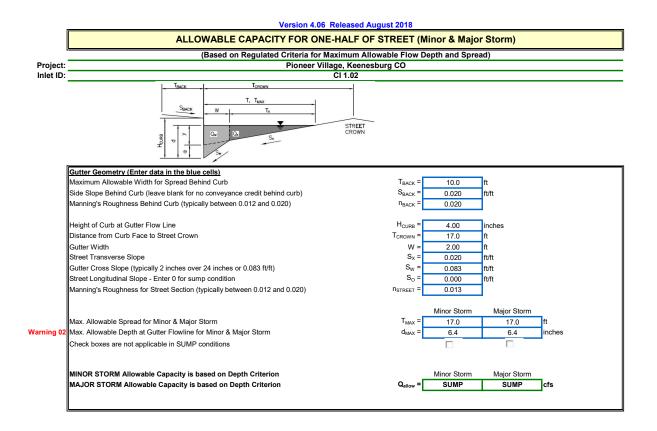


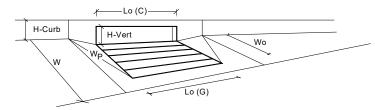
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	🧾 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	7
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	7
Curb Opening Information		MINOR	MAJOR	-
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	7
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	7
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.53	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.76	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.3	10.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.6	8.1	cfs



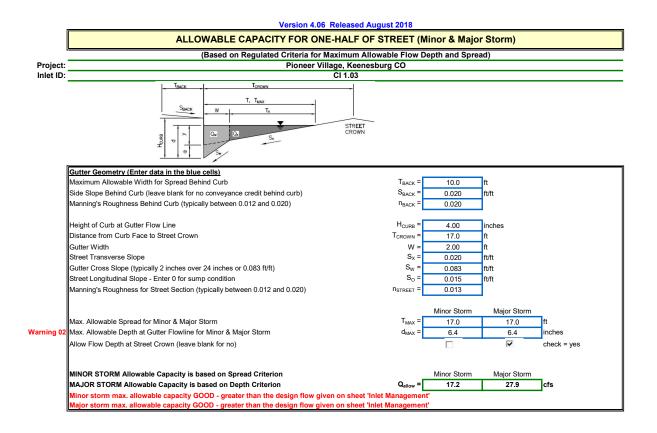


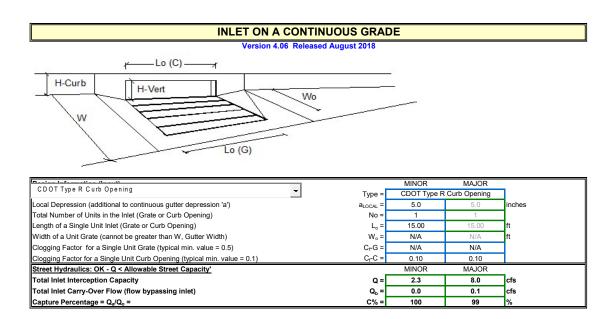
Design Information (Input)	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	🥅 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.53	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.76	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.3	10.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.9	3.1	cfs

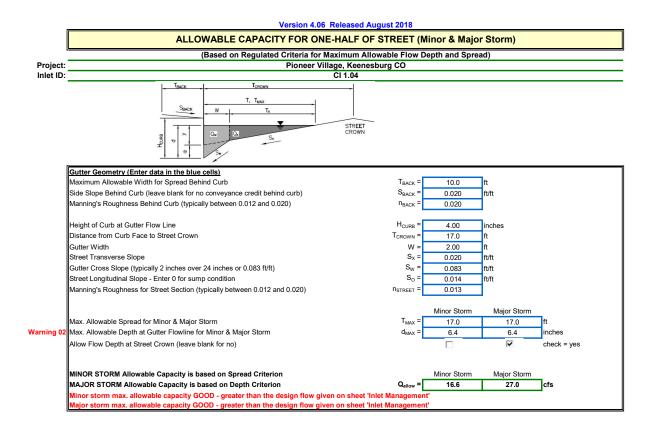


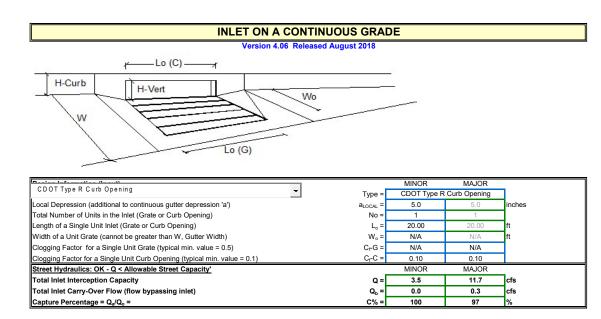


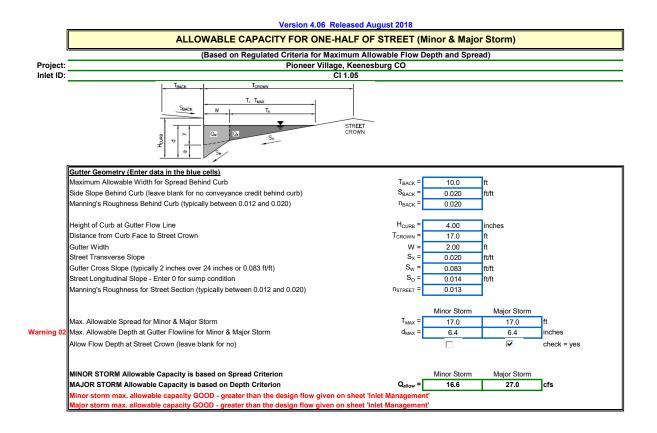
CDOT Type R Curb Opening	_	MINOR	MAJOR	_
	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information	-	MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.53	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.76	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.3	10.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.5	9.1	cfs

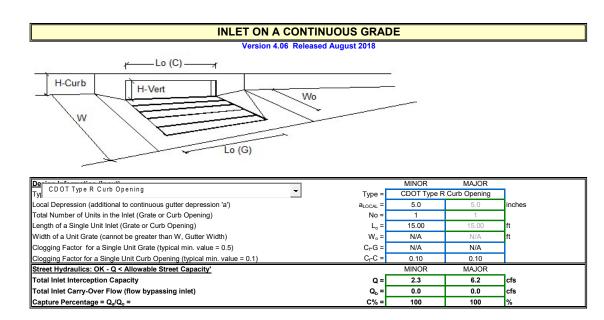


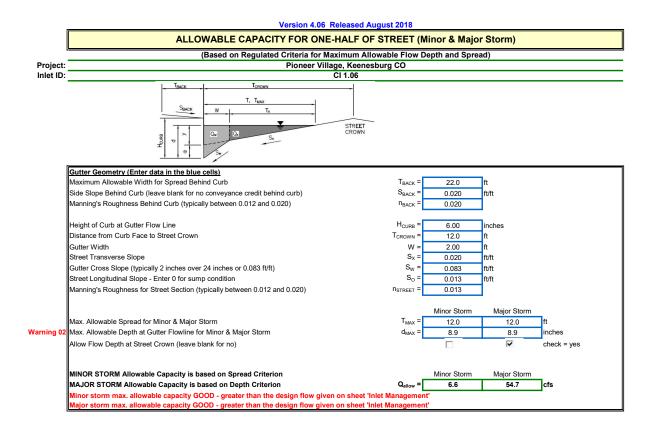


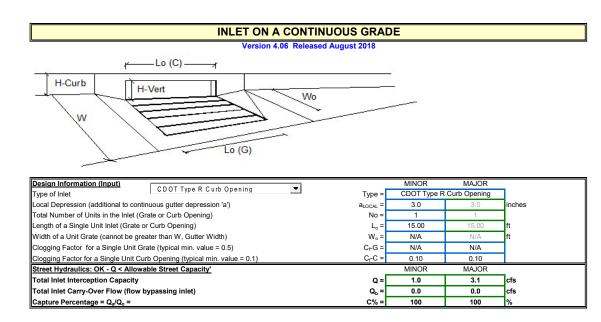


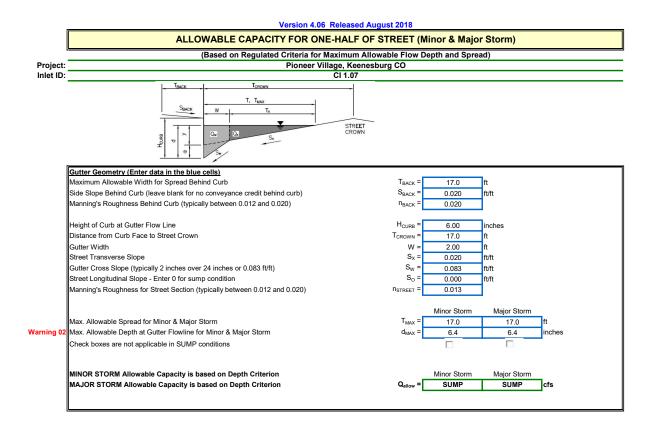


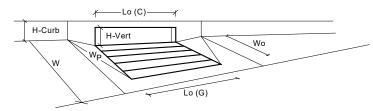




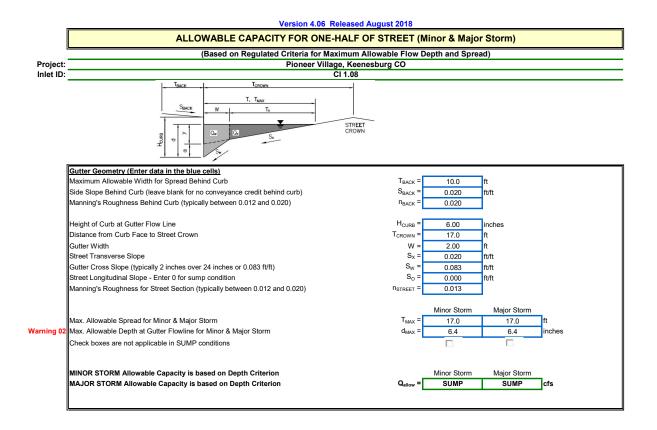


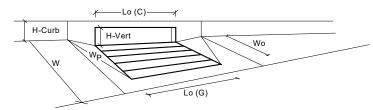




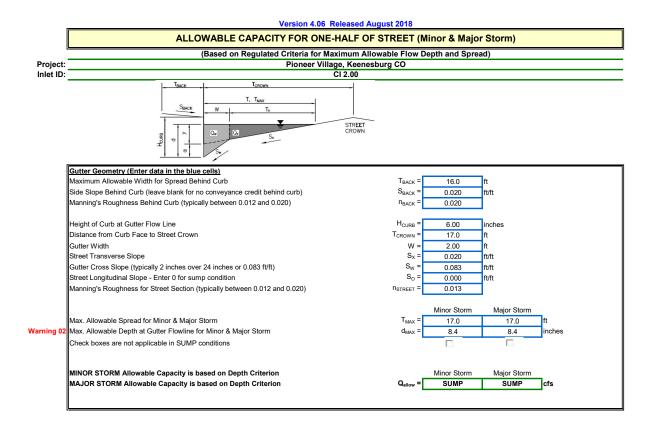


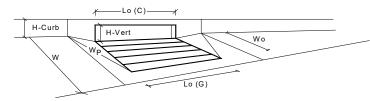
Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.4	inches
Grate Information		MINOR	MAJOR	🔽 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.37	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.60	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.81	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	8.0	11.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.8	2.1	cfs



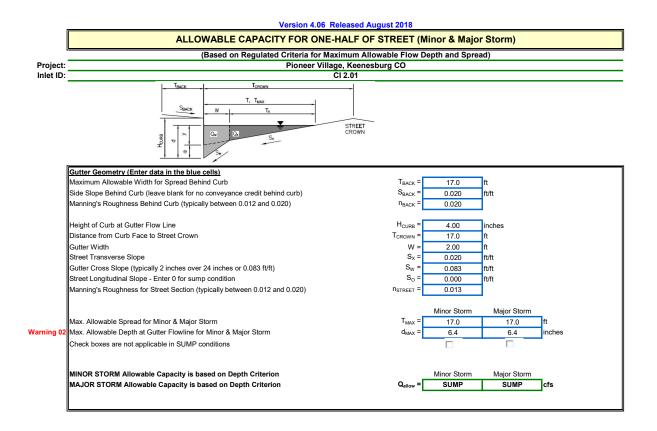


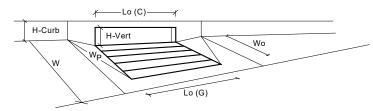
CDOT Type R Curb Opening	_	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.4	inches
Grate Information		MINOR	MAJOR	🔽 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C ₀ (G) =	N/A	N/A	-
Curb Opening Information	-	MINOR	MAJOR	-
Length of a Unit Curb Opening	L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.37	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.60	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.81	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	8.0	11.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.6	4.2	cfs



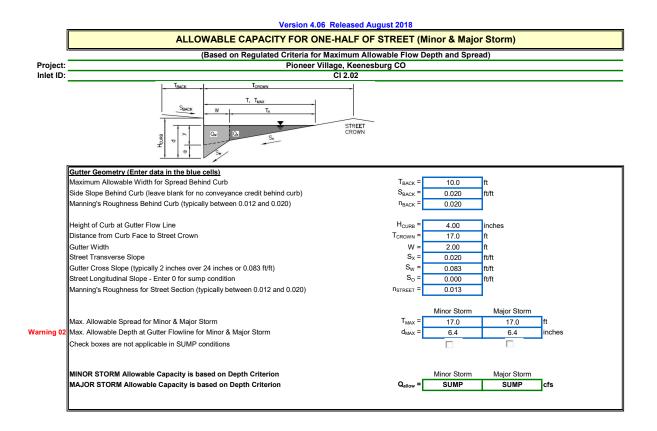


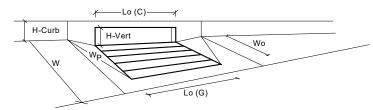
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	8.4	inches
Grate Information		MINOR	MAJOR	🔽 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	7
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.53	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.79	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.91	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.3	29.2	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	4.8	15.1	cfs



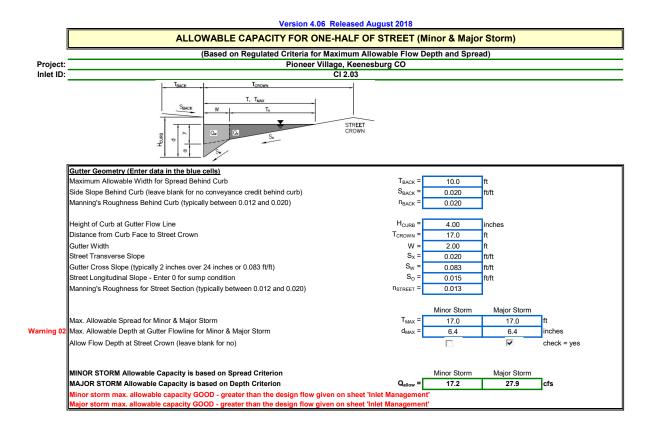


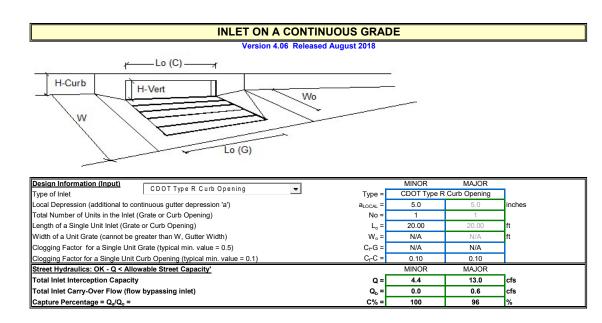
Design Information (Input) CDOT Type R Curb Openin	g 🔫 _	MINOR	MAJOR	
Type of Inlet	g Type =	CDOT Type I	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' fro	om above) a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.4	inches
Grate Information		MINOR	MAJOR	🔽 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	teet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	7
Curb Opening Information		MINOR	MAJOR	-
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.37	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.60	7
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.81	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogge	d condition) Q _a =	10.3	14.8	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK) Q _{PEAK REQUIRED} =	3.8	12.5	cfs

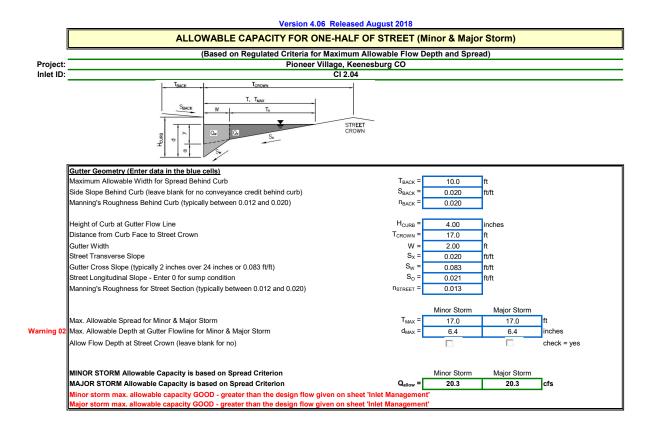


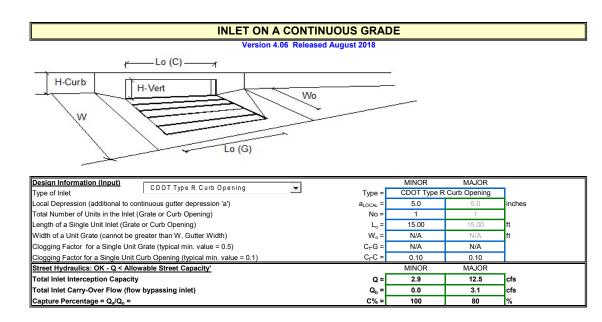


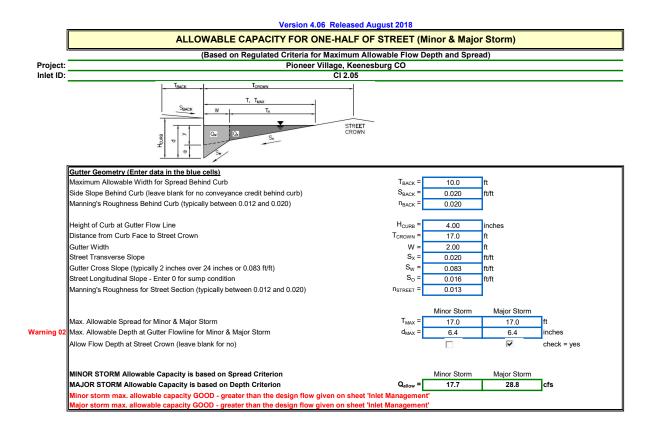
Design Information (Input) CDOT Type R Curb Opening	-	MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from about	ove) a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.4	inches
Grate Information		MINOR	MAJOR	🔽 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	teet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C ₀ (C) =	0.67	0.67]
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.37	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.60	7
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.81	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	
Total Inlet Interception Capacity (assumes clogged cor	ndition) Q _a =	10.3	14.8	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.0	12.4	cfs

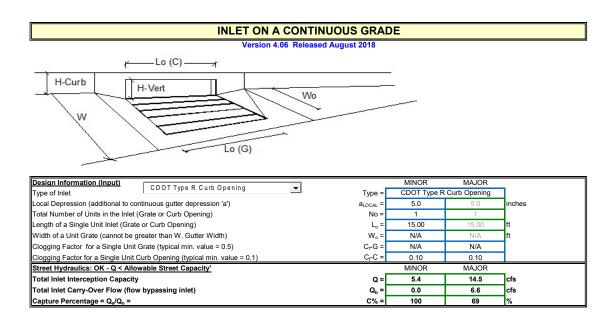


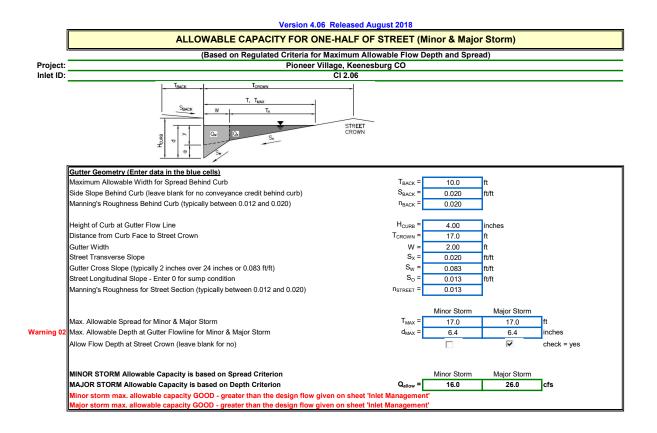


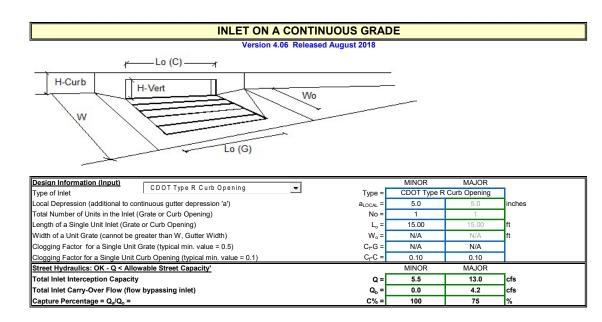


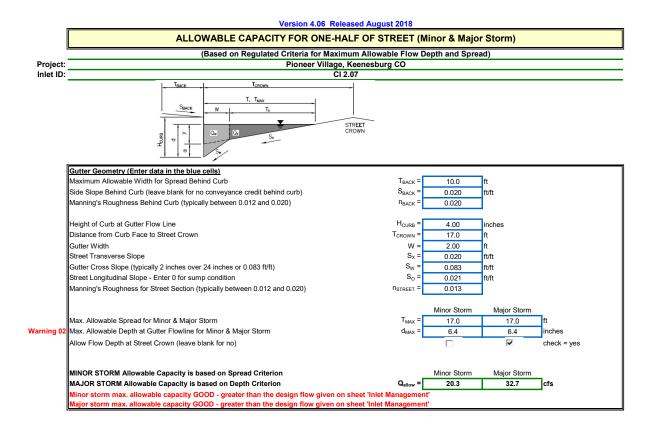






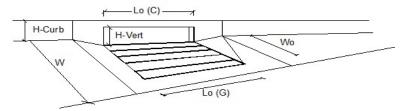




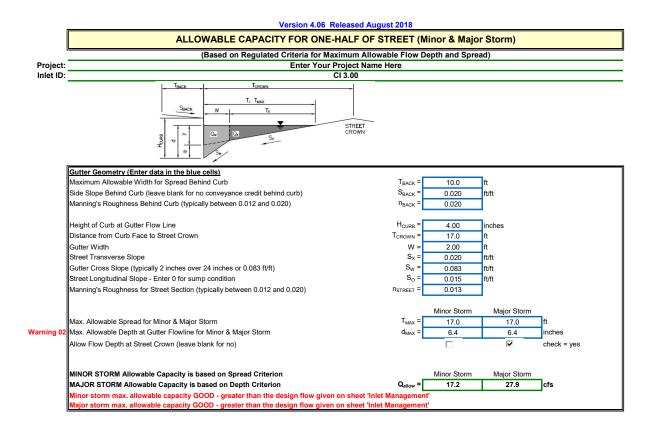






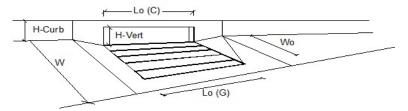


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.8	5.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q_a/Q_o =	C% =	100	100	%

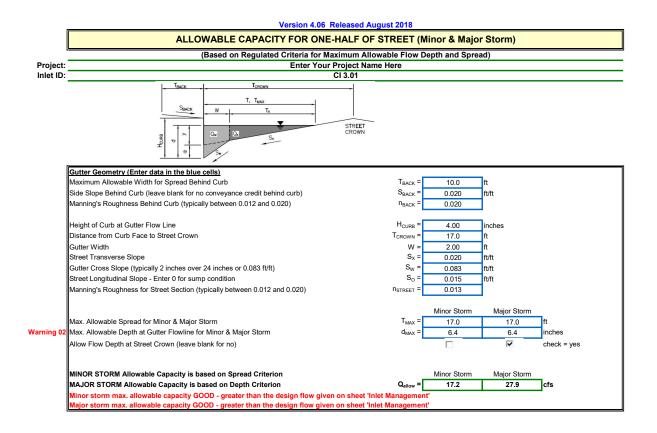






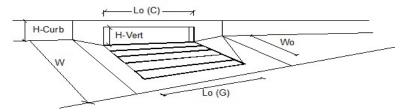


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.4	8.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	98	%

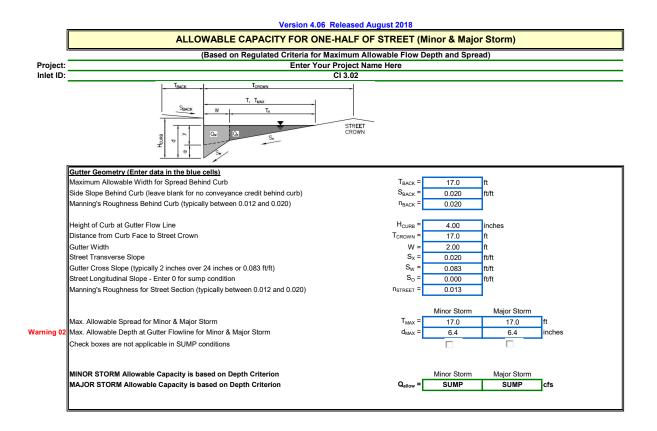


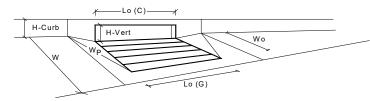




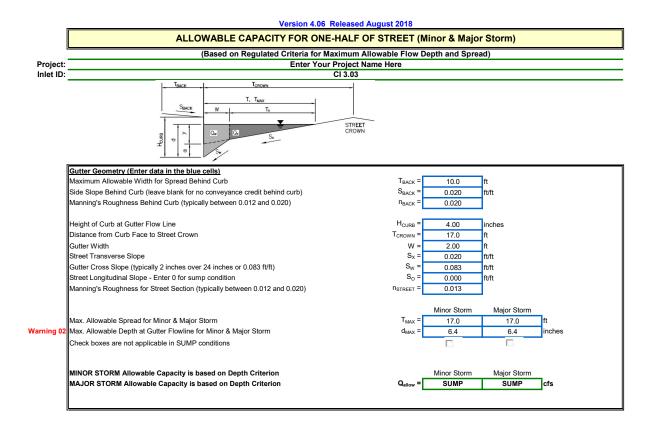


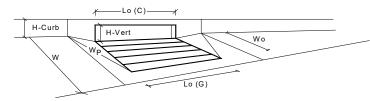
Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.9	13.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.7	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	95	%



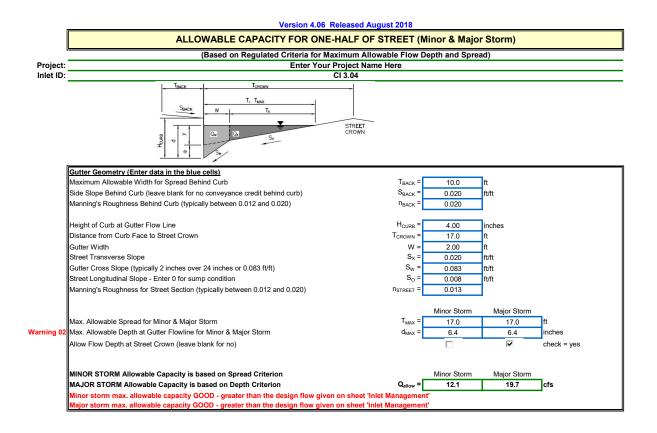


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.4	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.37	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.60	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.81	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	8.0	11.6	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	3.8	10.4	cfs



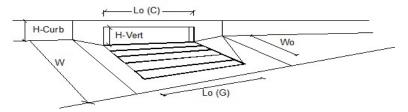


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	6.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.33	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.57	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.79	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	8.0	9.7	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.9	6.8	cfs

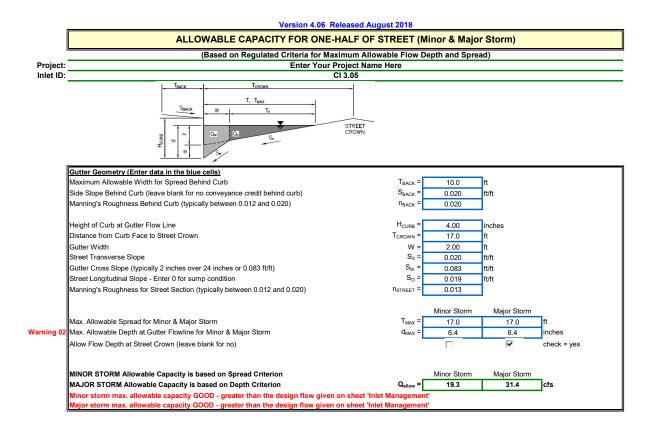






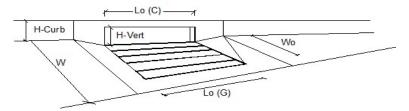


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	5.2	10.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.6	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	87	%

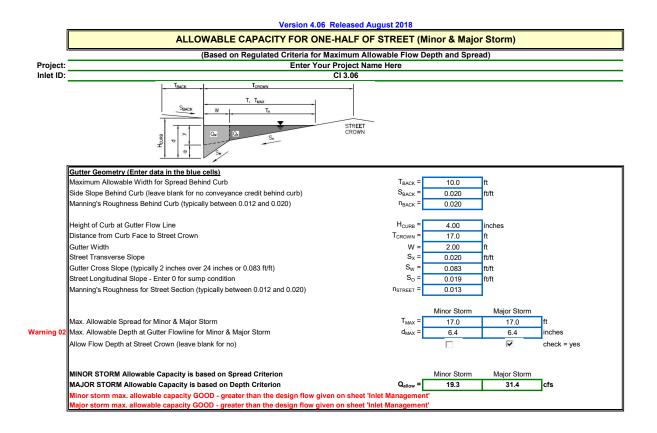






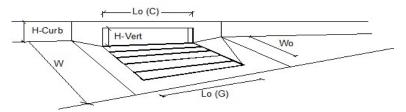


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.4	5.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

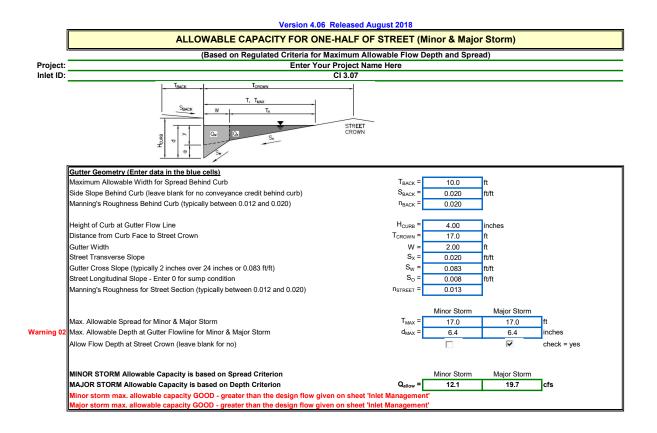






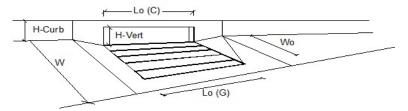


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.2	7.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q₀ =	C% =	100	100	%

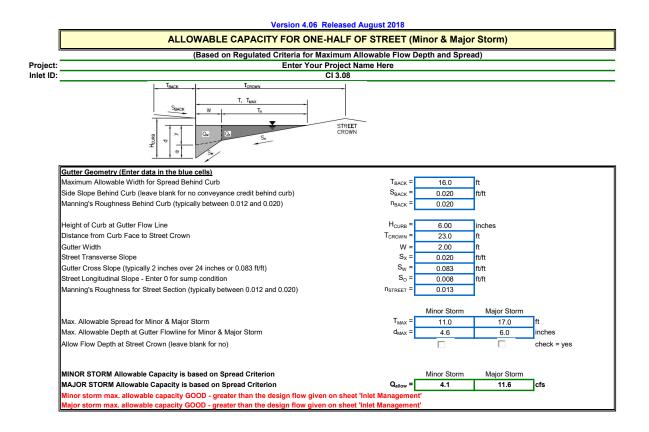






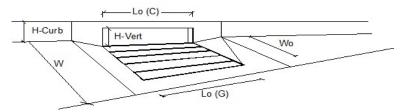


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R Curb Opening		
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.8	6.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	99	%

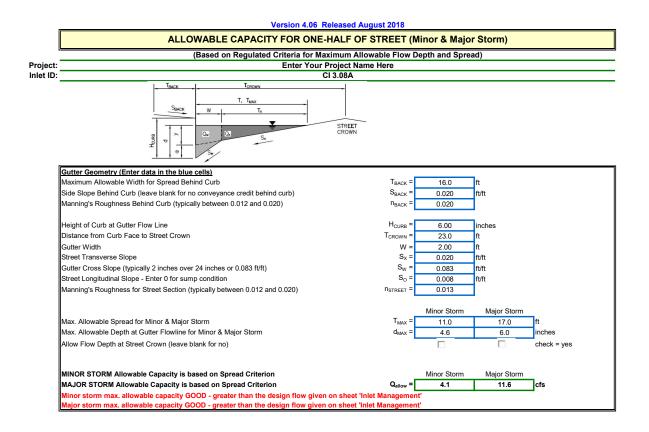






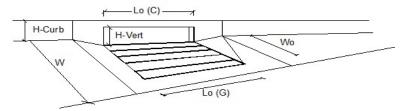


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.2	2.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

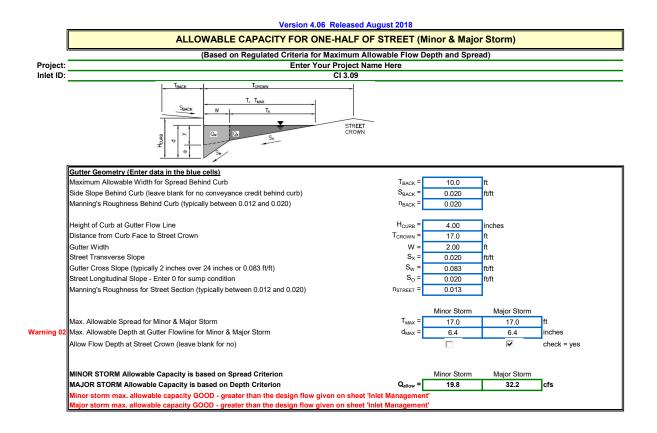






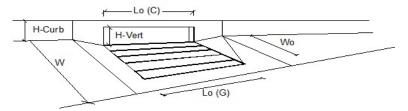


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	0.9	2.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

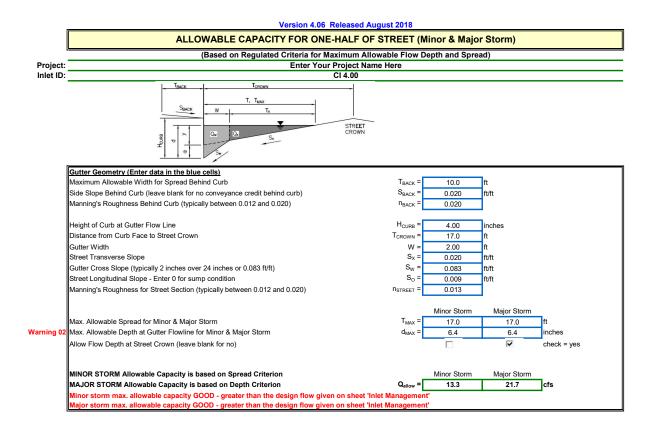






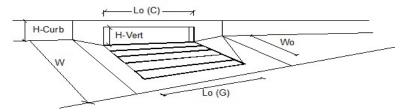


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.2	9.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	96	%

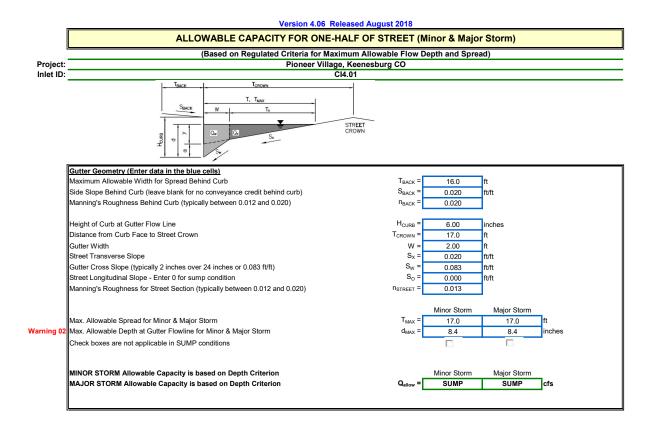


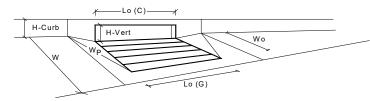




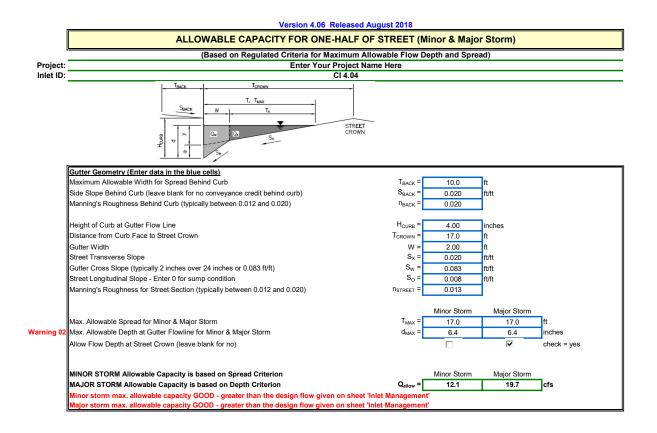


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.7	15.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	2.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	99	87	%



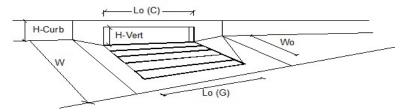


CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	8.4	inches
Grate Information		MINOR	MAJOR	🔽 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.53	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.79	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.91	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	1
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.3	29.2	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	2.3	10.8	cfs

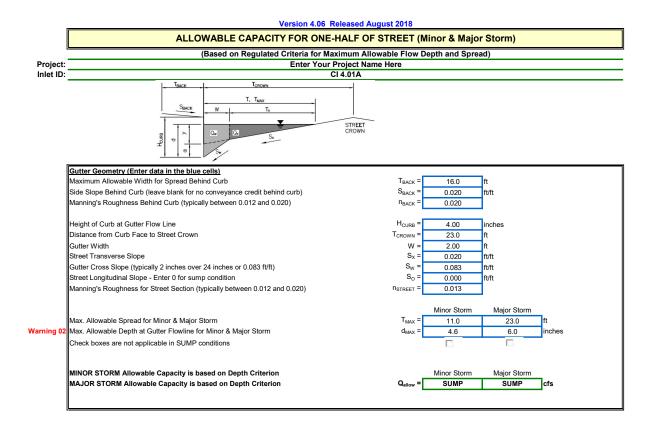


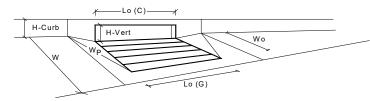




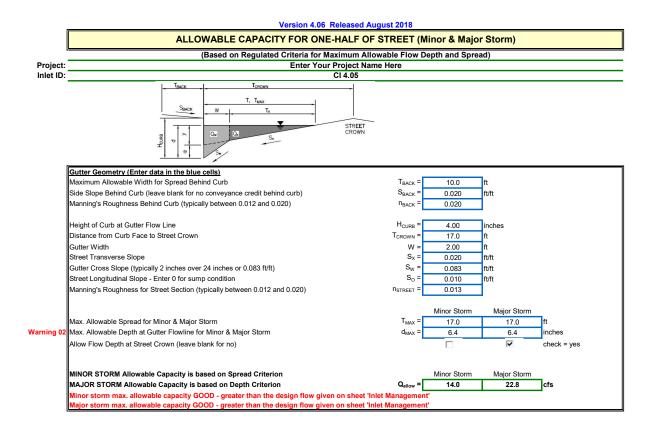


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	7.3	15.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	2.6	cfs
Capture Percentage = Q _a /Q _o =	C% =	98	86	%



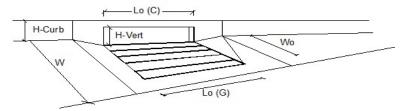


Design Information (Input)		MINOR	MAJOR	_
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	4.2	6.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	-
Length of a Unit Curb Opening	L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.18	0.33	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.39	0.57	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.65	0.79	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	3.2	9.7	cfs
WARNING: Inlet Capacity less than Q Peak for Minor Storm	Q PEAK REQUIRED =	3.5	8.2	cfs

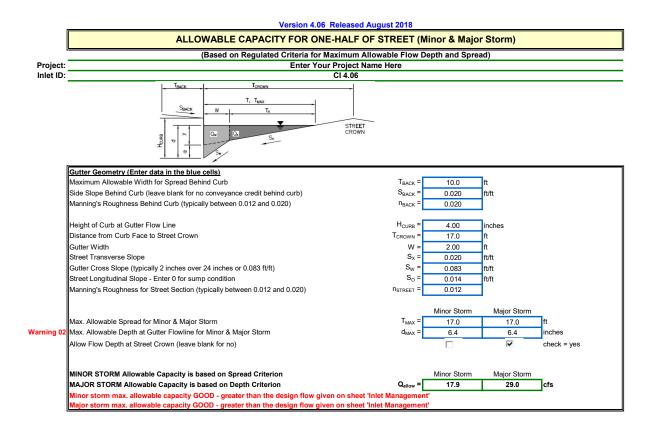






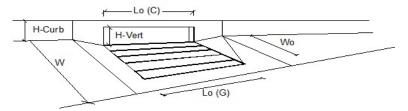


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	4.8	10.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.1	cfs
Capture Percentage = Q _a /Q₀ =	C% =	100	90	%

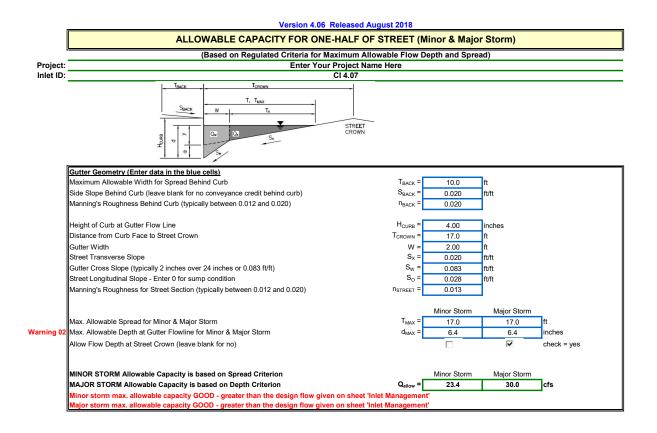






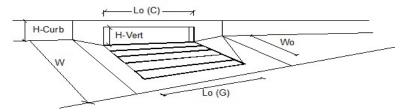


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.5	3.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

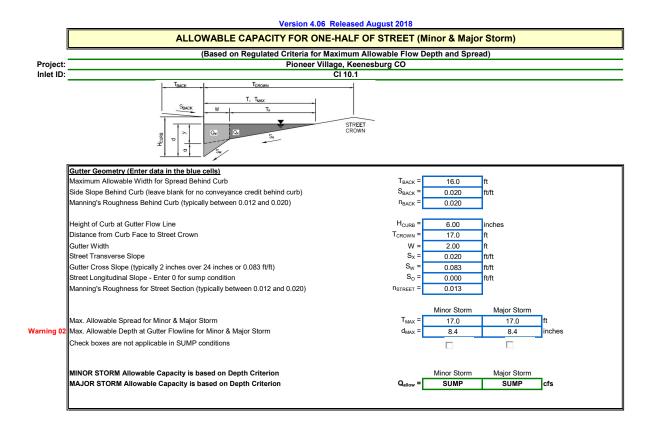


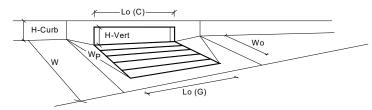




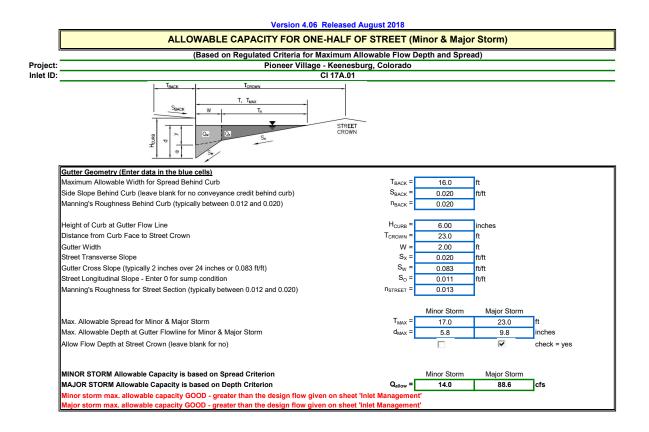


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.7	8.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%



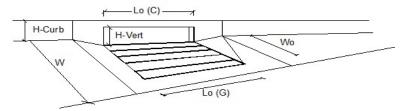


CDOT Type R Curb Opening		MINOR	MAJOR	
	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information	_	MINOR	MAJOR	_
Length of a Unit Curb Opening	L _o (C) =	15.00	15.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.53	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.76	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	8.0	8.0	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	1.6	4.2	cfs

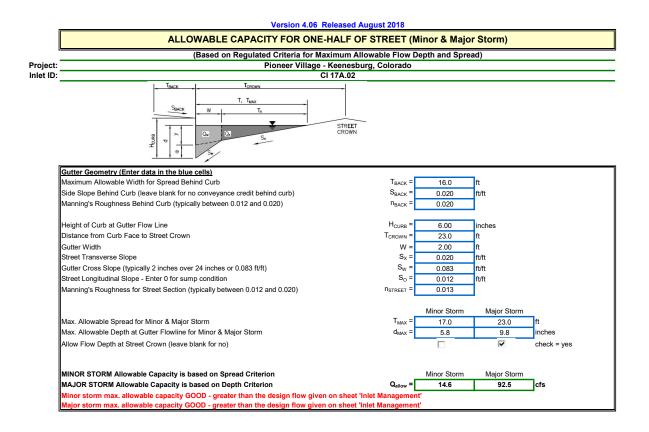






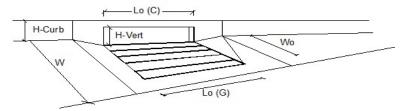


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	8.2	15.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	3.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	83	%

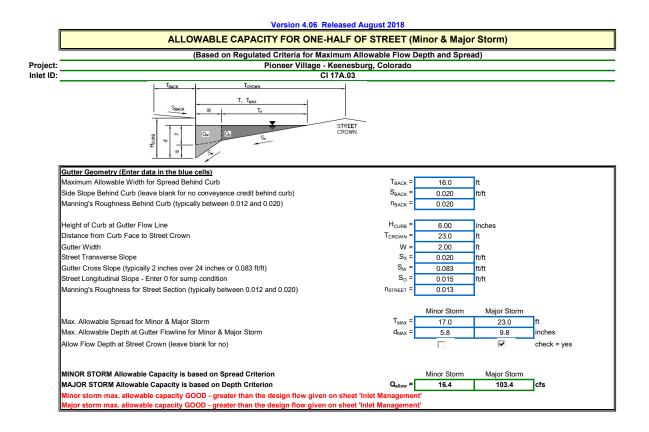






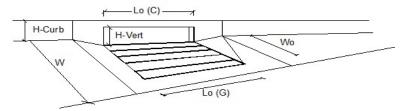


Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	9.3	17.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	5.2	cfs
Capture Percentage = Q _a /Q _o =	С% =	100	77	%

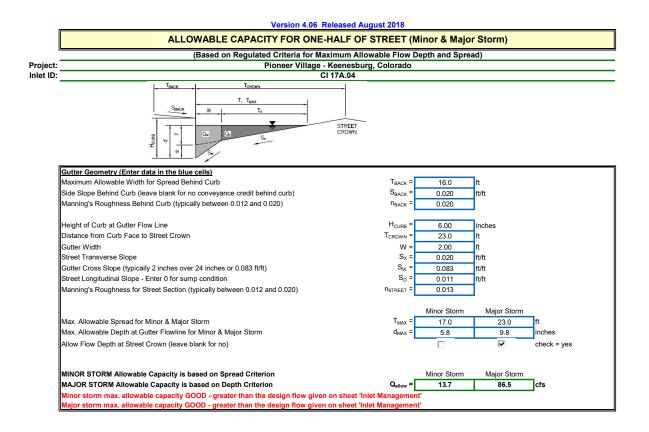






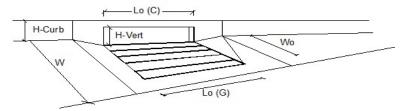


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.4	13.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	91	%

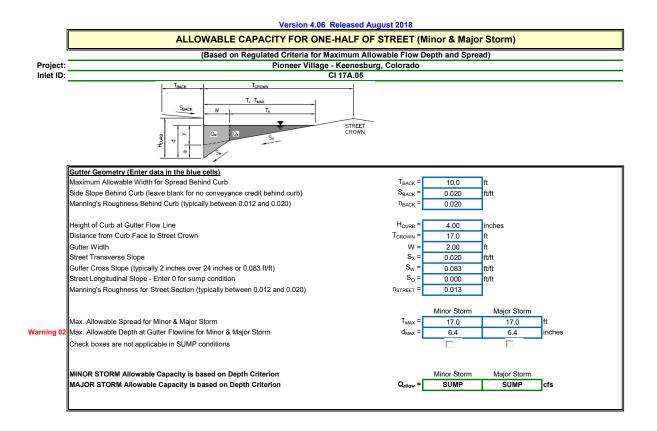


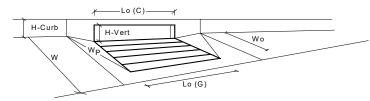




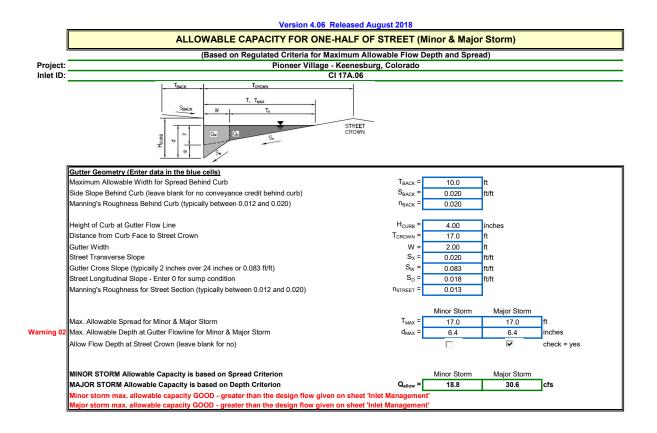


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	9.0	19.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	8.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	70	%



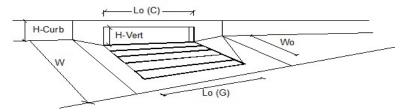


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	7
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	5.00	5.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	9.0	9.0	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	1
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	1
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.58	0.58	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.85	0.85	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.93	0.93	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	34.3	34.3	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	8.4	23.8	cfs

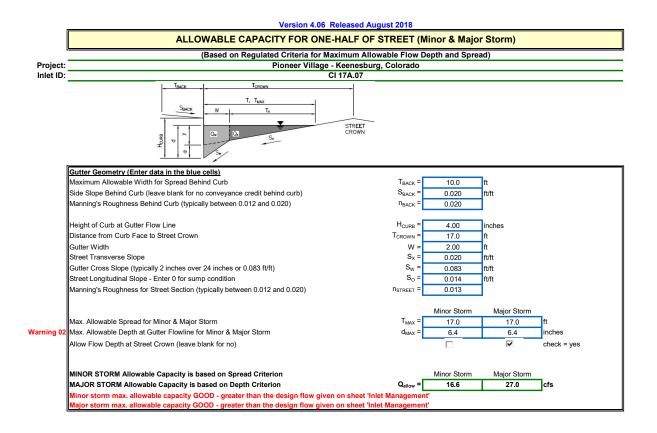






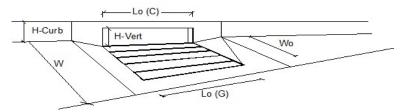


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	10.4	20.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	6.9	cfs
Capture Percentage = Q₂/Q₀ =	С% =	99	75	%

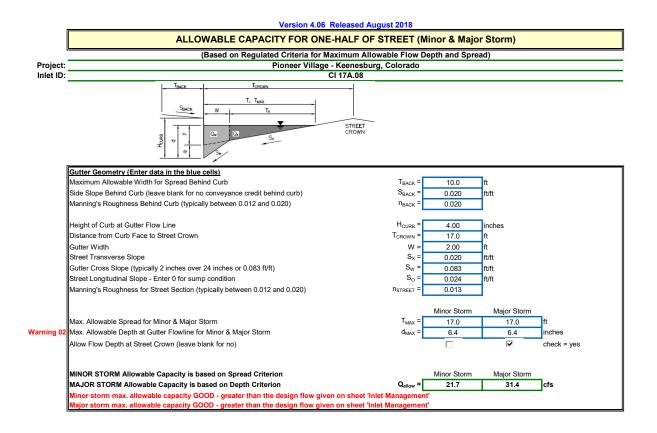






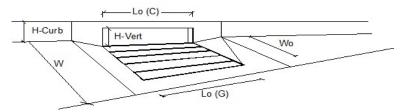


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.4	12.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	3.0	cfs
Capture Percentage = Q _a /Q _o =	С% =	100	80	%

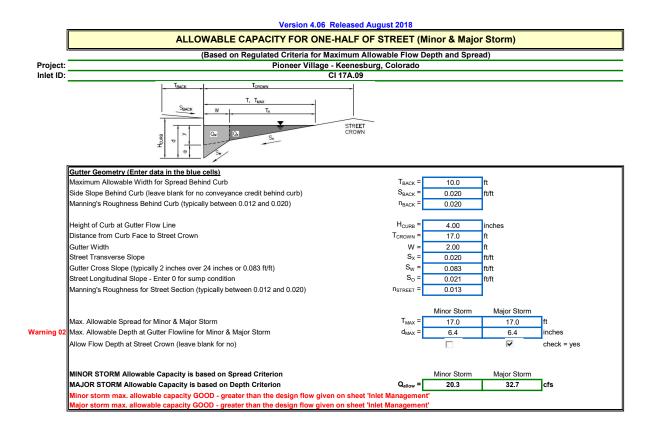






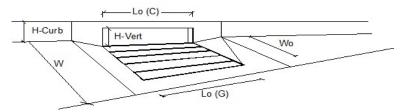


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.4	5.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	С% =	100	100	%

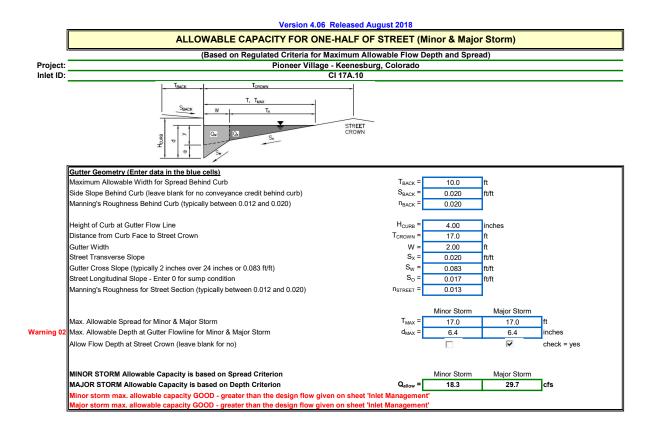






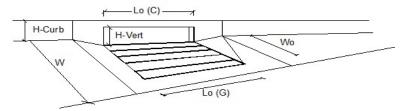


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.1	7.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q₀ =	C% =	100	100	%

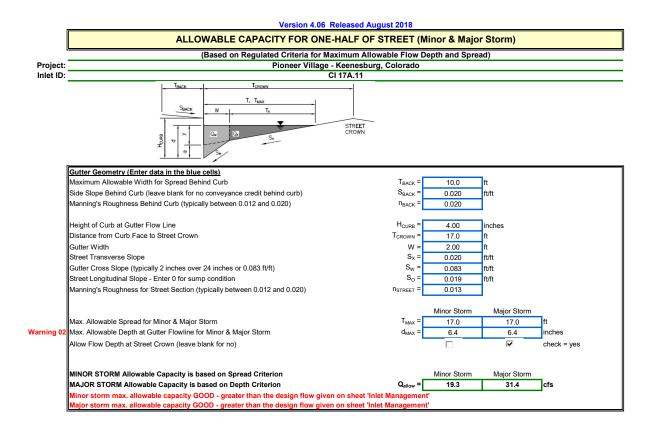






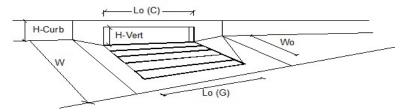


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	7.0	16.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	2.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	88	%

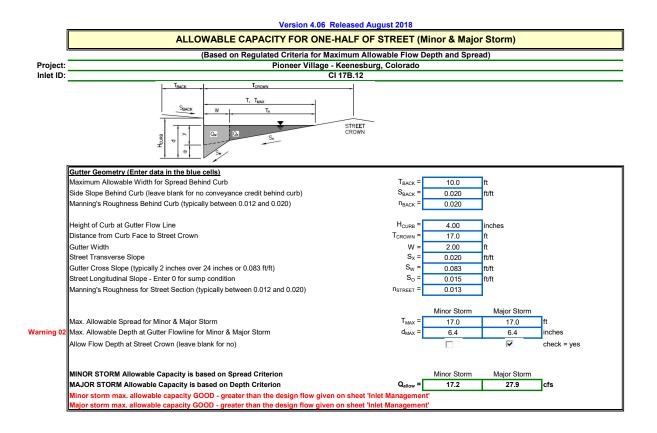






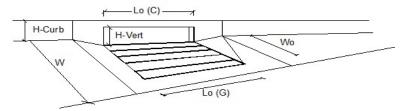


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	5.7	11.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.8	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	86	%

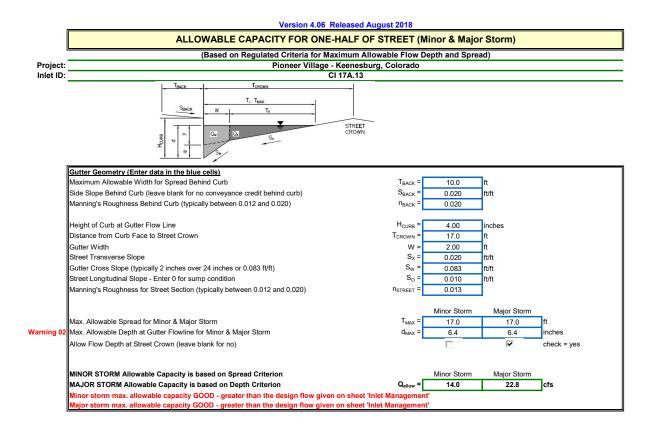






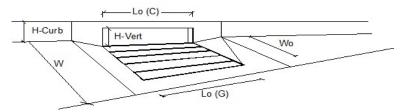


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	7.3	15.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	2.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	89	%

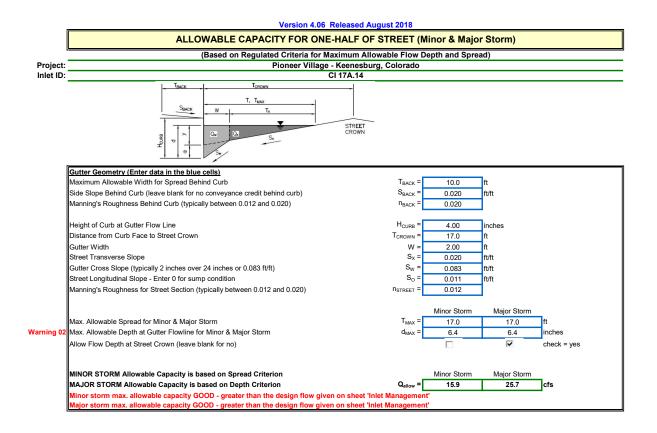






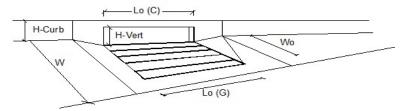


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.8	8.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.4	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	96	%







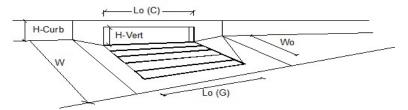


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.7	12.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.7	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	95	%

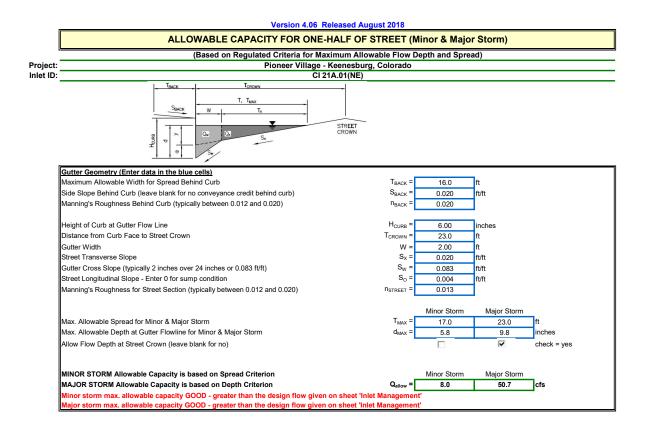
	ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)						
I	(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)						
ject:		Keenesburg, Colorado					
t ID:		21B.13					
		STREET CROWN					
	Httee	GROWN					
	Gutter Geometry (Enter data in the blue cells) Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	10.0	ft			
	Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft			
	Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020				
	Height of Curb at Gutter Flow Line	H _{CURB} =	4.00	inches			
	Distance from Curb Face to Street Crown	T _{CROWN} =	17.0	ft			
	Gutter Width	W =	2.00	ft			
	Street Transverse Slope	s _x =	0.020	ft/ft			
	Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _W =		ft/ft			
	Street Longitudinal Slope - Enter 0 for sump condition	S _o =	0.008	ft/ft			
	Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{STREET} =	0.013	1			
			Minor Storm	Major Storm			
	Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	17.0	17.0	ft		
ng 02	Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	6.4	6.4	inches		
	Allow Flow Depth at Street Crown (leave blank for no)				check = yes		
	Maximum Capacity for 1/2 Street based On Allowable Spread		Minor Storm	Major Storm			
	Water Depth without Gutter Depression (Eq. ST-2)	y =	4.08	4.08	inches		
	Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	d _c =	2.0	2.0	inches		
	Gutter Depression (d _c - (W * S _x * 12))	a =	1.51	1.51	inches		
	Water Depth at Gutter Flowline	d =	5.59	5.59	inches		
	Allowable Spread for Discharge outside the Gutter Section W (T - W)	T _X =	15.0	15.0	ft		
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E _o =	0.350	0.350			
	Discharge outside the Gutter Section W, carried in Section T_X	Q _X =	7.5	7.5	cfs		
	Discharge within the Gutter Section W ($Q_T - Q_X$)	Q _W =	4.1	4.1	cfs		
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.6	0.6	cfs		
	Maximum Flow Based On Allowable Spread	Q _T =	12.1	12.1	cfs		
	Flow Velocity within the Gutter Section	V =	5.3	5.3	fps		
	V*d Product: Flow Velocity times Gutter Flowline Depth	V*d =	2.5	2.5			
	Maximum Capacity for 1/2 Street based on Allowable Depth		Minor Storm	Major Storm			
	Theoretical Water Spread	Т _{тн} =		20.4	ft		
	Theoretical Spread for Discharge outside the Gutter Section W (T - W)	T _{XTH} =	18.4	18.4	ft		
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E ₀ =	0.291	0.291	-		
	Theoretical Discharge outside the Gutter Section W, carried in Section T _{X TH}	Q _{X TH} =	12.9	12.9	cfs		
	Actual Discharge outside the Gutter Section W, (limited by distance T_{CROWN})	Q _X =	12.8	12.8	cfs		
	Discharge within the Gutter Section W ($Q_d - Q_X$)	Q _W =	5.3	5.3	cfs		
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	1.7	1.7	cfs		
	Total Discharge for Major & Minor Storm (Pre-Safety Factor)	Q =	19.7	19.7	cfs		
	Average Flow Velocity Within the Gutter Section	V = V*d =	5.9	5.9	tps		
	V*d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d ≥ 6") Storm	V^d = R =	3.1 1.00	3.1 1.00			
	Max Flow Based on Allowable Depth (Safety Factor Applied)	R = Q _d =	1.00 19.7	1.00 19.7	cfs		
	Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)		6.40	6.40	inches		
	Resultant Flow Depth at Street Crown (Safety Factor Applied)	d _{CROWN} =	0.81	0.81	inches		
				Malan Otam			
	IMINOR STORM Allowable Capacity is based on Spread Criterion		Minor Storm	IVIAIOF Storm			
	MINOR STORM Allowable Capacity is based on Spread Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion	Q _{allow} =	Minor Storm 12.1	Major Storm 19.7	cfs		





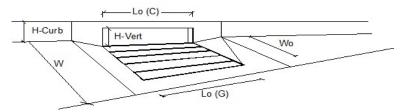


CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.4	3.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

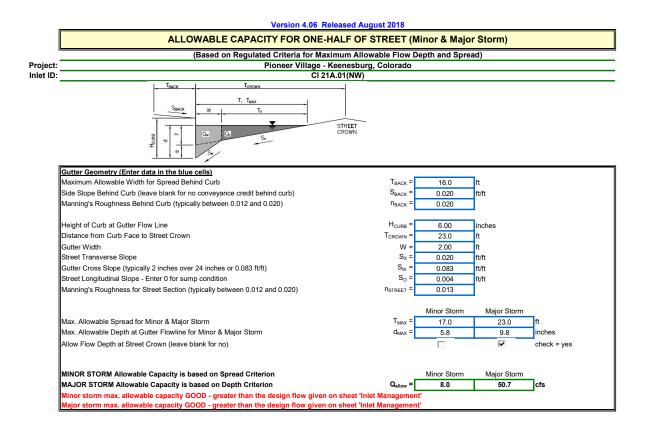






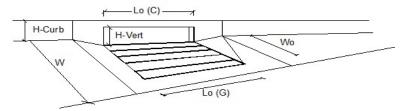


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	4.1	9.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	С% =	100	100	%

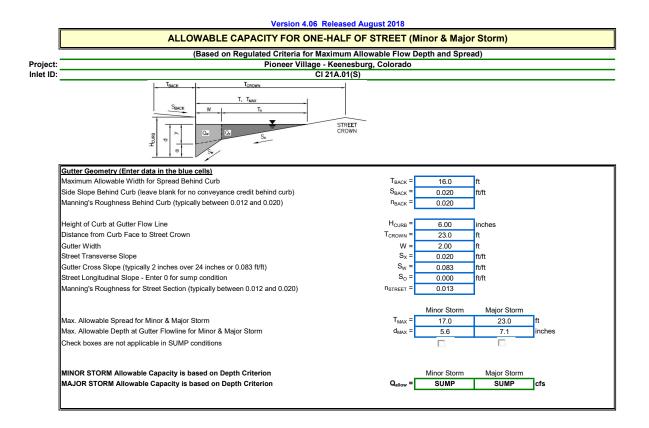






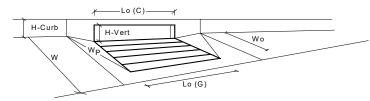


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	4.7	10.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	97	%

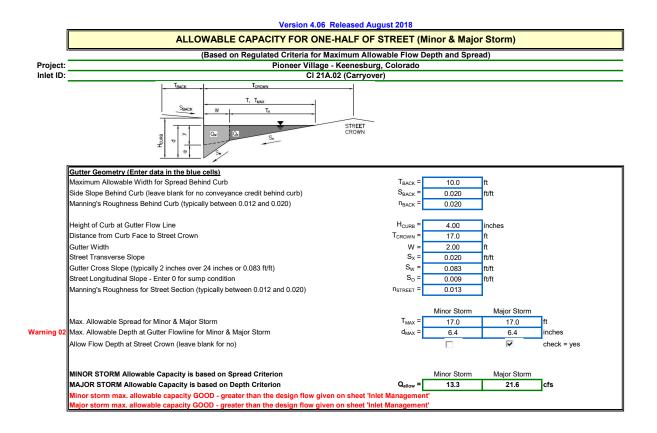


INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018

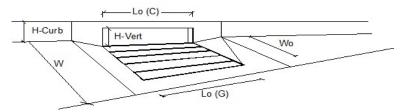


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	7.1	inches
Grate Information		MINOR	MAJOR	Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	20.00	20.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.43	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.67	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.76	0.85	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
		MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	10.3	19.4	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	8.3	19.1	cfs

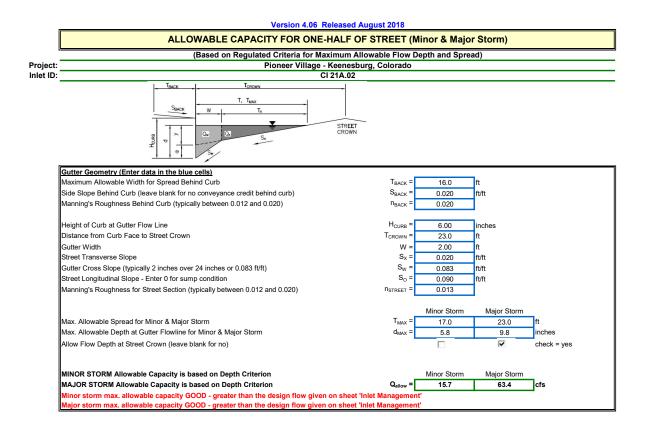






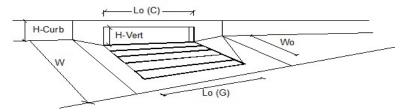


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.0	5.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	0	100	%

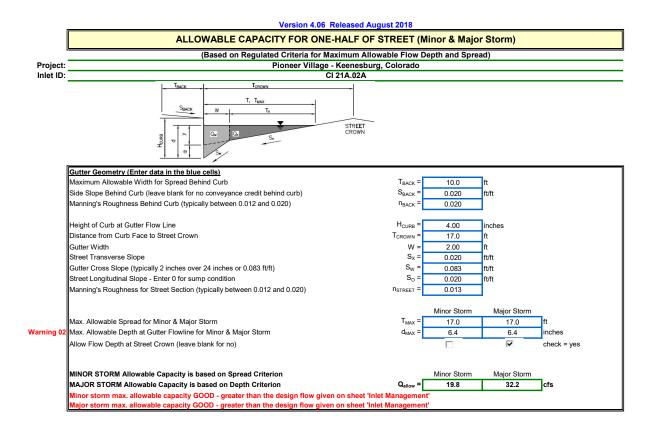






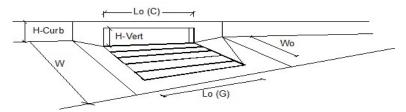


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	3.0	3.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	9.6	17.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	5.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	78	%

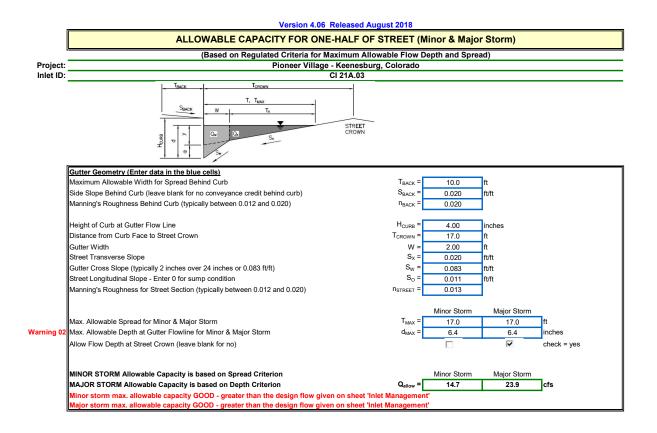






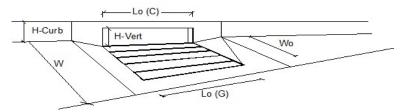


Design Information (Input)	Ĩ	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr−G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.0	3.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

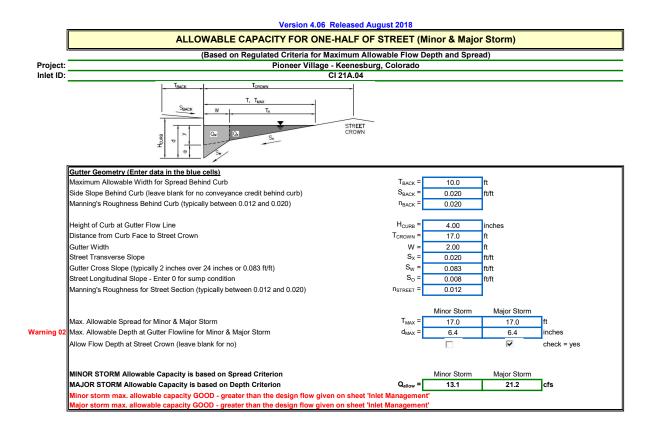






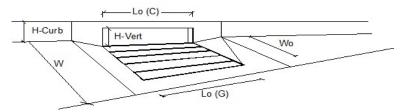


Design Information (Input)		MINOR	MAJOR	
Type of Inlet CDOT Type R Curb Opening	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	4.2	9.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.8	cfs
Capture Percentage = Q _a /Q _o =	С% =	100	92	%

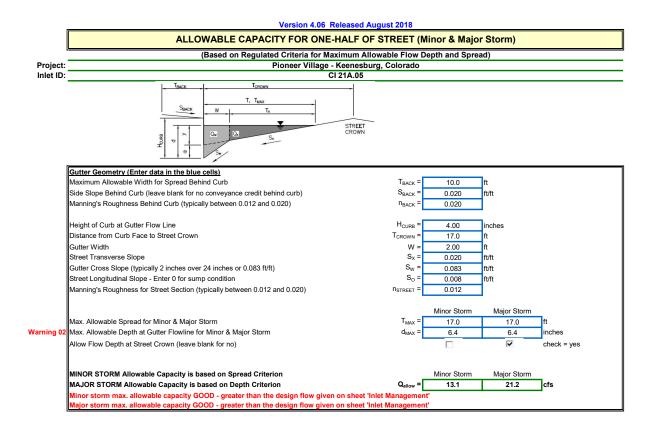






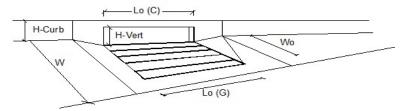


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	4.3	9.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.8	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	92	%

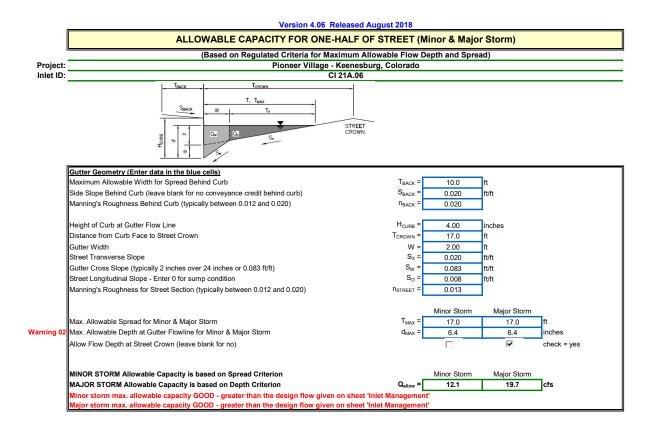






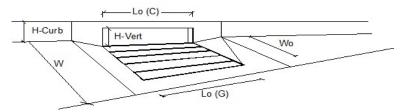


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr−G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	6.0	11.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	2.7	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	81	%

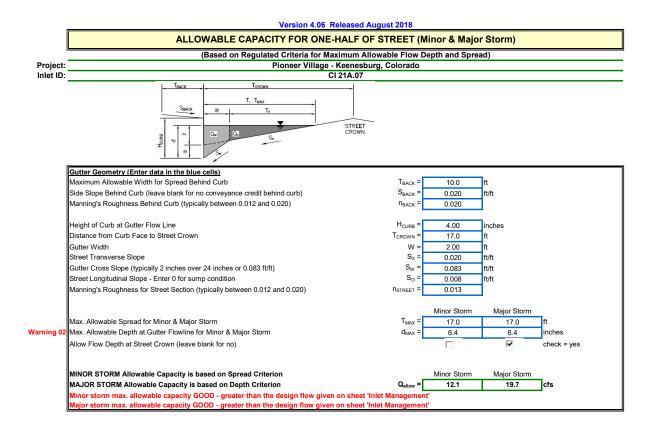






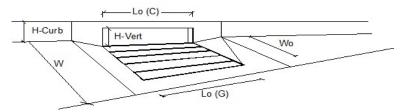


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.0	6.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	1.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	84	%

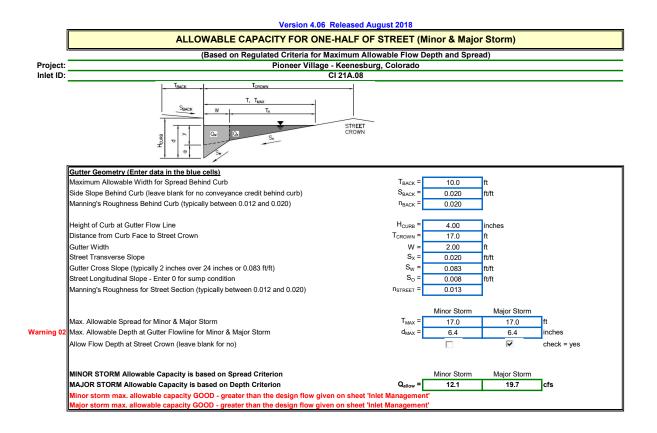






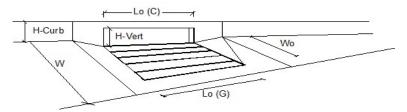


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.3	8.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	96	%

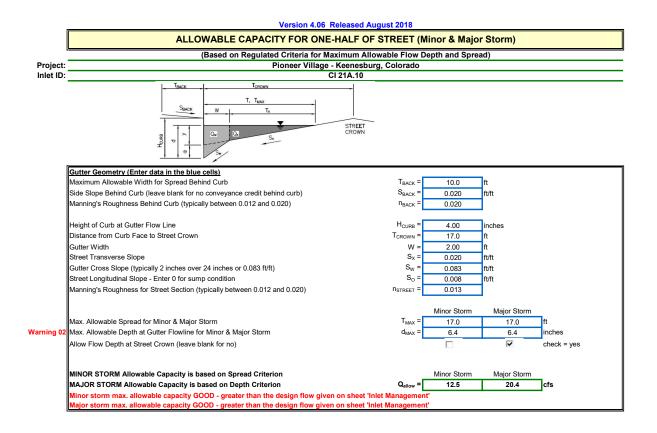






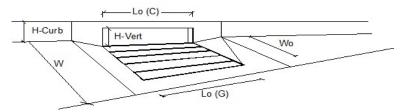


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	4.0	9.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	91	%

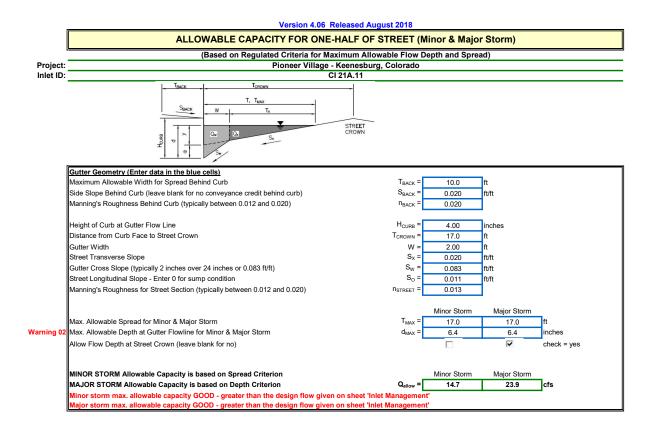






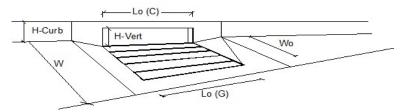


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	6.2	11.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	3.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	99	79	%

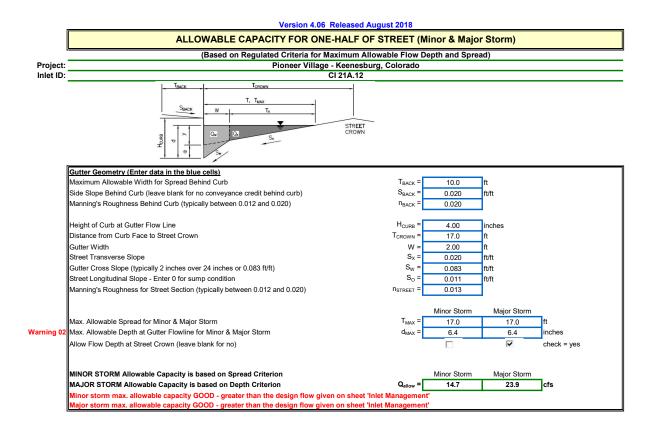






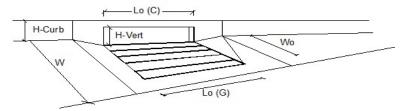


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.1	9.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.7	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	93	%

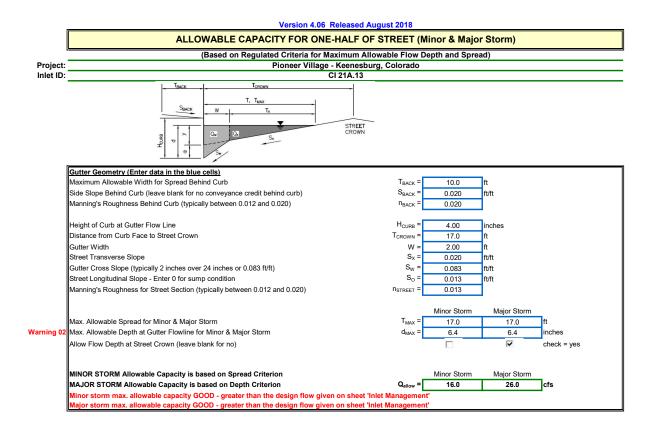






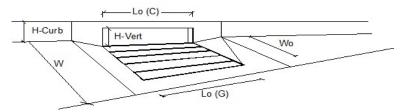


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	6.4	11.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	2.8	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	81	%

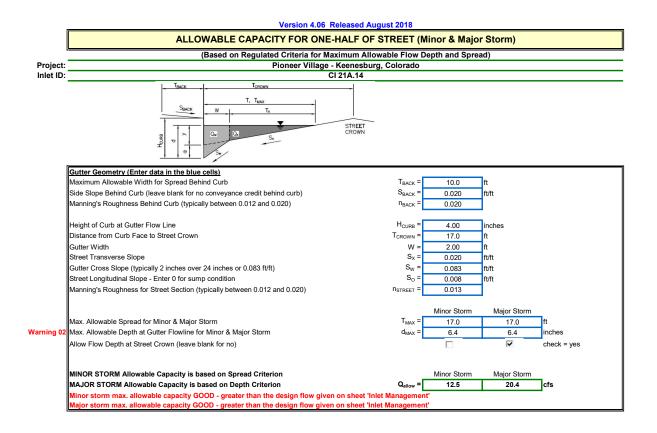






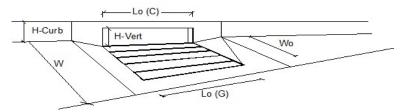


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.8	8.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	97	%

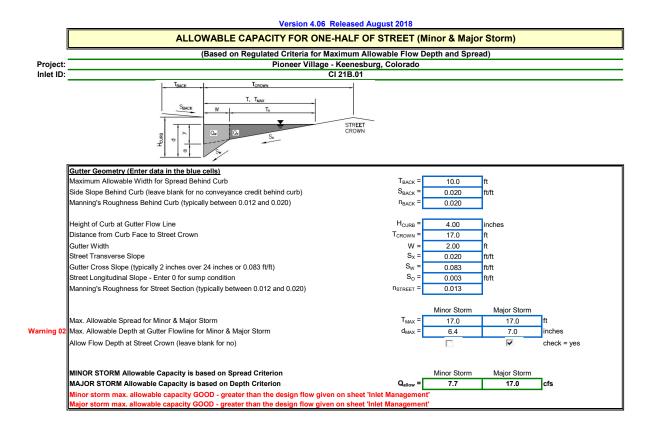






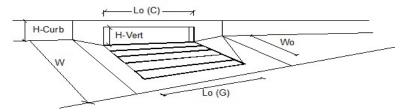


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.4	5.8	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q₀/Q₀ =	C% =	100	99	%

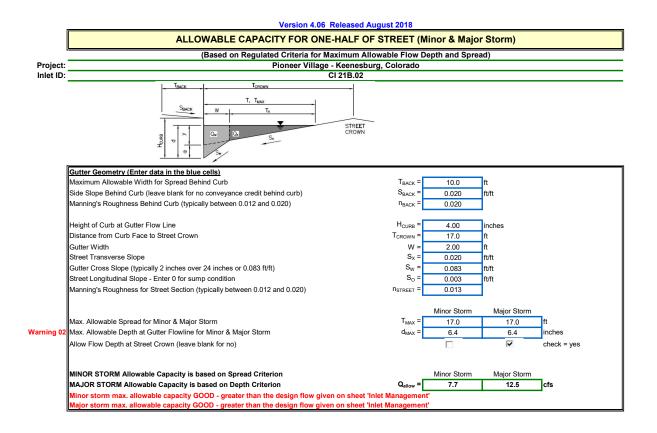






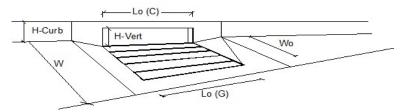


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.5	11.9	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	1.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	97	91	%

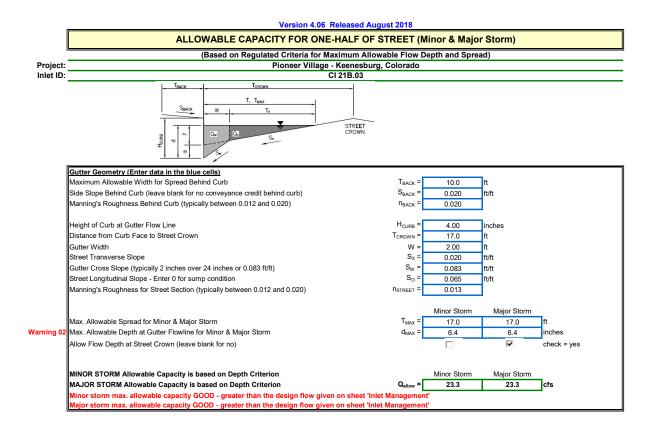






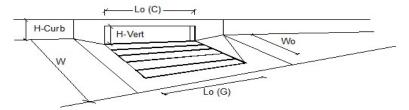


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.9	6.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	96	%

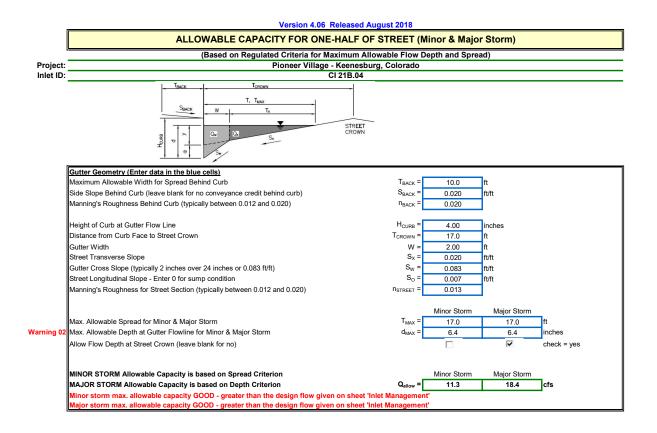






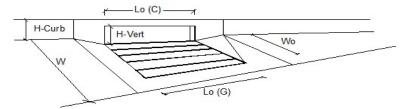


CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.5	8.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

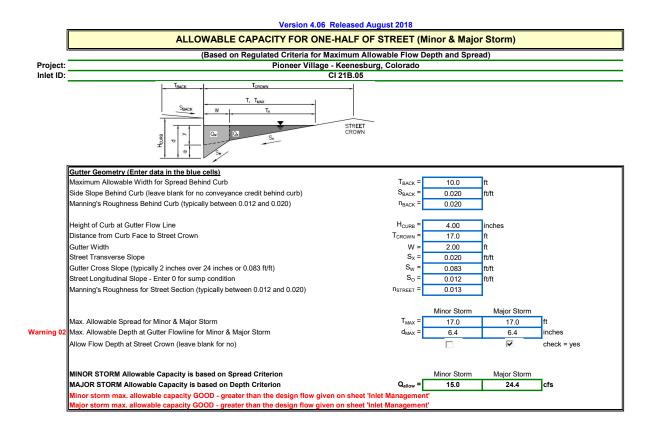






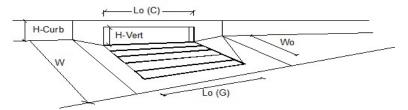


CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	3.6	8.1	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.3	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	96	%

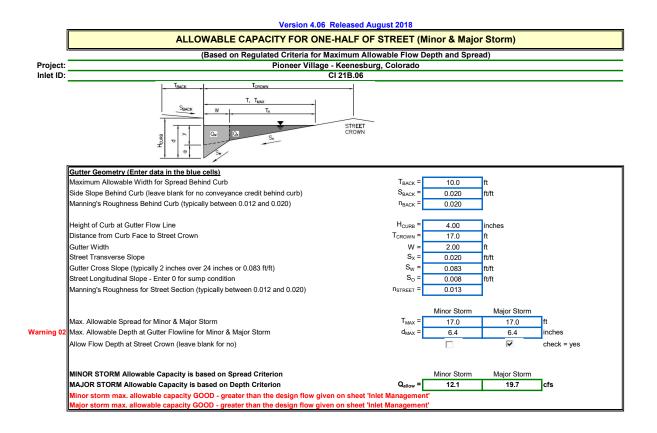






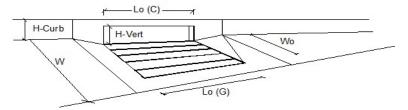


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.7	4.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

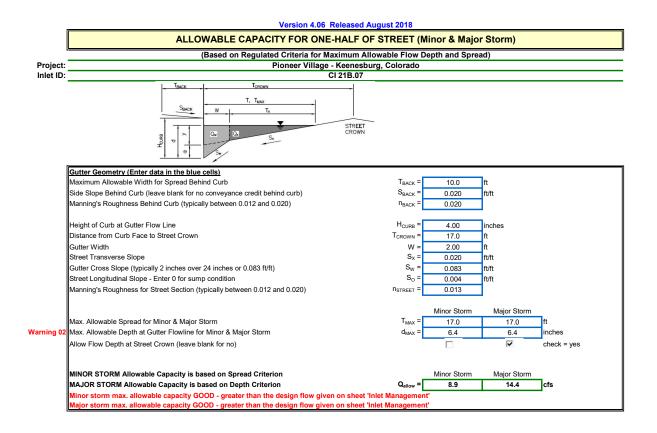






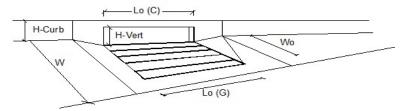


Design Information (Input)	Ĩ	MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	5.00	5.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr−G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.6	1.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%







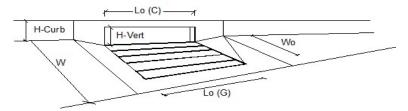


CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	1.5	4.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	98	%

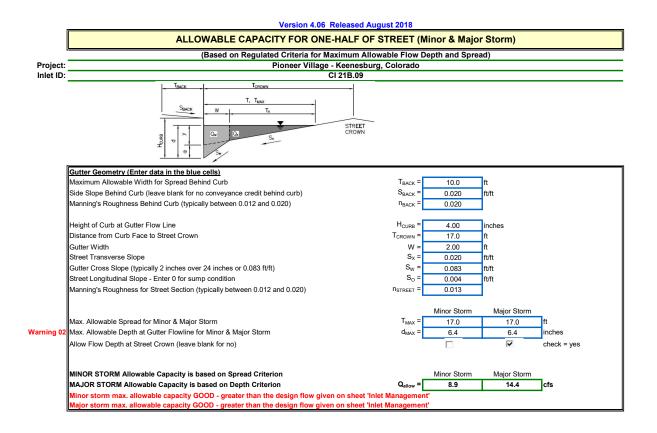
	ALLOWABLE CAPACITY FOR ONE	-HALF OF STREET (Minor & Majo	r Storm)			
	Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)						
oject: et ID:		- Keenesburg, Colorado CI 21B.08					
	TBACK TCROWN						
	T, T _{MAX}						
	Seack W Tx						
		STREET					
		CROWN					
	P S						
	Gutter Geometry (Enter data in the blue cells)						
	Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	10.0	ft			
	Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft			
	Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020				
	Height of Curb at Gutter Flow Line	H _{CURB} =	4.00	inches			
	Distance from Curb Face to Street Crown	T _{CROWN} =	17.0	ft			
	Gutter Width	W =		ft			
	Street Transverse Slope	S _X =		ft/ft			
	Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _w =		ft/ft			
	Street Longitudinal Slope - Enter 0 for sump condition	S _o =		ft/ft			
	Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{STREET} =	0.013	1			
		-	Minor Storm	Major Storm			
	Max. Allowable Spread for Minor & Major Storm	T _{MAX} =		17.0	ft		
ing 02	Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =		6.4	inches		
	Allow Flow Depth at Street Crown (leave blank for no)				check = yes		
	Maximum Capacity for 1/2 Street based On Allowable Spread		Minor Storm	Major Storm			
	Water Depth without Gutter Depression (Eq. ST-2)	y =		4.08	inches		
	Vertical Depth between Gutter Lip and Gutter Flowline (usually 2") Gutter Depression (d_c - (W * S _x * 12))	d _C = a =		2.0	inches inches		
	Water Depth at Gutter Flowline	a - d =	1.51 5.59	1.51 5.59	inches		
	Allowable Spread for Discharge outside the Gutter Section W (T - W)	u - T _x =		15.0	ft		
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	Ê0 =		0.350	-		
	Discharge outside the Gutter Section W, carried in Section T_X	Q _x =		75.2	cfs		
	Discharge within the Gutter Section W $(Q_T - Q_X)$	Q _w =	40.5	40.5	cfs		
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =		5.6	cfs		
	Maximum Flow Based On Allowable Spread	Q _T =		121.3	cfs		
	Flow Velocity within the Gutter Section	V =	52.9	52.9	fps		
	V*d Product: Flow Velocity times Gutter Flowline Depth	V*d =	24.7	24.7			
	Maximum Capacity for 1/2 Street based on Allowable Depth		Minor Storm	Major Storm			
	Theoretical Water Spread	T _{TH} =	20.4	20.4	ft		
	Theoretical Spread for Discharge outside the Gutter Section W (T - W)	Т _{х тн} =	18.4	18.4	ft		
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E _o =	0.291	0.291			
	Theoretical Discharge outside the Gutter Section W, carried in Section T_{XTH}	Q _{X TH} =	129.1	129.1	cfs		
	Actual Discharge outside the Gutter Section W, (limited by distance T _{CROWN})	Q _X =		127.7	cfs		
	Discharge within the Gutter Section W (Q _d - Q _X)	Q _W =	53.0	53.0	cfs		
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	16.6	16.6	cfs		
	Total Discharge for Major & Minor Storm (Pre-Safety Factor)	Q =		197.3	cfs		
	Average Flow Velocity Within the Gutter Section	V =	58.8	58.8	fps		
	V*d Product: Flow Velocity Times Gutter Flowline Depth	V*d =		31.4			
		R=		0.06	cfs		
	Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \ge 6^{\circ}$) Storm		11.2	11.2	inches		
	Max Flow Based on Allowable Depth (Safety Factor Applied)	Q _d =	2.87				
		Qd = d = d _{CROWN} =		2.87 0.00	inches		
	Max Flow Based on Allowable Depth (Safety Factor Applied) Resultant Flow Depth at Gutter Flowline (Safety Factor Applied) Resultant Flow Depth at Street Crown (Safety Factor Applied)	d =	0.00	0.00	inches		
	Max Flow Based on Allowable Depth (Safety Factor Applied) Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	d =	0.00 Minor Storm		inches		



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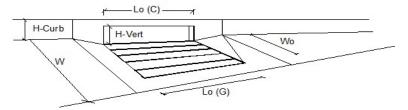


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.6	6.7	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

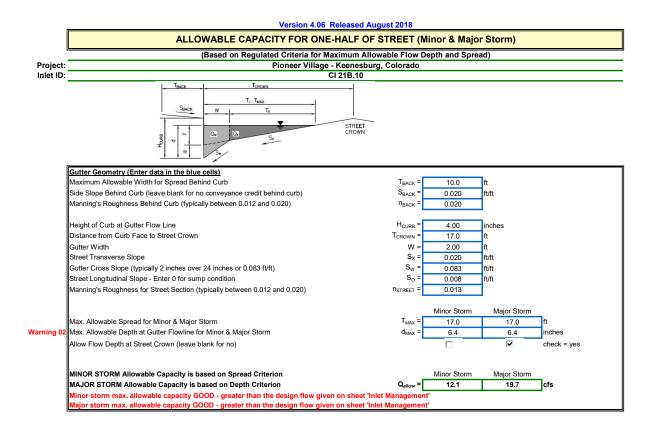






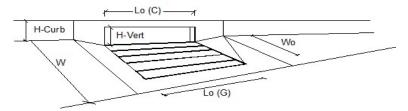


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	20.00	20.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	4.3	11.2	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.8	cfs
Capture Percentage = Q _a /Q₀ =	C% =	99	93	%

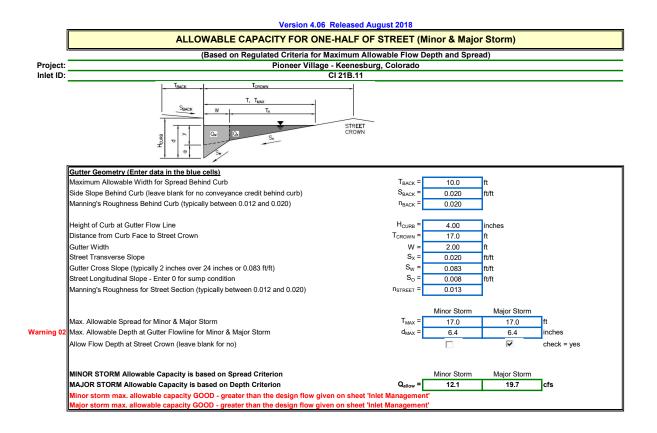




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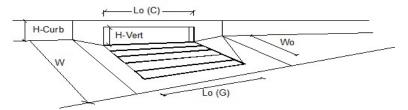


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	2.7	5.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.6	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	90	%







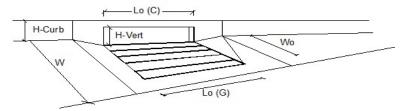


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.7	4.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

10		ximum Allowable Flow I Keenesburg, Colorado I 21B.12	Depth and Spre	ad)	
ilet ID:	C				
-		1218.12			
		STREET CROWN			
	H H H H H H H H H H H H H H H H H H H				
	Gutter Geometry (Enter data in the blue cells)	-		1.	
	Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	10.0	ft	
	Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft	
ľ	Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020	1	
	Height of Curb at Gutter Flow Line	H _{CURB} =	4.00	inches	
	Distance from Curb Face to Street Crown	T _{CROWN} =	17.0	ft	
	Gutter Width	W =	2.00	ft	
	Street Transverse Slope	S _X =	0.020	ft/ft	
	Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _W =	0.083	ft/ft	
	Street Longitudinal Slope - Enter 0 for sump condition	S _o =	0.008	ft/ft	
	Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{STREET} =	0.020		
			Minor Storm	Major Storm	
I	Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	17.0	17.0	ft
ning 02	Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	6.4	6.4	inches
ŀ	Allow Flow Depth at Street Crown (leave blank for no)			V	check = yes
	Maximum Capacity for 1/2 Street based On Allowable Spread		Minor Starm	Majar Starm	
	Water Depth without Gutter Depression (Eq. ST-2)	v =	Minor Storm 4.08	Major Storm 4.08	inches
	Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	y = d _C =	2.0	2.0	inches
	Gutter Depression ($d_c - (W * S_x * 12)$)	a =	1.51	1.51	inches
	Water Depth at Gutter Flowline	d =	5.59	5.59	inches
	Allowable Spread for Discharge outside the Gutter Section W (T - W)	т _х =	15.0	15.0	ft
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E ₀ =	0.350	0.350	-
	Discharge outside the Gutter Section W, carried in Section T _x	Q _x =	4.9	4.9	cfs
	Discharge within the Gutter Section W ($Q_T - Q_X$)	Q _W =	2.6	2.6	cfs
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.6	0.6	cfs
1	Maximum Flow Based On Allowable Spread	Q _T =	8.1	8.1	cfs
1	Flow Velocity within the Gutter Section	V =	3.4	3.4	fps
ľ	V*d Product: Flow Velocity times Gutter Flowline Depth	V*d =	1.6	1.6	
	Maximum Capacity for 1/2 Street based on Allowable Depth		Minor Storm	Major Storm	
	Theoretical Water Spread	Т _{тн} =	20.4	20.4	ft
	Theoretical Spread for Discharge outside the Gutter Section W (T - W)	Т _{х тн} =	18.4	18.4	ft
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E _o =	0.291	0.291	
ŀ	Theoretical Discharge outside the Gutter Section W, carried in Section T_{XTH}	Q _{X TH} =	8.4	8.4	cfs
	Actual Discharge outside the Gutter Section W, (limited by distance T_{CROWN})	Q _X =	8.3	8.3	cfs
	Discharge within the Gutter Section W $(Q_d - Q_X)$	Q _W =	3.4	3.4	cfs
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	1.7	1.7	cfs
ŀ	Total Discharge for Major & Minor Storm (Pre-Safety Factor)	Q =	13.4	13.4	cfs
ŀ	Average Flow Velocity Within the Gutter Section	V =	3.8	3.8	fps
	V*d Product: Flow Velocity Times Gutter Flowline Depth	V*d =	2.0	2.0	4
	Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \ge 6$ ") Storm	R=	1.00	1.00	
	Max Flow Based on Allowable Depth (Safety Factor Applied)	Q _d =	13.4	13.4	cfs
	Resultant Flow Depth at Gutter Flowline (Safety Factor Applied) Resultant Flow Depth at Street Crown (Safety Factor Applied)	d = d _{CROWN} =	6.40 0.81	6.40 0.81	inches inches
	·	-chown	0.01	0.01	
	MINOR STORM Allowable Capacity is based on Spread Criterion		Minor Storm	Major Storm	
	MAJOR STORM Allowable Capacity is based on Depth Criterion Minor storm max. allowable capacity GOOD - greater than the design flow given	Q _{allow} =	8.1	13.4	cfs





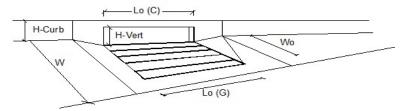


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr−G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.9	4.3	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	98	%

	ALLOWABLE CAPACITY FOR ONE-HA	LF OF STREET (M	/linor & Majo	r Storm)	
	(Based on Regulated Criteria for Maxim	um Allowable Flow I	Depth and Spre	ad)	
roject:	Pioneer Village - Kee CI 21				
nlet ID:		B.14			
	Seace W Tx	TREET			
	H P P S				
	Gutter Geometry (Enter data in the blue cells)	-		1.	
	Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	10.0	ft	
	Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft	
	Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020	1	
	Height of Curb at Gutter Flow Line	H _{CURB} =	4.00	inches	
	Distance from Curb Face to Street Crown	T _{CROWN} =	17.0	ft	
	Gutter Width	W =	2.00	ft	
	Street Transverse Slope	S _X =	0.020	ft/ft	
	Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _W =	0.083	ft/ft	
	Street Longitudinal Slope - Enter 0 for sump condition	S _o =	0.750	ft/ft	
	Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{STREET} =	0.013	1	
	May Allewahle Coreed for Minor 9 Major Storm	т -	Minor Storm	Major Storm	
mina 02	Max. Allowable Spread for Minor & Major Storm	T _{MAX} = d _{MAX} =	17.0	17.0 6.4	ft inches
ning 02	Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	UMAX -	6.4	0.4	
	Allow Flow Depth at Street Crown (leave blank for no)				check = yes
	Maximum Capacity for 1/2 Street based On Allowable Spread		Minor Storm	Major Storm	
	Water Depth without Gutter Depression (Eq. ST-2)	y =	4.08	4.08	inches
	Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	d _c =	2.0	2.0	inches
	Gutter Depression (d _c - (W * S _x * 12))	a =	1.51	1.51	inches
	Water Depth at Gutter Flowline	d =	5.59	5.59	inches
	Allowable Spread for Discharge outside the Gutter Section W (T - W)	T _X =	15.0	15.0	ft
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E _o =	0.350	0.350	
	Discharge outside the Gutter Section W, carried in Section T _x	Q _X =	75.2	75.2	cfs
	Discharge within the Gutter Section W $(Q_T - Q_X)$	Q _W =	40.5	40.5	cfs
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	5.6	5.6	cfs
	Mandanana Flam Daard On Allamakia Onesad			121.3	cfs
	Maximum Flow Based On Allowable Spread	Q _T =	121.3		
	Flow Velocity within the Gutter Section	Q _T = V =	121.3 52.9	52.9	fps
	-				
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth	V =	52.9 24.7	52.9 24.7	
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth	V = V*d =	52.9 24.7 Minor Storm	52.9 24.7 Major Storm	fps
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread	V = V*d = T _{TH} =	52.9 24.7 Minor Storm 20.4	52.9 24.7 Major Storm 20.4	fps ft
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W)	V = V*d = Т _{ТН} = Т _{Х ТН} =	52.9 24.7 Minor Storm 20.4 18.4	52.9 24.7 Major Storm 20.4 18.4	fps
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	V = V*d = Т _{ттн} = Т _{х тн} = Е _о =	52.9 24.7 Minor Storm 20.4 18.4 0.291	52.9 24.7 Major Storm 20.4 18.4 0.291	fps ft ft
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{X TH}	V = V*d = T _{TH} = T _{XTH} = E ₀ = Q _{XTH} =	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1	fps ft ft cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{XTH} Actual Discharge outside the Gutter Section W, (limited by distance T _{CROWN})	$V = V^*d =$ $T_{TH} =$ $T_{XTH} =$ $E_0 =$ $Q_{XTH} =$ $Q_X =$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7	fps ft ft cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{X TH} Actual Discharge outside the Gutter Section W, (Imitted by distance T _{CROWN}) Discharge within the Gutter Section W (Q _d - Q _x)	$V = V^* d = T_{TTH} = T_{XTH} = E_O = Q_{XTH} = Q_{YTH} = Q_{YTH$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7 53.0	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0	fps ft ft cfs cfs cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{x TH} Actual Discharge outside the Gutter Section W, (limited by distance T _{CROWN}) Discharge within the Gutter Section W (Q _d - Q _x) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	$V = V^* d =$ $T_{TH} =$ $T_{XTH} =$ $E_0 =$ $Q_{XTH} =$ $Q_W =$ $Q_{BACK} =$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6	fps ft ft cfs cfs cfs cfs cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{XTH} Actual Discharge outside the Gutter Section W (Q _d - Q _x) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor)	$V = V^* d = T_{TTH} = T_{XTH} = E_O = Q_{XTH} = Q_{YTH} = Q_{YTH$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3	fps ft ft cfs cfs cfs cfs cfs cfs cfs cfs cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{X TH} Actual Discharge outside the Gutter Section W, carried in Section T _{X TH} Actual Discharge outside the Gutter Section W ($Q_d - Q_X$) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section	$V = V^* d = V^* d = T_{TTH} = E_0 = Q_{TTH} = Q_X = Q_{W} = Q_{BACK} = Q_{BACK} = Q = V = V = V = V = V = V = V = V = V$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8	fps ft ft cfs cfs cfs cfs cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{X TH} Actual Discharge outside the Gutter Section W, (Imitted by distance T _{CROWN}) Discharge within the Gutter Section W ($Q_d - Q_x$) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V*d Product: Flow Velocity Times Gutter Flowline Depth	$V = V^* d = V^* d = T_{TTH} = E_0 = Q_{TTH} = Q_X TH = Q_X TH = Q_X = Q_{BACK} = Q_BACK = Q = V = V^* d = V^* V^* V = V^$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4	fps ft ft cfs cfs cfs cfs cfs cfs cfs cfs cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{x TH} Actual Discharge outside the Gutter Section W, (limited by distance T _{CROWN}) Discharge within the Gutter Section W (Q _d - Q _x) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge flow Velocity Within the Gutter Section V*d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d ≥ 6") Storm	$V = V^* d =$ $T_{TH} =$ $T_{XTH} =$ $E_0 =$ $Q_{XTH} =$ $Q_{W} =$ $Q_{BACK} =$ $Q =$ $V =$ $V^* d =$ $R =$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06	fps ft ft cfs cfs cfs cfs cfs cfs cfs fps
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{XTH} Actual Discharge outside the Gutter Section W, (Imited by distance T _{CROWN}) Discharge within the Gutter Section W ($Q_4 - Q_X$) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V*d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d $\geq 6^*$) Storm Max Flow Based on Allowable Depth (Safety Factor Applied)	$V = V^* d =$ $T_{TH} =$ $T_{XTH} =$ $C_0 =$ $Q_{XTH} =$ $Q_W =$ $Q_{BACK} =$ $Q =$ $V =$ $V^* d =$ $R =$ $Q_d =$ $Q_d =$	52.9 24.7 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06 11.2	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06 11.2	fps ft ft cfs cfs cfs cfs cfs cfs cfs cfs cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T_{XTH} Actual Discharge outside the Gutter Section W, carried in Section T_{XTH} Actual Discharge outside the Gutter Section W ($Q_a - Q_x$) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V"d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d \geq 6") Storm Max Flow Based on Allowable Depth (Safety Factor Applied) Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	$V = V^*d = V^*d = T_{TH} = E_0 = Q_{XTH} = Q_X = Q_{ACK} = Q_{ACK} = Q_{ACK} = V = V^*d = R = Q_d = Q_d = Q_d = d = d = d$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06 11.2 2.87	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06	fps ft ft cfs cfs cfs cfs cfs cfs cfs fps
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T _{XTH} Actual Discharge outside the Gutter Section W, (Imited by distance T _{CROWN}) Discharge within the Gutter Section W ($Q_4 - Q_X$) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V*d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d $\geq 6^*$) Storm Max Flow Based on Allowable Depth (Safety Factor Applied)	$V = V^* d =$ $T_{TH} =$ $T_{XTH} =$ $C_0 =$ $Q_{XTH} =$ $Q_W =$ $Q_{BACK} =$ $Q =$ $V =$ $V^* d =$ $R =$ $Q_d =$ $Q_d =$	52.9 24.7 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06 11.2	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06 111.2 2.87	fps ft ft cfs cfs cfs cfs cfs cfs cfs cfs cfs cfs
	Flow Velocity within the Gutter Section V*d Product: Flow Velocity times Gutter Flowline Depth Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7) Theoretical Discharge outside the Gutter Section W, carried in Section T_{XTH} Actual Discharge outside the Gutter Section W, carried in Section T_{XTH} Actual Discharge outside the Gutter Section W ($Q_a - Q_x$) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V"d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d \geq 6") Storm Max Flow Based on Allowable Depth (Safety Factor Applied) Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	$V = V^*d = V^*d = T_{TH} = E_0 = Q_{XTH} = Q_X = Q_{ACK} = Q_{ACK} = Q_{ACK} = V = V^*d = R = Q_d = Q_d = Q_d = d = d = d$	52.9 24.7 Minor Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06 11.2 2.87	52.9 24.7 Major Storm 20.4 18.4 0.291 129.1 127.7 53.0 16.6 197.3 58.8 31.4 0.06 111.2 2.87	fps ft ft cfs cfs cfs cfs cfs cfs cfs cfs cfs cfs





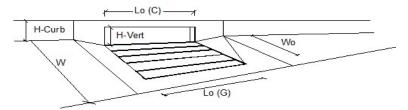


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	1.7	4.0	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.0	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	100	%

	Version 4.06 Released August 2018 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)									
	(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)									
ject:	Pioneer Village - Ke									
et ID:	CI21	B.15								
		STREET CROWN								
	2 0 53									
	Gutter Geometry (Enter data in the blue cells)	Ŧ		٦.						
	Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	10.0	ft						
	Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft						
	Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020							
	Height of Curb at Gutter Flow Line	H _{CURB} =	4.00	inches						
	Distance from Curb Face to Street Crown	T _{CROWN} =	17.0	ft						
	Gutter Width	W =	2.00	ft						
	Street Transverse Slope	S _X =		ft/ft						
	Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _W =		ft/ft						
	Street Longitudinal Slope - Enter 0 for sump condition	S _o =	0.008	ft/ft						
	Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{STREET} =	0.013							
			Minor Storm	Major Storm						
	Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	17.0	17.0	ft					
ng 02	Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	6.4	6.4	inches					
	Allow Flow Depth at Street Crown (leave blank for no)			V	check = yes					
	Mavimum Canadity for 1/2 Street based On Allowable Sureed		Miner Sterm	Majar Ctarm						
	Maximum Capacity for 1/2 Street based On Allowable Spread Water Depth without Gutter Depression (Eq. ST-2)	v -	Minor Storm 4.08	Major Storm 4.08	inches					
	Vertical Depth without Gutter Depression (Eq. 51-2) Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	y = d _c =	2.0	2.0	inches					
	Gutter Depression ($d_c - (W * S_x * 12)$)	a=	1.51	1.51	inches					
	Water Depth at Gutter Flowline	d =	5.59	5.59	inches					
	Allowable Spread for Discharge outside the Gutter Section W (T - W)	u - T _X =	15.0	15.0	ft					
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	Ê0 =	0.350	0.350	-					
	Discharge outside the Gutter Section W, carried in Section T_x	Q _x =		7.5	cfs					
	Discharge within the Gutter Section W ($Q_T - Q_X$)	Q _W =	4.1	4.1	cfs					
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.6	0.6	cfs					
	Maximum Flow Based On Allowable Spread	Q _T =	12.1	12.1	cfs					
	Flow Velocity within the Gutter Section	V =	5.3	5.3	fps					
	V*d Product: Flow Velocity times Gutter Flowline Depth	V*d =	2.5	2.5						
	Maximum Capacity for 1/2 Street based on Allowable Depth		Minor Storm	Major Storm						
	Theoretical Water Spread	T _{TH} =		20.4	ft					
	Theoretical Spread for Discharge outside the Gutter Section W (T - W)	Т _{х тн} =	18.4	18.4	ft					
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	E _o =	0.291	0.291						
	Theoretical Discharge outside the Gutter Section W, carried in Section T_{XTH}	Q _{X TH} =	12.9	12.9	cfs					
		Q _X =	12.8	12.8	cfs					
	Actual Discharge outside the Gutter Section W, (limited by distance T _{CROWN})	-^		5.3	cfs					
	Actual Discharge outside the Gutter Section W, (limited by distance Γ_{CROWN}) Discharge within the Gutter Section W (Q _d - Q _X)	Q _W =	5.3	0.0						
			5.3 1.7	1.7	cfs					
	Discharge within the Gutter Section W $(Q_d - Q_X)$	Q _W =	1.7 19.7		cfs cfs					
	Discharge within the Gutter Section W (Q_d - Q_x) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _W = Q _{BACK} =	1.7	1.7						
	Discharge within the Gutter Section W (Q _d - Q _x) Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V*d Product: Flow Velocity Times Gutter Flowline Depth	Q _W = Q _{BACK} = Q = V = V*d =	1.7 19.7 5.9 3.1	1.7 19.7	cfs					
	Discharge within the Gutter Section W $(Q_d - Q_x)$ Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V'd Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d \geq 6") Storm	Q _W = Q _{BACK} = Q = V = V*d = R =	1.7 19.7 5.9 3.1 1.00	1.7 19.7 5.9 3.1 1.00	cfs fps					
	Discharge within the Gutter Section W $(Q_d - Q_x)$ Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V ⁺ d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d $\geq 6^{\circ}$) Storm Max Flow Based on Allowable Depth (Safety Factor Applied)	Q _W = Q _{BACK} = Q = V = V*d = R = Q _d =	1.7 19.7 5.9 3.1 1.00 19.7	1.7 19.7 5.9 3.1 1.00 19.7	cfs fps cfs					
	Discharge within the Gutter Section W $(Q_d - Q_x)$ Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V*d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \ge 6^{\circ}$) Storm Max Flow Based on Allowable Depth (Safety Factor Applied) Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	Q _W = Q _{BACK} = Q = V = V*d = R = Q_d = d =	1.7 19.7 5.9 3.1 1.00 19.7 6.40	1.7 19.7 5.9 3.1 1.00 19.7 6.40	cfs fps cfs inches					
	Discharge within the Gutter Section W $(Q_d - Q_x)$ Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V ⁺ d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor (d $\geq 6^{\circ}$) Storm Max Flow Based on Allowable Depth (Safety Factor Applied)	Q _W = Q _{BACK} = Q = V = V*d = R = Q _d =	1.7 19.7 5.9 3.1 1.00 19.7	1.7 19.7 5.9 3.1 1.00 19.7	cfs fps cfs					
	Discharge within the Gutter Section W $(Q_d - Q_x)$ Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns) Total Discharge for Major & Minor Storm (Pre-Safety Factor) Average Flow Velocity Within the Gutter Section V*d Product: Flow Velocity Times Gutter Flowline Depth Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \ge 6^{\circ}$) Storm Max Flow Based on Allowable Depth (Safety Factor Applied) Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	Q _W = Q _{BACK} = Q = V = V*d = R = Q_d = d =	1.7 19.7 5.9 3.1 1.00 19.7 6.40 0.81 Minor Storm	1.7 19.7 5.9 3.1 1.00 19.7 6.40	cfs fps cfs inches					



Version 4.06 Released August 2018

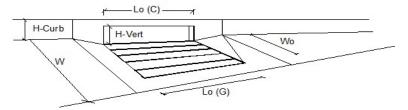


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type F	Curb Opening	7
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	10.00	10.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'	_	MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	2.6	5.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.6	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	91	%

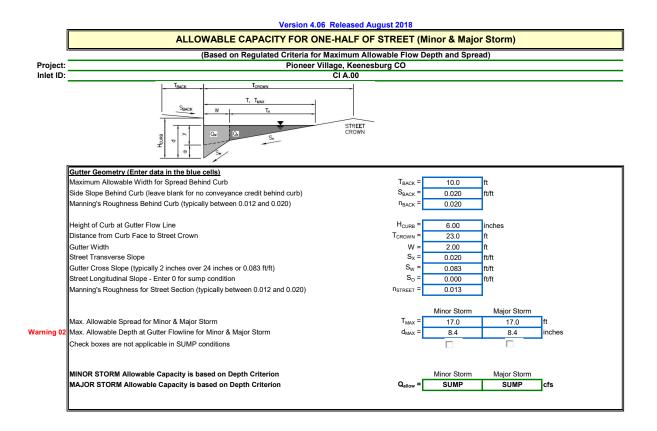
	Version 4.06 Released August 2018 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)									
	(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread)									
oject:		Keenesburg, Colorado 21B.16								
let ID:		218.10								
	SEACK W Tx									
	Provide the second seco	STREET CROWN								
	Gutter Geometry (Enter data in the blue cells)	-		٦.						
	Maximum Allowable Width for Spread Behind Curb	T _{BACK} =	10.0	ft						
	Side Slope Behind Curb (leave blank for no conveyance credit behind curb)	S _{BACK} =	0.020	ft/ft						
	Manning's Roughness Behind Curb (typically between 0.012 and 0.020)	n _{BACK} =	0.020							
	Height of Curb at Gutter Flow Line	H _{CURB} =	4.00	inches						
	Distance from Curb Face to Street Crown	T _{CROWN} =	17.0	ft						
	Gutter Width	W =	2.00	ft						
	Street Transverse Slope	S _X =	0.020	ft/ft						
	Gutter Cross Slope (typically 2 inches over 24 inches or 0.083 ft/ft)	S _W =	and the second se	ft/ft						
	Street Longitudinal Slope - Enter 0 for sump condition	S _o =	0.004	ft/ft						
	Manning's Roughness for Street Section (typically between 0.012 and 0.020)	n _{STREET} =	0.013							
			Minor Storm	Major Storm						
	Max. Allowable Spread for Minor & Major Storm	T _{MAX} =	17.0	17.0	ft					
ning 02	Max. Allowable Depth at Gutter Flowline for Minor & Major Storm	d _{MAX} =	6.4	6.4	inches					
	Allow Flow Depth at Street Crown (leave blank for no)			V	check = yes					
	Maximum Capacity for 1/2 Street based On Allowable Spread Water Depth without Gutter Depression (Eq. ST-2)		Minor Storm 4.08	Major Storm 4.08	inchos					
	Vertical Depth between Gutter Lip and Gutter Flowline (usually 2")	y = d _C =	2.0	2.0	inches inches					
	Gutter Depression (d_c - (W * S_x * 12))	a=	1.51	1.51	inches					
	Water Depth at Gutter Flowline	a = d =	5.59	5.59	inches					
	Allowable Spread for Discharge outside the Gutter Section W (T - W)	u - T _X =	15.0	15.0	ft					
	Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	Ê0 =	0.350	0.350	-					
	Discharge outside the Gutter Section W, carried in Section T_X	Q _x =	5.5	5.5	cfs					
	Discharge within the Gutter Section W ($Q_T - Q_X$)	Q _W =	3.0	3.0	cfs					
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	0.4	0.4	cfs					
	Maximum Flow Based On Allowable Spread	Q _T =	8.9	8.9	cfs					
	Flow Velocity within the Gutter Section	V =	3.9	3.9	fps					
	V*d Product: Flow Velocity times Gutter Flowline Depth	V*d =	1.8	1.8						
	Maximum Capacity for 1/2 Street based on Allowable Depth Theoretical Water Spread	T _{TH} =	Minor Storm	Major Storm	ft					
		т _н = Т _{х тн} =		20.4	ft					
	Theoretical Spread for Discharge outside the Gutter Section W (T - W) Gutter Flow to Design Flow Ratio by FHWA HEC-22 method (Eq. ST-7)	'хтн – Ео =	18.4 0.291	18.4 0.291						
	Theoretical Discharge outside the Gutter Section W, carried in Section T_{XTH}	с _о – Q _{X TH} =	9.4	9.4	cfs					
	Actual Discharge outside the Gutter Section W, Climited by distance T _{CROWN})	Q _X 1H = Q _X =	9.4	9.4	cfs					
	Discharge within the Gutter Section W ($Q_d - Q_X$)	Q _W =	3.9	3.9	cfs					
	Discharge Behind the Curb (e.g., sidewalk, driveways, & lawns)	Q _{BACK} =	1.2	1.2	cfs					
	Total Discharge for Major & Minor Storm (Pre-Safety Factor)	Q =	14.4	1.2	cfs					
	Average Flow Velocity Within the Gutter Section	Q - V =	4.3	4.3	fina					
	V*d Product: Flow Velocity Times Gutter Flowline Depth	V*d =	2.3	2.3	ips					
	Slope-Based Depth Safety Reduction Factor for Major & Minor ($d \ge 6$ ") Storm	R=	1.00	1.00	-					
	Max Flow Based on Allowable Depth (Safety Factor Applied)	Q _d =	14.4	14.4	cfs					
	Resultant Flow Depth at Gutter Flowline (Safety Factor Applied)	d =	6.40	6.40	inches					
			0.81	0.81	inches					
	Resultant Flow Depth at Street Crown (Safety Factor Applied)	d _{CROWN} =								
		a _{crown} =		Maire Ote						
	Resultant Flow Depth at Street Crown (Safety Factor Applied) MINOR STORM Allowable Capacity is based on Spread Criterion MAJOR STORM Allowable Capacity is based on Depth Criterion	a _{CROWN} = Q _{allow} =	Minor Storm	Major Storm 14.4	cfs					





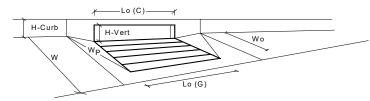


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type I	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C _f -G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	5.3	10.4	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.1	2.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	98	83	%

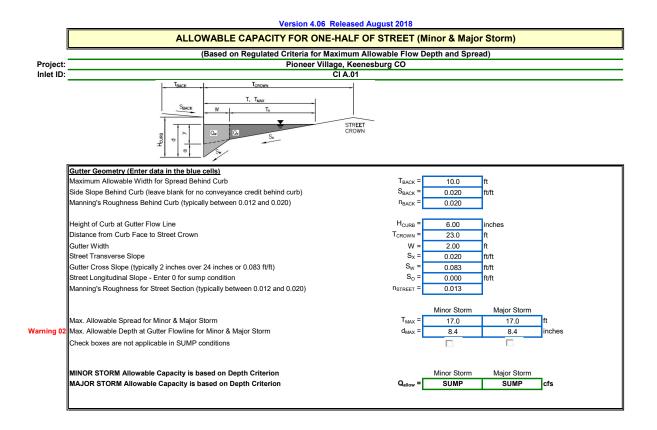


INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018

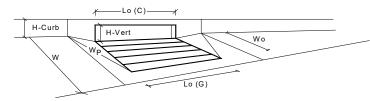


Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	8.4	inches
Grate Information		MINOR	MAJOR	🔽 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	C _f (C) =	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.53	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.79	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	1.00	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.9	17.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.7	2.8	cfs

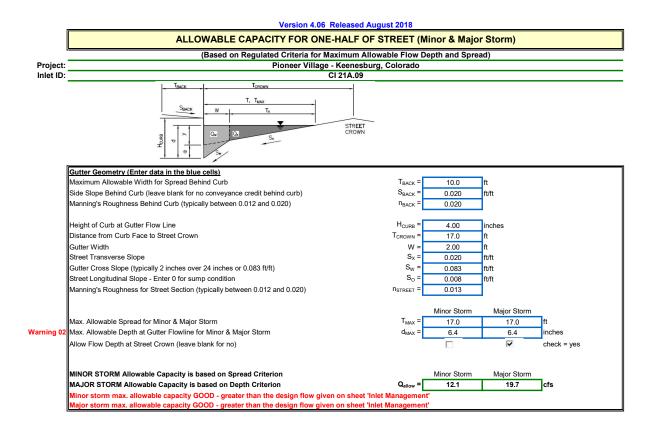


INLET IN A SUMP OR SAG LOCATION

Version 4.06 Released August 2018

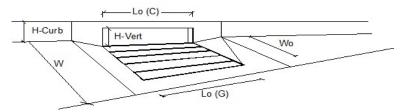


Design Information (Input) CDOT Type R Curb Opening		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type R	Curb Opening	
Local Depression (additional to continuous gutter depression 'a' from above)	a _{local} =	3.00	3.00	inches
Number of Unit Inlets (Grate or Curb Opening)	No =	1	1	
Water Depth at Flowline (outside of local depression)	Ponding Depth =	5.6	5.6	inches
Grate Information		MINOR	MAJOR	🧾 Override Depths
Length of a Unit Grate	L _o (G) =	N/A	N/A	feet
Width of a Unit Grate	W _o =	N/A	N/A	feet
Area Opening Ratio for a Grate (typical values 0.15-0.90)	A _{ratio} =	N/A	N/A	
Clogging Factor for a Single Grate (typical value 0.50 - 0.70)	C _f (G) =	N/A	N/A	
Grate Weir Coefficient (typical value 2.15 - 3.60)	C _w (G) =	N/A	N/A	
Grate Orifice Coefficient (typical value 0.60 - 0.80)	C _o (G) =	N/A	N/A	1
Curb Opening Information		MINOR	MAJOR	
Length of a Unit Curb Opening	L _o (C) =	10.00	10.00	feet
Height of Vertical Curb Opening in Inches	H _{vert} =	6.00	6.00	inches
Height of Curb Orifice Throat in Inches	H _{throat} =	6.00	6.00	inches
Angle of Throat (see USDCM Figure ST-5)	Theta =	63.40	63.40	degrees
Side Width for Depression Pan (typically the gutter width of 2 feet)	W _p =	2.00	2.00	feet
Clogging Factor for a Single Curb Opening (typical value 0.10)	$C_{f}(C) =$	0.10	0.10	
Curb Opening Weir Coefficient (typical value 2.3-3.7)	C _w (C) =	3.60	3.60	
Curb Opening Orifice Coefficient (typical value 0.60 - 0.70)	C _o (C) =	0.67	0.67	
Low Head Performance Reduction (Calculated)		MINOR	MAJOR	
Depth for Grate Midwidth	d _{Grate} =	N/A	N/A	ft
Depth for Curb Opening Weir Equation	d _{Curb} =	0.30	0.30	ft
Combination Inlet Performance Reduction Factor for Long Inlets	RF _{Combination} =	0.53	0.53	
Curb Opening Performance Reduction Factor for Long Inlets	RF _{Curb} =	0.91	0.91	
Grated Inlet Performance Reduction Factor for Long Inlets	RF _{Grate} =	N/A	N/A	
	_	MINOR	MAJOR	_
Total Inlet Interception Capacity (assumes clogged condition)	Q _a =	6.9	6.9	cfs
Inlet Capacity IS GOOD for Minor and Major Storms(>Q PEAK)	Q PEAK REQUIRED =	0.6	2.1	cfs









Design Information (Input)		MINOR	MAJOR	
Type of Inlet	Type =	CDOT Type I	R Curb Opening	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	5.0	5.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	15.00	15.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	W _o =	N/A	N/A	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	Cr-G =	N/A	N/A	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C _f -C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	3.1	9.5	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	Q _b =	0.0	0.9	cfs
Capture Percentage = Q _a /Q _o =	C% =	100	91	%



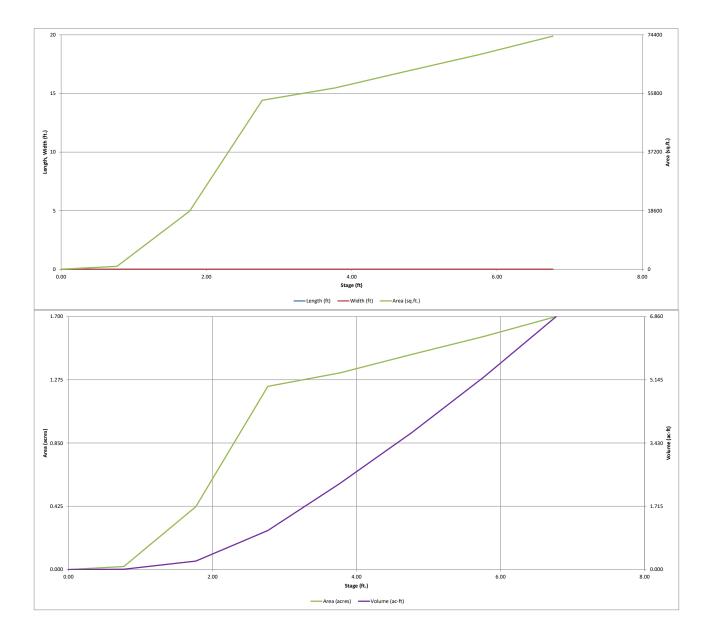
MHFD-Detention, Version 4.03 (May 2020)

Project:	Pioneer Village
Basin ID:	Pond 1 and 2
	1 AND 2 ORFICE
PERMANENT ORIFIC	

Depth Increment = 0.10 ft

ZONE	1 AND 2	ORIFICE			Depth Increment =	0.10	ft				Optional			
PERMANENT ORIFIC POOL Example Zone		on (Retentio	n Pond)		Stage - Storage	Stage	Optional Override	Length	Width	Area	Override	Area	Volume	Volume
Example 2016	comgulatio		n Fond)		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft 3)	(ac-ft)
Wetenshed Tefermetics													(10)	(de te)
Watershed Information		-			Top of Micropool		0.00				0	0.000		
Selected BMP Type =	EDB				4879		0.77				888	0.020	342	0.008
Watershed Area -	CC AC				4000		1.77				19.406	0.422	0.090	0.220
Watershed Area =	66.46	acres			4880		1.77				18,406	0.423	9,989	0.229
Watershed Length =	3,508	ft			4881		2.77				53,622	1.231	46,002	1.056
Watershed Length to Centroid =	1,872	ft			4882		3.77				57,524	1.321	101,575	2.332
•					4883									
Watershed Slope =	0.011	ft/ft					4.77				62,952	1.445	161,813	3.715
Watershed Imperviousness =	47.87%	percent			4884		5.77				68,243	1.567	227,411	5.221
Percentage Hydrologic Soil Group A =	100.0%	percent			4885		6.77				74,017	1.699	298,541	6.854
Percentage Hydrologic Soil Group B =	0.0%	percent												
Percentage Hydrologic Soil Groups C/D =	0.0%	percent												
Target WQCV Drain Time =	40.0	hours												
Location for 1-hr Rainfall Depths =	User Input	-												
After providing required inputs above inc														
depths, click 'Run CUHP' to generate run														
the embedded Colorado Urban Hydro	igraph Procedu	ire.	Optional Use	r Overrides										
Water Quality Capture Volume (WQCV) =	1.111	acre-feet		acre-feet										
		-		-										
Excess Urban Runoff Volume (EURV) =	3.624	acre-feet		acre-feet										
2-yr Runoff Volume (P1 = 0.86 in.) =	1.448	acre-feet	0.86	inches										
5-yr Runoff Volume (P1 = 1.14 in.) =	1.973	acre-feet	1.14	inches										
10-yr Runoff Volume (P1 = 1.41 in.) =	2.612	acre-feet	1.41	inches										
		-		-										
25-yr Runoff Volume (P1 = 1.85 in.) =	3.910	acre-feet	1.85	inches										
50-yr Runoff Volume (P1 = 2.23 in.) =	5.523	acre-feet	2.23	inches										
100-yr Runoff Volume (P1 = 2.66 in.) =	7.670	acre-feet	2.66	inches										
		-		-										
500-yr Runoff Volume (P1 = 3.83 in.) =	13.699	acre-feet	3.83	inches										
Approximate 2-yr Detention Volume =	1.681	acre-feet												
Approximate 5-yr Detention Volume =	2.330	acre-feet												
Approximate 10-yr Detention Volume =	3.020	acre-feet												
		-												
Approximate 25-yr Detention Volume =	4.253	acre-feet												
Approximate 50-yr Detention Volume =	5.099	acre-feet												
Approximate 100-yr Detention Volume =	6.152	acre-feet												
supposition to yi Detenuori voidille =	0.102	1.00 C 10CL												
Define Zones and Basin Geometry														
Zone 1 Volume (WQCV) =	1.111	acre-feet												
Zone 2 Volume (EURV - Zone 1) =	2.513	acre-feet												
Zone 3 Volume (100-year - Zones 1 & 2) =	2.528	acre-feet												
Total Detention Basin Volume =	6.152	acre-feet												
		-												
Initial Surcharge Volume (ISV) =	user	ft ³												
Initial Surcharge Depth (ISD) =	user	ft												
Total Available Detention Depth (H _{total}) =	user	ft												
Depth of Trickle Channel $(H_{TC}) =$	user	ft												
		-												
Slope of Trickle Channel (S _{TC}) =	user	ft/ft												
Slopes of Main Basin Sides (Smain) =	user	H:V												
Basin Length-to-Width Ratio (RL/W) =	user	1												
basin Eerigan to Widan (dato (rt_/w) =	usei	1												
		-												
Initial Surcharge Area (A _{ISV}) =	user	ft ²												
Surcharge Volume Length $(L_{ISV}) =$	user	lft.												
Surcharge Volume Width (W _{ISV}) =		ft												
	user													
Depth of Basin Floor $(H_{FLOOR}) =$	user	ft												
Length of Basin Floor (L _{FLOOR}) =	user	ft												
Width of Basin Floor $(W_{FLOOR}) =$	user	ft												
		-												
Area of Basin Floor $(A_{FLOOR}) =$	user	ft ²												
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³												
Depth of Main Basin (H _{MAIN}) =	user	ft												
		-												
Length of Main Basin (L _{MAIN}) =	user	ft												
Width of Main Basin (W _{MAIN}) =	user	ft												
Area of Main Basin (A _{MAIN}) =	user	ft ²												
Volume of Main Basin (V _{MAIN}) =	user	ft ³												
		-												
Calculated Total Basin Volume (V _{total}) =	user	acre-feet												

MHFD-Detention, Version 4.03 (May 2020)



DETENTION BASIN OUTLET STRUCTURE DESIGN MHFD-Detention, Version 4.03 (May 2020 Project: Pioneer Village Basin ID: Pond 1 and 2 Estimated Estimated ZONE Volume (ac-ft) Stage (ft) Outlet Type VOLUME EURV WQCV Zone 1 (WQCV) 2.82 1.111 Orifice Plate 100-YEAF Zone 2 (EURV) 4.71 2.513 Orifice Plate ZONE 1 AND 2 Zone 3 (100-year) 6.36 2.528 Weir&Pipe (Restrict) Example Zone Configuration (Retention Pond) Total (all zones) 6.152 User Input: Orifice at Underdrain Outlet (typically used to drain WQCV in a Filtration BMP) Calculated Parameters for Underdrain ft (distance below the filtration media surface) Underdrain Orifice Area Underdrain Orifice Invert Depth = N/A N/A ft² Underdrain Orifice Centroid = Underdrain Orifice Diameter = N/A inches N/A feet Calculated Parameters for Plate User Input: Orifice Plate with one or more orifices or Elliptical Slot Weir (typically used to drain WQCV and/or EURV in a sedimentation BMP) Invert of Lowest Orifice = ft (relative to basin bottom at Stage = 0 ft) WO Orifice Area per Row = 3.472E-02 0.00 lft² Depth at top of Zone using Orifice Plate = 4.71 ft (relative to basin bottom at Stage = 0 ft) Elliptical Half-Width = N/A feet Orifice Plate: Orifice Vertical Spacing = 18.84 inches Elliptical Slot Centroid = N/A feet ft² Orifice Plate: Orifice Area per Row = 5.00 Elliptical Slot Area = sq. inches (use rectangular openings) N/A User Input: Stage and Total Area of Each Orifice Row (numbered from lowest to highest) Row 1 (required) Row 2 (optional) Row 3 (optional) Row 4 (optional) Row 5 (optional) Row 6 (optional) Row 7 (optional) Row 8 (optional) Stage of Orifice Centroid (ft) 0.00 1.60 3.20 Orifice Area (sq. inches) 5.00 5.00 5.00 Row 9 (optional) Row 10 (optional) Row 11 (optional) Row 12 (optional) Row 13 (optional) Row 14 (optional) Row 15 (optional) Row 16 (optional) Stage of Orifice Centroid (ft) Orifice Area (sg. inches) User Input: Vertical Orifice (Circular or Rectangular) Calculated Parameters for Vertical Orifice Not Selected Not Selected Not Selected Not Selected ft² Invert of Vertical Orifice = N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Area N/A N/A Depth at top of Zone using Vertical Orifice = N/A N/A ft (relative to basin bottom at Stage = 0 ft) Vertical Orifice Centroid = N/A N/A feet inches Vertical Orifice Diameter = N/A N/A User Input: Overflow Weir (Dropbox with Flat or Sloped Grate and Outlet Pipe OR Rectangular/Trapezoidal Weir (and No Outlet Pipe) Calculated Parameters for Overflow Weir Zone 3 Weir Not Selected Zone 3 Weir Not Selected Overflow Weir Front Edge Height, Ho = 4.71 ft (relative to basin bottom at Stage = 0 ft) Height of Grate Upper Edge, H_t = N/A 5.88 N/A feet Overflow Weir Slope Length = Overflow Weir Front Edge Length = 8.00 N/A feet 4.81 N/A feet Overflow Weir Grate Slope = 4.00 N/A H:V Grate Open Area / 100-yr Orifice Area = 15.87 N/A Horiz. Length of Weir Sides = feet Overflow Grate Open Area w/o Debris = 28.88 ft² 4.67 N/A N/A Overflow Grate Open Area % = Overflow Grate Open Area w/ Debris = 75% N/A %, grate open area/total area 28.88 N/A fť Debris Clogging % = 0% N/A User Input: Outlet Pipe w/ Flow Restriction Plate (Circular Orifice, Restrictor Plate, or Rectangular Orifice) Calculated Parameters for Outlet Pipe w/ Flow Restriction Plate Zone 3 Restrictor Not Selected Zone 3 Restrictor Not Selected Depth to Invert of Outlet Pipe = 2.50 Outlet Orifice Area = ft² N/A ft (distance below basin bottom at Stage = 0 ft) 1.82 N/A Outlet Pipe Diameter = 24.00 N/A inches Outlet Orifice Centroid : 0.64 N/A feet Restrictor Plate Height Above Pipe Invert = 13.50 . inches Half-Central Angle of Restrictor Plate on Pipe = 1.70 N/A radians User Input: Emergency Spillway (Rectangular or Trapezoidal) Calculated Parameters for Spillway Spillway Invert Stage= 6.36 ft (relative to basin bottom at Stage = 0 ft) Spillway Design Flow Depth= 0.41 feet Spillway Crest Length = Stage at Top of Freeboard = 100.00 feet 7.77 feet Spillway End Slopes : 4.00 H:V Basin Area at Top of Freeboard 1.70 acres Freeboard above Max Water Surface = 1.00 feet Basin Volume at Top of Freeboard = 6.85 acre-ft Routed Hydrograph Results in the Inflow Hv phs table (Co nns W throu The user can override the o ring new valu EURV Design Storm Return Period = WQCV 2 Year 5 Year 10 Year 25 Year 50 Year 100 Year 500 Year One-Hour Rainfall Depth (in) = 0.86 1.14 1.41 N/A N/A 1.85 2.23 2.66 3.83 13.699 CUHP Runoff Volume (acre-ft) 1.111 3.624 1.448 1.973 2.612 3.910 5.523 7.670 Inflow Hydrograph Volume (acre-ft) = N/A N/A 1.448 1.973 2.612 3.910 5.523 7.670 13.699 CUHP Predevelopment Peak O (cfs) : N/A N/A 0.0 0.2 0.4 14.0 29.1 71.4 3.1 OPTIONAL Override Predevelopment Peak Q (cfs) = N/A N/A Predevelopment Unit Peak Flow, g (cfs/acre) : 0.00 N/A N/A 0.00 0.01 0.05 0.21 0.44 1.07 Peak Inflow Q (cfs) 57.0 81.9 146.2 N/A 22.0 38.0 N/A 12.5 16.5 Peak Outflow Q (cfs) : 0.5 0.9 0.5 0.6 0.7 14.3 24.2 100.6 1.2 Ratio Peak Outflow to Predevelopment Q = N/A N/A N/A 0.4 0.8 1.6 1.0 Structure Controlling Flow : Plate Overflow Weir 1 Plate Plate Plate Overflow Weir 1 Overflow Weir 1 Outlet Plate Spillway Max Velocity through Grate 1 (fps) = N/A N/A N/A N/A N/A 0.0 0.5 0.8 0.9 Max Velocity through Grate 2 (fps) = N/A N/A N/A N/A N/A N/A N/A N/A N/A Time to Drain 97% of Inflow Volume (hours) = 80 67 83 82 73 Time to Drain 99% of Inflow Volume (hours) 40 49 60 84 84 71 88 89 87

Maximum Ponding Depth (ft) =

Maximum Volume Stored (acre-ft) =

Area at Maximum Ponding Depth (acres)

2.82

1.24

4.71

1.44

2.99

1.25

3.39

1.29

1 837

3.86

1.33

4.76

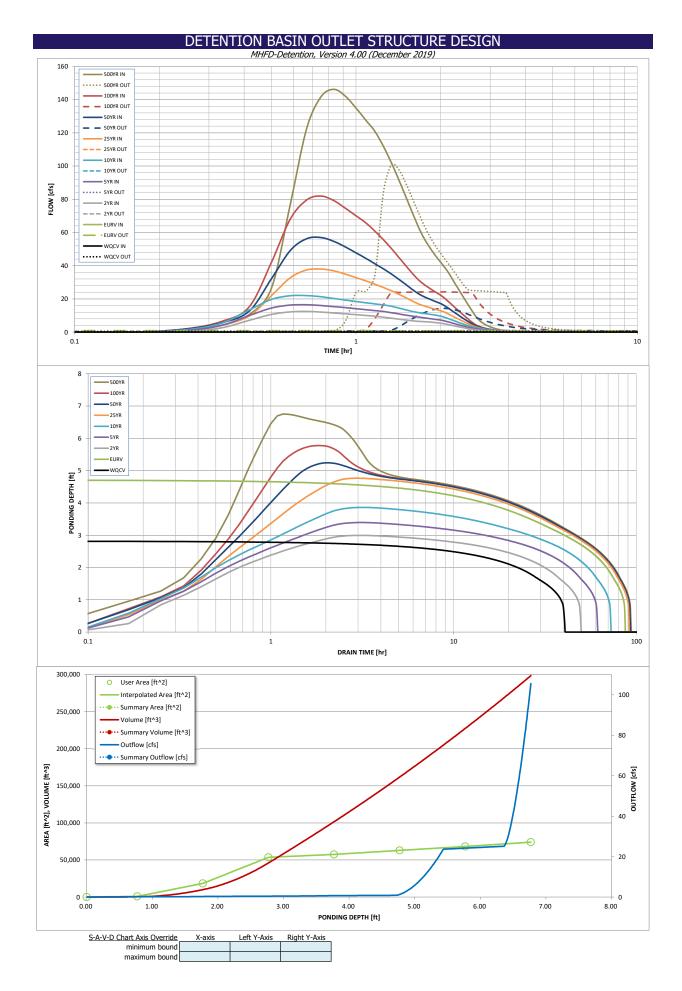
1.44 3.700 5.24

1.50

5.78

1.57

6.75 1.70 6.820



Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

SOURCE CUHP <	Icfs 500 Year [cfs] 00 0.00 00 0.00 00 0.00 00 0.00 00 0.04 01 0.056 10 10.56 12 26.25 36 76.61 96 122.26 48 141.63 93 146.22 19 142.07 56 134.91 95 120.91 85 120.91 85 120.91 85 122.26 49 92.14 21 81.94 19 72.31 49 63.36 52 56.13 50 50.68 52 46.11 15 42.00 21 38.20
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MHFD-Detention, Version 4.03 (May 2020) Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope changes (e.g. ISV and Floor) from the S-A-V table on
							changes (e.g. ISV and Floor)
							Sheet 'Basin'.
							Sheet Basin.
							Also include the inverts of all
							outlets (e.g. vertical orifice,
							overflow grate, and spillway,
							where applicable).
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Pond A Forebay Notch

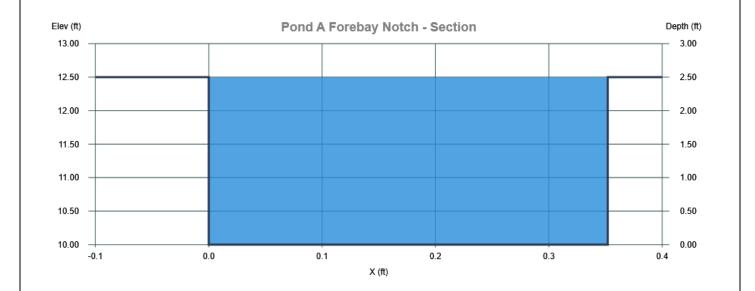
04-01-2021

Channel 1

Project Name: New Project

RECTANGULAR		DISCHARGE	
Bottom Width	= 0.35 ft	Method	= Known Q
Total Depth	= 2.50 ft	Known Q	= 1.64 cfs
Invert Elevation	= 10.00 ft		
Channel Slope	= 0.300 %		
Manning's n	= 0.013		

Flow	Depth	Area	Velocity	WP	n-value	Crit Depth	HGL	EGL	Max Shear	Top Width
(cfs)	(ft)	(sqft)	(ft/s)	(ft)		(ft)	(ft)	(ft)	(lb/sqft)	(ft)
1.64	2.49	0.88	1.87	5.33	0.013	0.88	12.49	12.54	0.47	0.35



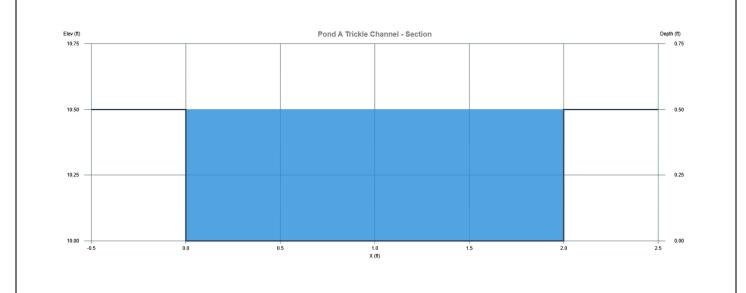
Pond A Trickle Channel

04-09-2021

Channel 1

RECTANGULAR		DISCHARGE	
Bottom Width	= 2.00 ft	Method	= Q vs Depth
Total Depth	= 0.50 ft	Q Min	= 0.11 cfs
Invert Elevation	= 10.00 ft	Q Max	= 3.88 cfs
Channel Slope	= 0.500 %	Increments	= 10
Manning's n	= 0.013		

Flow	Depth	Area	Velocity	WP	n-value	Crit Depth	HGL	EGL	Max Shear	Top Width
(cfs)	(ft)	(sqft)	(ft/s)	(ft)		(ft)	(ft)	(ft)	(lb/sqft)	(ft)
3.88	0.50	1.00	3.88	3.00	0.013	0.49	10.50	10.73	0.16	2.00



MHFD-Detention, Version 4.04 (February 2021)

Basin ID: Pond B	
ZONE 2 ZONE 2 ZONE 1 ZONE 1 AND 2 ZONE 1 AND 2	100-YEAR ORIFICE

Watershed Information

Selected BMP Type =	EDB	
Watershed Area =	51.64	acres
Watershed Length =	4,072	ft
Watershed Length to Centroid =	1,942	ft
Watershed Slope =	0.014	ft/ft
Watershed Imperviousness =	58.00%	percent
Percentage Hydrologic Soil Group A =	50.0%	percent
Percentage Hydrologic Soil Group B =	50.0%	percent
Percentage Hydrologic Soil Groups C/D =	0.0%	percent
Target WQCV Drain Time =	40.0	hours
Location for 1-hr Rainfall Depths =	User Input	

After providing required inputs above including 1-hour rainfall depths, click 'Run CUHP' to generate runoff hydrographs using the embedded Colorado Urban Hydrograph Procedure.

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Water Quality Capture Volume (WQCV) =	0.988	acre-feet		acı
Excess Urban Runoff Volume (EURV) =	3.420	acre-feet		acı
2-yr Runoff Volume (P1 = 0.86 in.) =	1.890	acre-feet	0.86	inc
5-yr Runoff Volume (P1 = 1.14 in.) =	2.671	acre-feet	1.14	inc
10-yr Runoff Volume (P1 = 1.41 in.) =	3.438	acre-feet	1.41	inc
25-yr Runoff Volume (P1 = 1.85 in.) =	5.370	acre-feet	1.85	inc
50-yr Runoff Volume (P1 = 2.23 in.) =	6.941	acre-feet	2.23	inc
100-yr Runoff Volume (P1 = 2.66 in.) =	9.020	acre-feet	2.66	inc
500-yr Runoff Volume (P1 = 3.83 in.) =	14.217	acre-feet	3.83	inc
Approximate 2-yr Detention Volume =	1.739	acre-feet		
Approximate 5-yr Detention Volume =	2.438	acre-feet		
Approximate 10-yr Detention Volume =	3.245	acre-feet		
Approximate 25-yr Detention Volume =	4.257	acre-feet		
Approximate 50-yr Detention Volume =	4.901	acre-feet		
Approximate 100-yr Detention Volume =	5.754	acre-feet		

Define Zones and Basin Geometry

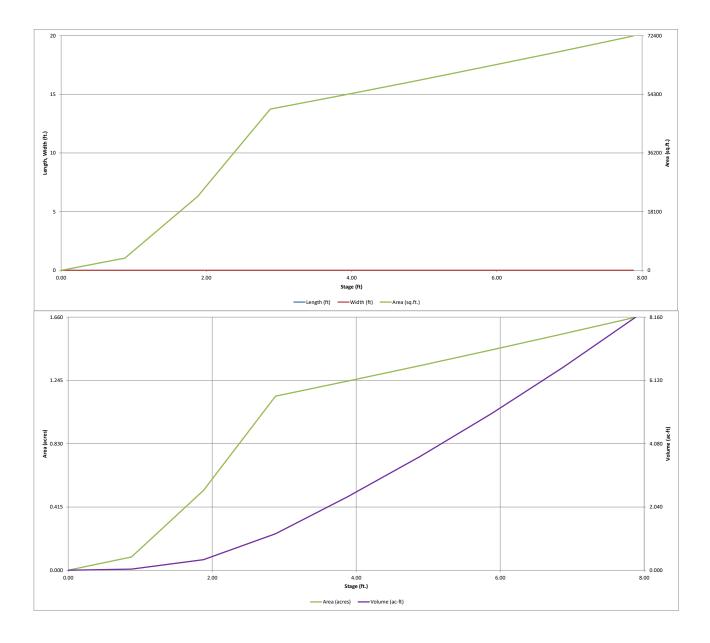
The Lones and Basin Besined)		
Zone 1 Volume (WQCV) =	0.988	acre-feet
Zone 2 Volume (EURV - Zone 1) =	2.432	acre-feet
Zone 3 Volume (100-year - Zones 1 & 2) =	2.334	acre-feet
Total Detention Basin Volume =	5.754	acre-feet
Initial Surcharge Volume (ISV) =	user	ft ³
Initial Surcharge Depth (ISD) =	user	ft
Total Available Detention Depth $(H_{total}) =$	user	ft
Depth of Trickle Channel (H _{TC}) =	user	ft
Slope of Trickle Channel (S _{TC}) =	user	ft/ft
Slopes of Main Basin Sides (S _{main}) =	user	H:V
Basin Length-to-Width Ratio (R _{L/W}) =	user	
Initial Surcharge Area (A _{ISV}) =	user	ft ²
Surcharge Volume Length $(L_{ISV}) =$	user	ft
Surcharge Volume Width (W_{ISV}) =	user	ft
Depth of Basin Floor (H _{FLOOR}) =	user	ft
Length of Basin Floor $(L_{FLOOR}) =$	user	ft
Width of Basin Floor (W _{FLOOR}) =	user	ft
Area of Basin Floor (A _{FLOOR}) =	user	ft ²
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³
Depth of Main Basin $(H_{MAIN}) =$	user	ft
Length of Main Basin $(L_{MAIN}) =$	user	ft
Width of Main Basin (W_{MAIN}) =	user	ft
Area of Main Basin (A _{MAIN}) =	user	ft ²
Volume of Main Basin (V _{MAIN}) =	user	ft ³
Calculated Total Pacin Volume (V) -		acro foot

Calculated Total Basin Volume (V_{total}) = user

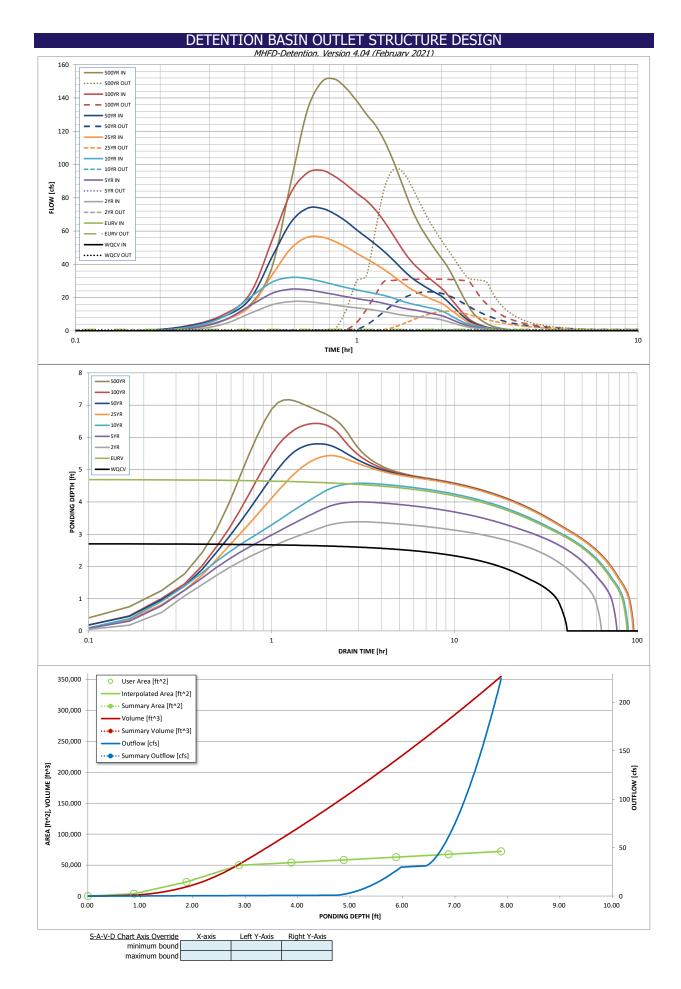
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MHFD-Detention, Version 4.04 (February 2021)



Project:	Pioneer Village ~		-D-Detention, Vers	sion 4.04 (Februai	Y 2021)				
Basin ID:									
ZONE 3				Estimated	Estimated				
-ZONE 1				Stage (ft)	Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)	2.71	0.988	Orifice Plate	1		
ZONE 1 AND 2	100-YEAR ORIFICE		Zone 2 (EURV)	4.71	2.432	Orifice Plate			
PERMANENT ORIFICES			Zone 3 (100-year)	6.36	2.334	Weir&Pipe (Restrict)			
Example Zone	Configuration (Re	tention Pond)		Total (all zones)	5.754		•		
User Input: Orifice at Underdrain Outlet (typicall	v used to drain WC	CV in a Filtration B	MP)	. ,			Calculated Parame	ters for Underdrain	
Underdrain Orifice Invert Depth =			the filtration media	surface)	Underd	rain Orifice Area =		ft ²	
Underdrain Orifice Diameter =		inches		Surrace)		Orifice Centroid =		feet	
		Inches			onderdidin				
User Input: Orifice Plate with one or more orific	es or Elliptical Slot	Weir (typically used	to drain WOCV and	d/or ELID\/ in a ced	imentation BMP)		Calculated Parame	tors for Diato	
Invert of Lowest Orifice =	0.00		bottom at Stage =			ce Area per Row =	3.368E-02	ft ²	
Depth at top of Zone using Orifice Plate =	4.71		bottom at Stage =	,		ptical Half-Width =	N/A	feet	
			i Dolloin al Slage -	- 0 10)					
Orifice Plate: Orifice Vertical Spacing =	18.80	inches			•	cal Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	4.85	sq. inches (use rec	tangular openings)		E	lliptical Slot Area =	N/A	ft ²	
User Input: Stage and Total Area of Each Orific					1		1	1	1
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	1
Stage of Orifice Centroid (ft)	0.00	1.57	3.14						
Orifice Area (sq. inches)	4.85	4.85	4.85]
									-
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									1
Orifice Area (sq. inches)									
									1
User Input: Vertical Orifice (Circular or Rectange	ular)						Calculated Parame	ters for Vertical Ori	fice
+	Not Selected	Not Selected					Not Selected	Not Selected	1
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage -	-0ft) Ver	tical Orifice Area =	N/A	N/A	ft ²
		N/A		-			N/A		1
Depth at top of Zone using Vertical Orifice =	N/A		ft (relative to basin	i Dollom al Slage =	= 0 IL) Vertica	Orifice Centroid =	IN/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches						
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoid	al Weir (and No Ou	itlet Pipe)		Calculated Parame	ters for Overflow W	<u>/eir</u>
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected	
Overflow Weir Front Edge Height, Ho =	4.71	N/A	ft (relative to basin b	ottom at Stage = 0 f	t) Height of Grate	Upper Edge, H _t =	5.88	N/A	feet
Overflow Weir Front Edge Length =	8.00	N/A	feet	-	Overflow W	eir Slope Length =	4.81	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V	Gr	ate Open Area / 10		10.00	N/A	
Horiz. Length of Weir Sides =	4.67	N/A	feet		verflow Grate Open		26.80	N/A	ft ²
Overflow Grate Type =	Type C Grate	N/A			Overflow Grate Open		26.80	N/A	ft ²
			0/	C C	Weillow Grate Oper	TATEd W/ DEDTIS -	20.00	IN/A	Jrt
Debris Clogging % =	0%	N/A	%						
	(C) 0 (C)				6				
User Input: Outlet Pipe w/ Flow Restriction Plate			ectangular Orifice)		<u>Ca</u>	iculated Parameters	s for Outlet Pipe w/		ate
	Zone 3 Restrictor	Not Selected					Zone 3 Restrictor	Not Selected	
Depth to Invert of Outlet Pipe =	0.26	N/A	ft (distance below ba	asin bottom at Stage		utlet Orifice Area =	2.68	N/A	ft ²
Outlet Pipe Diameter =	24.00	N/A	inches		Outlet	Orifice Centroid =	0.87	N/A	feet
Restrictor Plate Height Above Pipe Invert =	19.10		inches	Half-Cent	ral Angle of Restric	tor Plate on Pipe =	2.20	N/A	radians
User Input: Emergency Spillway (Rectangular or	Trapezoidal)								
Spillway Invert Stage=	6.44	A (valative to basis	hattan at Chana				Calculated Parame	ters for Spillway	
, , ,	0.44	It (relative to basi	bottom at Stage =	= 0 ft)	Spillway D	esign Flow Depth=	Calculated Parame	feet	
Spillway Crest Length =		feet	i bottom at Stage =	= 0 ft)		esign Flow Depth= op of Freeboard =			
	32.00	feet	i bottom at Stage =	= 0 ft)	Stage at T	op of Freeboard =	0.94 8.38	feet feet	
Spillway End Slopes =	32.00 4.00	feet H:V	i bottom at Stage =	= 0 ft)	Stage at 1 Basin Area at 1	op of Freeboard = op of Freeboard =	0.94 8.38 1.66	feet feet acres	
	32.00	feet	i bottom at Stage =	= 0 ft)	Stage at 1 Basin Area at 1	op of Freeboard =	0.94 8.38	feet feet	
Spillway End Slopes =	32.00 4.00	feet H:V	i bottom at Stage =	= 0 ft)	Stage at 1 Basin Area at 1	op of Freeboard = op of Freeboard =	0.94 8.38 1.66	feet feet acres	
Spillway End Slopes =	32.00 4.00 1.00	feet H:V feet			Stage at 1 Basin Area at 1	op of Freeboard = op of Freeboard = op of Freeboard =	0.94 8.38 1.66 8.16	feet feet acres acre-ft	4 <i>F).</i>
Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results	32.00 4.00 1.00	feet H:V feet	HP hydrographs and	d runoff volumes by	Stage at T Basin Area at T Basin Volume at T <u>y entering new valu</u>	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy	0.94 8.38 1.66 8.16 drographs table (Co	feet feet acres acre-ft <i>olumns W through 1</i>	
Spillway End Slopes = Freeboard above Max Water Surface =	32.00 4.00 1.00	feet H:V feet			Stage at T Basin Area at T Basin Volume at T	op of Freeboard = op of Freeboard = op of Freeboard =	0.94 8.38 1.66 8.16	feet feet acres acre-ft	4 <i>F).</i> 500 Year 3.83
Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period =	32.00 4.00 1.00 <i>The user can overn</i> WQCV	feet H:V feet ride the default CUI EURV	HP hydrographs and 2 Year	d runoff volumes by 5 Year	Stage at 1 Basin Area at 1 Basin Volume at 1 Ventering new value 10 Year	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year	0.94 8.38 1.66 8.16 drographs table (CC	feet feet acres acre-ft <i>blumns W through /</i> 100 Year	500 Year
Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) =	32.00 4.00 1.00 The user can oven WQCV N/A 0.988 N/A	feet H:V feet EURV N/A 3.420 N/A	HP hydrographs and 2 Year 0.86 1.890 1.890	d runoff volumes by 5 Year 1.14 2.671 2.671	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new valu 10 Year 1.41 3.438 3.438	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370	0.94 8.38 1.66 8.16 drographs table (CC 50 Year 2.23 6.941 6.941	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020	500 Year 3.83 14.217 14.217
Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) =	32.00 4.00 1.00 <i>The user can overn</i> WQCV N/A 0.988 N/A N/A	feet H:V feet EURV N/A 3.420 N/A N/A	HP hydrographs and 2 Year 0.86 1.890	d runoff volumes by 5 Year 1.14 2.671	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new value 10 Year 1.41 3.438	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370	0.94 8.38 1.66 8.16 drographs table (Co 50 Year 2.23 6.941	feet feet acres acre-ft <u>100 Year</u> <u>2.66</u> 9.020	500 Year 3.83 14.217
Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) =	32.00 4.00 1.00 <i>The user can overn</i> WOCV N/A 0.988 N/A N/A N/A	feet H:V feet <u>EURV</u> N/A 3.420 N/A N/A N/A	HP hydrographs and 2 Year 0.86 1.890 1.890 0.1	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new valuu 10 Year 1.41 3.438 3.438 0.5	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370 12.2	0.94 8.38 1.66 8.16 drographs table (Co 50 Year 2.23 6.941 6.941 21.2	feet feet acres acre-ft <u>100 Year</u> <u>2.66</u> <u>9.020</u> <u>9.020</u> <u>9.020</u>	500 Year 3.83 14.217 14.217 64.3
Spillway End Slopes = Freeboard above Max Water Surface = Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) =	32.00 4.00 1.00 7he user can oven N/A 0.988 N/A N/A N/A N/A N/A	feet H:V feet <u>EURV</u> N/A 3.420 N/A N/A N/A N/A	HP hydrographs and 2 Year 0.86 1.890 1.890 0.1 0.00	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new value 1.41 3.438 3.438 0.5 0.01	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370 1.2.2 0.24	0.94 8.38 1.66 8.16 drographs table (Co 50 Year 2.23 6.941 6.941 21.2 0.41	feet feet acres acre-ft <u>100 Year</u> <u>2.66</u> <u>9.020</u> <u>9.020</u> <u>34.2</u> <u>0.66</u>	500 Year 3.83 14.217 14.217 64.3 1.25
Spillway End Slopes = Freeboard above Max Water Surface = Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) =	32.00 4.00 1.00 7he user can oven WQCV N/A 0.988 N/A N/A N/A N/A N/A	feet H:V feet EURV N/A 3.420 N/A N/A N/A N/A N/A	HP hydrographs and 2 Year 0.86 1.890 0.1 	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new valu 10 Year 1.41 3.438 3.438 0.5 0.01 32.1	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370 12.2 0.24 56.4	0.94 8.38 1.66 8.16 drographs table (CC 50 Year 2.23 6.941 6.941 21.2 0.41 73.7	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 34.2 <u>0.66</u> 96.5	500 Year 3.83 14.217 14.217 64.3 1.25 1.25 151.3
Spillway End Slopes = Freeboard above Max Water Surface = Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) =	32.00 4.00 1.00 WQCV N/A 0.988 N/A N/A N/A N/A N/A N/A 0.4	feet H:V feet EURV N/A 3.420 N/A N/A N/A N/A N/A N/A 0.8	HP hydrographs and 2 Year 0.86 1.890 0.1 0.00 17.6 0.6	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new value 1.41 3.438 3.438 0.5 0.01 32.1 0.8	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370 12.2 0.24 56.4 11.9	0.94 8.38 1.66 8.16 6.91 2.23 6.941 21.2 0.41 73.7 2.3.4	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 34.2 <u>0.66</u> 96.5 31.2	500 Year 3.83 14.217 14.217 64.3 1.25 1.25 151.3 97.2
Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Unflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q =	32.00 4.00 1.00 7 <i>The user can overr</i> WQCV N/A 0.988 N/A N/A N/A N/A N/A N/A N/A	feet H:V feet EURV N/A 3.420 N/A N/A N/A N/A N/A 0.8 N/A	<i>HP hydrographs and</i> 2 Year 0.86 1.890 1.890 0.1 0.00 17.6 0.6 N/A	d runoff volumes b) 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7 2.3	Stage at 1 Basin Area at 1 Basin Volume at 1 0 Year 1.41 3.438 3.438 0.5 0.01 32.1 0.8 1.6	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370 12.2 0.24 56.4 11.9 1.0	0.94 8.38 1.66 8.16 50 Year 2.23 6.941 6.941 21.2 0.41 73.7 23.4 1.1	feet feet acres acre-ft 100 Year 2.66 9.020 9.020 34.2 0.66 96.5 31.2 0.9	500 Year 3.83 14.217 14.217 64.3 1.25 151.3 97.2 1.5
Spillway End Slopes = Freeboard above Max Water Surface = Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Surflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow =	32.00 4.00 1.00 7he user can oven N/A 0.988 N/A N/A N/A N/A N/A N/A N/A N/A N/A Plate	feet H:V feet N/A N/A N/A N/A N/A N/A N/A N/A O.8 N/A Overflow Weir 1	AP hydrographs and 2 Year 0.86 1.890 0.1 0.00 17.6 0.6 N/A Plate	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7 2.3 Plate	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new valu 10 Year 1.41 3.438 3.438 0.5 0.01 32.1 0.8 1.6 Plate	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370 12.2 0.24 56.4 11.9 1.0 Overflow Weir 1	0.94 8.38 1.66 8.16 drographs table (CC 50 Year 2.23 6.941 6.941 21.2 0.41 73.7 23.4 1.1 Overflow Weir 1	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 34.2 <u>0.66</u> 96.5 31.2 0.9 Spillway	500 Year 3.83 14.217 14.217 64.3 1.25 151.3 97.2 1.5 Spillway
Spillway End Slopes = Freeboard above Max Water Surface = Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) =	32.00 4.00 1.00 7he user can oven N/A 0.988 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet H:V feet EURV N/A 3.420 N/A N/A N/A N/A N/A N/A Overflow Weir 1 N/A	HP hydrographs and 2 Year 0.86 1.890 0.1 0.00 17.6 0.6 N/A Plate N/A	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7 2.3 Plate N/A	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new valu 10 Year 1.41 3.438 3.438 0.5 0.5 0.01 32.1 0.8 1.6 Plate N/A	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 12.2 0.24 56.4 11.9 1.0 Overflow Weir 1 0.4	0.94 8.38 1.66 8.16 drographs table (CC 50 Year 2.23 6.941 6.941 21.2 0.41 73.7 23.4 1.1 Overflow Weir 1 0.8	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 9.020 34.2 <u>0.66</u> 96.5 31.2 0.9 5pillway 1.1	500 Year 3.83 14.217 14.217 64.3 1.25 151.3 97.2 1.5 Spillway 1.2
Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) =	32.00 4.00 1.00 <i>The user can overn</i> WQCV N/A 0.988 N/A N/A N/A N/A N/A N/A N/A Plate N/A N/A N/A	feet H:V feet EURV N/A 3.420 N/A N/A N/A N/A N/A Overflow Weir 1 N/A N/A N/A	HP hydrographs and 2 Year 0.86 1.890 0.1 0.00 17.6 0.6 N/A Plate N/A N/A	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7 2.3 Plate	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new valu 10 Year 1.41 3.438 3.438 0.5 0.01 32.1 0.8 1.6 Plate	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 1.22 0.24 56.4 11.9 1.0 Overflow Weir 1 0.4 N/A	0.94 8.38 1.66 8.16 drographs table (CC 50 Year 2.23 6.941 6.941 21.2 0.41 73.7 23.4 1.1 Overflow Weir 1	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 34.2 <u>0.66</u> 96.5 31.2 0.9 Spillway 1.1 N/A	500 Year 3.83 14.217 14.217 64.3 1.25 151.3 97.2 1.5 Spillway 1.2 N/A
Spillway End Slopes = Freeboard above Max Water Surface = Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) =	32.00 4.00 1.00 7he user can oven N/A 0.988 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet H:V feet EURV N/A 3.420 N/A N/A N/A N/A N/A N/A Overflow Weir 1 N/A	HP hydrographs and 2 Year 0.86 1.890 0.1 0.00 17.6 0.6 N/A Plate N/A	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 	Stage at 1 Basin Area at 1 Basin Volume at 1 9 <i>entering new valu</i> 10 Year 1.41 3.438 3.438 0.5 0.01 32.1 0.8 1.6 Plate N/A N/A	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 12.2 0.24 56.4 11.9 1.0 Overflow Weir 1 0.4	0.94 8.38 1.66 8.16 6.91 2.23 6.941 21.2 0.41 73.7 23.4 1.1 0verflow Weir 1 0.8 N/A	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 9.020 34.2 <u>0.66</u> 96.5 31.2 0.9 5pillway 1.1	500 Year 3.83 14.217 14.217 64.3 1.25 151.3 97.2 1.5 Spillway 1.2
Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) =	32.00 4.00 1.00 7he user can oven N/A 0.988 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	feet H:V feet N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	HP hydrographs and 2 Year 0.86 1.890 0.1 0.00 17.6 0.6 N/A Plate N/A N/A S8	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7 2.3 Plate N/A N/A 70	Stage at 1 Basin Area at 1 Basin Volume at 1 V entering new value 1.41 3.438 3.438 0.5 0.01 32.1 0.8 1.6 Plate N/A N/A 80	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 5.370 12.2 0.24 56.4 11.9 1.0 Overflow Weir 1 0.4 N/A 83	0.94 8.38 1.66 8.16 drographs table (Co 50 Year 2.23 6.941 2.22 0.41 73.7 23.4 1.1 Overflow Weir 1 0.8 N/A 80	feet feet acres acre-ft 100 Year 2.66 9.020 9.020 34.2 0.66 96.5 31.2 0.9 Spillway 1.1 N/A 77	500 Year 3.83 14.217 14.217 64.3 1.25 1.51.3 97.2 1.5 Spillway 1.2 N/A 72
Spillway End Slopes = Freeboard above Max Water Surface = Routed Hydrograph Results Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow Q (cfs) = Ratio Peak Outflow D redevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 99% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) =	32.00 4.00 1.00 7he user can oven WQCV N/A 0.988 N/A N/A N/A N/A N/A N/A N/A N/A Plate N/A N/A N/A 40	feet H:V feet EURV N/A 3.420 N/A N/A N/A N/A N/A N/A N/A N/A Overflow Weir 1 N/A N/A N/A 20 N/A Overflow Weir 1 N/A N/A N/A S N/A N/A S N/A S N/A S N/A S N/A S N/A S N/A N/A S N/A N/A S N/A N/A S N/A N/A S N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	Operation Operation <t< td=""><td>d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7 2.3 Plate N/A N/A N/A 70 74</td><td>Stage at 1 Basin Area at 1 Basin Volume at 1 I Ventering new value 10 Year 1.41 3.438 3.438 0.5 0.01 32.1 0.8 1.6 Plate N/A N/A 80 85</td><td>op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 12.2 0.24 56.4 11.9 1.0 Overflow Weir 1 0.4 N/A 83 90</td><td>0.94 8.38 1.66 8.16 drographs table (CC 50 Year 2.23 6.941 6.941 21.2 0.41 73.7 23.4 1.1 Overflow Weir 1 0.8 N/A 80 89</td><td>feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 34.2 <u>0.66</u> 96.5 31.2 0.9 Spillway 1.1 N/A 77 88</td><td>500 Year 3.83 14.217 14.217 64.3 1.25 151.3 97.2 1.5 Spillway 1.2 N/A 72 85</td></t<>	d runoff volumes by 5 Year 1.14 2.671 2.671 0.3 0.01 25.1 0.7 2.3 Plate N/A N/A N/A 70 74	Stage at 1 Basin Area at 1 Basin Volume at 1 I Ventering new value 10 Year 1.41 3.438 3.438 0.5 0.01 32.1 0.8 1.6 Plate N/A N/A 80 85	op of Freeboard = op of Freeboard = op of Freeboard = es in the Inflow Hy 25 Year 1.85 5.370 12.2 0.24 56.4 11.9 1.0 Overflow Weir 1 0.4 N/A 83 90	0.94 8.38 1.66 8.16 drographs table (CC 50 Year 2.23 6.941 6.941 21.2 0.41 73.7 23.4 1.1 Overflow Weir 1 0.8 N/A 80 89	feet feet acres acre-ft <u>100 Year</u> 2.66 9.020 9.020 34.2 <u>0.66</u> 96.5 31.2 0.9 Spillway 1.1 N/A 77 88	500 Year 3.83 14.217 14.217 64.3 1.25 151.3 97.2 1.5 Spillway 1.2 N/A 72 85



Outflow Hydrograph Workbook Filename:

Inflow Hydrograph	
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[SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
me Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.16	0.15	1.23
	0:15:00	0.00	0.00	0.53	1.43	2.16	1.85	2.80	3.03	5.99
	0:20:00	0.00	0.00	3.91	6.17	8.19	6.28	8.33	9.51	15.53
	0:25:00	0.00	0.00	10.46	15.13	20.01	14.56	18.97	22.06	38.26
-	0:30:00	0.00	0.00	15.70	22.56	29.30	33.58	44.44	54.28	89.28
-	0:35:00	0.00	0.00	17.63	25.06	32.14	49.50	65.18	82.94	132.23
ŀ	0:40:00	0.00	0.00	17.61	24.67	31.51	56.25	73.59	94.87	149.50
-	0:50:00	0.00	0.00	16.67 15.58	23.26 21.89	29.66 27.78	56.42 53.87	73.67 70.36	96.49 92.96	151.32 145.83
-	0:55:00	0.00	0.00	14.61	20.59	26.05	50.43	65.84	87.95	138.14
l l	1:00:00	0.00	0.00	13.82	19.42	24.62	46.56	60.65	82.66	130.13
	1:05:00	0.00	0.00	13.21	18.47	23.48	43.28	56.27	78.27	123.54
	1:10:00	0.00	0.00	12.45	17.58	22.41	40.07	52.02	72.60	114.71
-	1:15:00	0.00	0.00	11.56	16.55	21.30	36.88	47.82	65.94	104.26
-	1:20:00	0.00	0.00	10.66	15.36	19.97	33.55	43.38	58.87	92.96
-	1:25:00	0.00	0.00	9.84	14.22	18.43	30.24	38.96	51.90	81.70
ŀ	1:30:00	0.00	0.00	9.22	13.34	17.11	27.09	34.77	45.66	71.75
-	1:40:00	0.00	0.00	8.78 8.43	12.73 12.05	16.10 15.24	24.52 22.53	31.40 28.78	40.78 37.02	64.04 58.01
ŀ	1:45:00	0.00	0.00	8.12	11.30	13.24	22.35	26.55	33.81	52.81
1	1:50:00	0.00	0.00	7.81	10.58	13.74	19.35	24.55	30.91	48.11
	1:55:00	0.00	0.00	7.31	9.89	12.97	17.95	22.70	28.24	43.76
	2:00:00	0.00	0.00	6.70	9.20	12.06	16.62	20.93	25.70	39.64
-	2:05:00	0.00	0.00	5.91	8.16	10.66	14.73	18.49	22.56	34.65
-	2:10:00	0.00	0.00	5.04	6.96	9.05	12.54	15.69	19.13	29.27
-	2:15:00 2:20:00	0.00	0.00	4.21	5.79	7.50	10.39	12.94	15.78	24.05
ŀ	2:25:00	0.00	0.00	3.44 2.78	4.72 3.81	6.11 4.95	8.39 6.61	10.41 8.14	12.65 9.81	19.18 14.78
-	2:30:00	0.00	0.00	2.27	3.11	4.07	5.07	6.19	7.35	11.13
-	2:35:00	0.00	0.00	1.88	2.58	3.41	4.01	4.89	5.69	8.63
	2:40:00	0.00	0.00	1.57	2.17	2.86	3.23	3.93	4.48	6.78
	2:45:00	0.00	0.00	1.31	1.81	2.39	2.62	3.18	3.52	5.30
	2:50:00	0.00	0.00	1.09	1.50	1.98	2.11	2.55	2.75	4.12
-	2:55:00	0.00	0.00	0.90	1.24	1.63	1.71	2.06	2.15	3.19
-	3:00:00	0.00	0.00	0.75	1.01	1.33	1.38	1.66	1.67	2.46
-	3:05:00 3:10:00	0.00	0.00	0.62	0.83	1.09	1.13	1.35	1.33	1.95
-	3:15:00	0.00	0.00	0.51	0.68	0.89	0.92	1.10 0.88	1.08 0.87	1.58 1.27
-	3:20:00	0.00	0.00	0.33	0.43	0.56	0.58	0.69	0.70	1.01
ľ	3:25:00	0.00	0.00	0.25	0.33	0.43	0.45	0.54	0.54	0.78
	3:30:00	0.00	0.00	0.19	0.24	0.32	0.34	0.40	0.41	0.58
	3:35:00	0.00	0.00	0.13	0.17	0.23	0.24	0.29	0.29	0.41
-	3:40:00	0.00	0.00	0.08	0.12	0.15	0.16	0.19	0.19	0.27
-	3:45:00	0.00	0.00	0.05	0.07	0.09	0.10	0.11	0.11	0.16
ŀ	3:50:00	0.00	0.00	0.02	0.04	0.05	0.05	0.06	0.06	0.08
ŀ	3:55:00 4:00:00	0.00	0.00	0.01	0.02	0.02	0.02	0.02	0.02	0.02
-	4:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	4:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:25:00 4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
F	4:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	4:45:00 4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
F	5:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:05:00 5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:30:00 5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ļ	5:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
-	5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:55:00 6:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021) Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Volume [ac-ft]	V	Total Outflow [cfs]	
		F	For best results, include the
			stages of all grade slope
			changes (e.g. ISV and Floor) from the S-A-V table on
		f	rom the S-A-V table on
	-		Sheet 'Basin'.
	-	+l,	Nee include the inverte of all
			Also include the inverts of all outlets (e.g. vertical orifice,
	-		overflow grate, and spillway,
	_		where applicable).
	_		
	_		
	_		
	_		
	_		
	_		
	_		
	_		
	1	1	
	-		
		+	
	+	+	
	-	+	
	+	+	
	_		
		+	
	-	+	
	-	+	
	-		
1		1	
	-	+	
	-	+	
		+	
1		+	

Pond B Forebay Notch

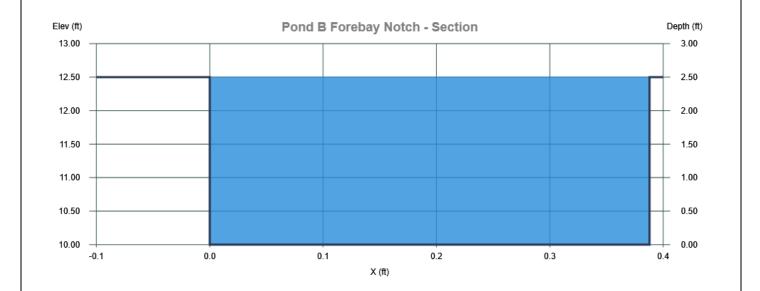
04-01-2021

Channel 1

Project Name: New Project

RECTANGULAR		DISCHARGE	
Bottom Width	= 0.39 ft	Method	= Known Q
Total Depth	= 2.50 ft	Known Q	= 1.93 cfs
Invert Elevation	= 10.00 ft		
Channel Slope	= 0.300 %		
Manning's n	= 0.013		

Flow	Depth	Area	Velocity	WP	n-value	Crit Depth	HGL	EGL	Max Shear	Top Width
(cfs)	(ft)	(sqft)	(ft/s)	(ft)		(ft)	(ft)	(ft)	(lb/sqft)	(ft)
1.93	2.50	0.97	1.99	5.39	0.013	0.92	12.50	12.56	0.47	0.39



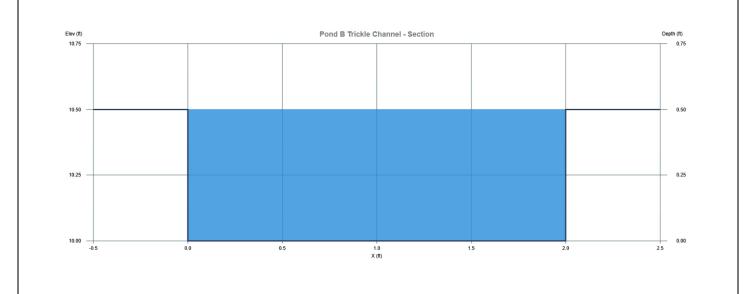
Pond B Trickle Channel

04-09-2021

Channel 2

RECTANGULAR		DISCHARGE	
Bottom Width	= 2.00 ft	Method	= Q vs Depth
Total Depth	= 0.50 ft	Q Min	= 0.08 cfs
Invert Elevation	= 10.00 ft	Q Max	= 3.01 cfs
Channel Slope	= 0.300 %	Increments	= 10
Manning's n	= 0.013		

Flow	Depth	Area	Velocity	WP	n-value	Crit Depth	HGL	EGL	Max Shear	Top Width
(cfs)	(ft)	(sqft)	(ft/s)	(ft)		(ft)	(ft)	(ft)	(lb/sqft)	(ft)
3.01	0.50	1.00	3.01	3.00	0.013	0.42	10.50	10.64	0.09	2.00



Depth Increment = 1.00 ft

ZONE	1 AND 2	ORIFICE	R		Depth Increment =	1.00	ft				Ontional		
PERMANENT ORIFI		on (Retentio	on Pond)		Stage - Storage	Stage	Optional Override	Length	Width	Area	Optional Override	Area	Volume
Example Lone	oomgalaa		,, o		Description	(ft)	Stage (ft)	(ft)	(ft)	(ft ²)	Area (ft ²)	(acre)	(ft 3)
Watershed Information					Top of Micropool		0.00				0	0.000	
Selected BMP Type =	EDB	1			4863		0.79				2,680	0.062	1,058
Watershed Area =	144.88	acres			4864		1.79				37,698	0.865	21,247
Watershed Length =	5,740	-					2.79				91,521	2.101	85,856
Watershed Length = Watershed Length to Centroid =	2,455	ft ft			4865 4866		3.79				91,521 98,660	2.101	180,947
Watershed Length to Centrold = Watershed Slope =	0.008	ft/ft			4867		4.79				102,931	2.363	281,742
		-											
Watershed Imperviousness =	49.00%	percent			4868		5.79				107,997	2.479	387,206
Percentage Hydrologic Soil Group A =	100.0%	percent			4869		6.79				113,712	2.610	498,061
Percentage Hydrologic Soil Group B =	0.0%	percent			4869.71		7.50				118,652	2.724	580,550
Percentage Hydrologic Soil Groups C/D =	0.0%	percent			4870		7.79				121,268	2.784	615,339
Target WQCV Drain Time =	40.0	hours			4871		8.79				124,198	2.851	738,072
Location for 1-hr Rainfall Depths =	User Input				4871.2		8.99				125,693	2.886	763,061
After providing required inputs above in													
depths, click 'Run CUHP' to generate run													
the embedded Colorado Urban Hydro	ograph Proced	ure.	Optional Use	er Overrides									
Water Quality Capture Volume (WQCV) =	2.457	acre-feet		acre-feet									
Excess Urban Runoff Volume (EURV) =	8.139	acre-feet		acre-feet									
2-yr Runoff Volume (P1 = 0.86 in.) =	4.248	acre-feet	0.86	inches									
5-yr Runoff Volume (P1 = 1.14 in.) =	5.786	acre-feet	1.14	inches									
10-yr Runoff Volume (P1 = 1.41 in.) =	7.539	acre-feet	1.41	inches									
25-yr Runoff Volume (P1 = 1.85 in.) =	10.932	acre-feet	1.85	inches									
50-yr Runoff Volume (P1 = 2.23 in.) =	14.760	acre-feet	2.23	inches									
		-		-									
100-yr Runoff Volume (P1 = 2.66 in.) =	19.737	acre-feet	2.66	inches									
500-yr Runoff Volume (P1 = 3.83 in.) =	33.551	acre-feet	3.83	inches									
Approximate 2-yr Detention Volume =	3.779	acre-feet											
Approximate 5-yr Detention Volume =	5.235	acre-feet											
Approximate 10-yr Detention Volume =	6.779	acre-feet											
Approximate 25-yr Detention Volume =	9.533	acre-feet											
Approximate 50-yr Detention Volume =	11.412	acre-feet											
Approximate 100-yr Detention Volume =	13.730	acre-feet											
•		-											
Define Zones and Basin Geometry													
	2.457	acre-feet											
Zone 1 Volume (WQCV) =	-												
Zone 2 Volume (EURV - Zone 1) =	5.682	acre-feet											
Zone 3 Volume (100-year - Zones 1 & 2) =	5.591	acre-feet											
Total Detention Basin Volume =	13.730	acre-feet											
Initial Surcharge Volume (ISV) =	user	ft ³											
Initial Surcharge Depth (ISD) =	user	ft											
Total Available Detention Depth (H _{total}) =	user	ft											
Depth of Trickle Channel (H _{TC}) =	user	ft											
Slope of Trickle Channel (STC) =	user	ft/ft											
Slopes of Main Basin Sides (S _{main}) =	user	H:V											
		1											
Basin Length-to-Width Ratio $(R_{L/W}) =$	user												
		٦.											
Initial Surcharge Area (A _{ISV}) =	user	ft ²											
Surcharge Volume Length $(L_{ISV}) =$	user	ft											
Surcharge Volume Width $(W_{ISV}) =$	user	ft											
Depth of Basin Floor (H _{FLOOR}) =	user	ft											
Length of Basin Floor $(L_{FLOOR}) =$	user	ft											
Width of Basin Floor (W _{FLOOR}) =	user	ft											
Area of Basin Floor (A _{FLOOR}) =	user	ft ²											
Volume of Basin Floor (V _{FLOOR}) =	user	ft ³											
Depth of Main Basin (H _{MAIN}) =	user	ft											
		-											
Length of Main Basin (L _{MAIN}) =	user	ft A											
Width of Main Basin (W _{MAIN}) =	user	ft											
Area of Main Basin (A _{MAIN}) =	user	ft ²											
Volume of Main Basin (V _{MAIN}) =	user	ft ³											L
Calculated Total Basin Volume (V_{total}) =	user	acre-feet											
												-	
												-	
													-

Volume (ac-ft)

0.024

0.488

1.971

4.154

6.468

8.889

11.434

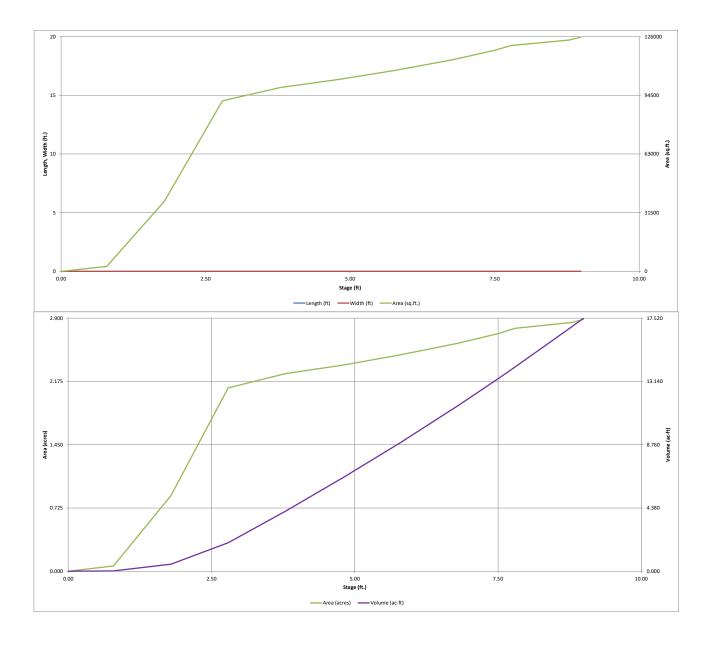
13.328

14.126

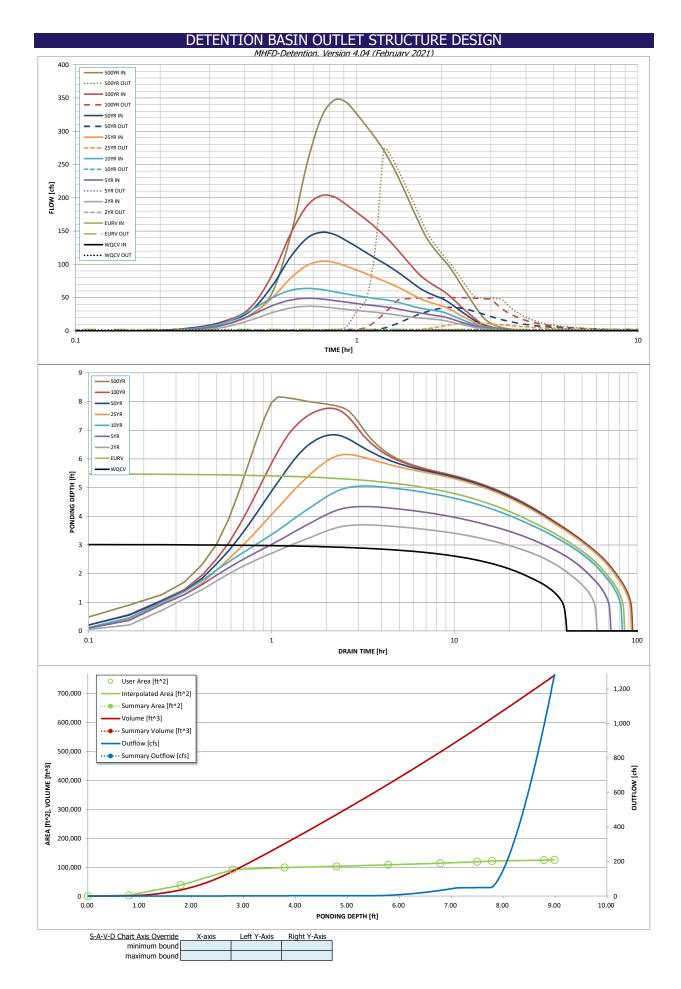
16.944

17.517

MHFD-Detention, Version 4.04 (February 2021)



		MHI	-D-Detention, vers	ion 4.04 (Februar	y 2021)				
	Pioneer Village								
Basin ID:	Pond C (PA's 17 a	nd 21)							
ZONE 2	\bigcirc			Estimated	Estimated				
100-YR				Stage (ft)	Volume (ac-ft)	Outlet Type			
			Zone 1 (WQCV)	3.02	2.457	Orifice Plate			
i land	100-YEAR ORIFICE		Zone 2 (EURV)	5.49	5.682	Orifice Plate			
PERMANENT ORIFICES			Zone 3 (100-year)	7.65	5.591	Weir&Pipe (Restrict)			
POOL Example Zone	Configuration (Re	tention Pond)		Total (all zones)	13.730				
User Input: Orifice at Underdrain Outlet (typical	y used to drain WC	CV in a Filtration Bl	MP)			1	Calculated Parame	eters for Underdrain	
Underdrain Orifice Invert Depth =			the filtration media	surface)	Underd	rain Orifice Area =		ft ²	
Underdrain Orifice Diameter =	N/A	inches			Underdrain	Orifice Centroid =	N/A	feet	
User Input: Orifice Plate with one or more orific	es or Elliptical Slot	Weir (typically used	l to drain WQCV and	l/or EURV in a sed	mentation BMP)		Calculated Parame	ters for Plate	
Invert of Lowest Orifice =	0.00	ft (relative to basir	bottom at Stage =	0 ft)	WQ Orifi	ce Area per Row =	7.882E-02	ft ²	
Depth at top of Zone using Orifice Plate =	5.49	ft (relative to basir	bottom at Stage =	0 ft)	Elli	ptical Half-Width =	N/A	feet	
Orifice Plate: Orifice Vertical Spacing =	22.00	inches			Ellipti	cal Slot Centroid =	N/A	feet	
Orifice Plate: Orifice Area per Row =	11.35	sq. inches (use rec	tangular openings)		E	lliptical Slot Area =	N/A	ft ²	
User Input: Stage and Total Area of Each Orific	e Row (numbered f	rom lowest to highe	est)						
	Row 1 (required)	Row 2 (optional)	Row 3 (optional)	Row 4 (optional)	Row 5 (optional)	Row 6 (optional)	Row 7 (optional)	Row 8 (optional)	
Stage of Orifice Centroid (ft)		1.83	3.66						
Orifice Area (sq. inches)	11.35	11.35	11.35						
	Row 9 (optional)	Row 10 (optional)	Row 11 (optional)	Row 12 (optional)	Row 13 (optional)	Row 14 (optional)	Row 15 (optional)	Row 16 (optional)	
Stage of Orifice Centroid (ft)									
Orifice Area (sq. inches)									
									-
User Input: Vertical Orifice (Circular or Rectang	ular)		_	-			Calculated Parame	eters for Vertical Orif	fice
	Not Selected	Not Selected					Not Selected	Not Selected]
Invert of Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	= 0 ft) Ver	tical Orifice Area =	N/A	N/A	ft ²
Depth at top of Zone using Vertical Orifice =	N/A	N/A	ft (relative to basin	bottom at Stage =	= 0 ft) Vertical	Orifice Centroid =	N/A	N/A	feet
Vertical Orifice Diameter =	N/A	N/A	inches					•	•
User Input: Overflow Weir (Dropbox with Flat o	r Sloped Grate and	Outlet Pipe OR Rec	tangular/Trapezoid	al Weir (and No Ou	tlet Pipe)		Calculated Parame	eters for Overflow W	/eir
	Zone 3 Weir	Not Selected					Zone 3 Weir	Not Selected]
Overflow Weir Front Edge Height, Ho =	5.49	N/A	ft (relative to basin b	ottom at Stage = 0 f	t) Height of Grate	e Upper Edge, H _t =	6.66		feet
Overflow Weir Front Edge Length =	8.00	N/A	feet		Overflow W	eir Slope Length =	4.81	N/A	feet
Overflow Weir Grate Slope =	4.00	N/A	H:V	Gr	ate Open Area / 10	0-yr Orifice Area =	6.82	N/A	1
Horiz. Length of Weir Sides =	4.67	N/A	1						
Overflow Grate Type =			feet	0\	erflow Grate Open	Area w/o Debris =	26.80		ft ²
Overnow Grate Type –	Type C Grate	N/A	reet		•		26.80 26.80	N/A	ft ² ft ²
Debris Clogging % =		N/A	w		erflow Grate Open			N/A	
		N/A			erflow Grate Open			N/A	
	0%	N/A N/A	%		verflow Grate Open Overflow Grate Oper	n Area w/ Debris =	26.80	N/A	ft²
Debris Clogging % =	0%	N/A N/A	%		verflow Grate Open Overflow Grate Oper	n Area w/ Debris =	26.80	N/A N/A	ft²
Debris Clogging % =	0% e (Circular Orifice, R	N/A N/A estrictor Plate, or R	%	c	verflow Grate Open Sverflow Grate Open <u>Ca</u>	n Area w/ Debris =	26.80 s for Outlet Pipe w/	N/A N/A / Flow Restriction Pla Not Selected	ft²
Debris Clogging % =	0% e (Circular Orifice, R Zone 3 Restrictor	N/A N/A estrictor Plate, or R Not Selected N/A	% ectangular Orifice)	c	verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) Ou	n Area w/ Debris =	26.80 s for Outlet Pipe w/ Zone 3 Restrictor	N/A N/A / Flow Restriction Pla Not Selected N/A	ft ²
Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe =	0% e (Circular Orifice, R Zone 3 Restrictor 0.25 30.00	N/A N/A estrictor Plate, or R Not Selected N/A	% tectangular Orifice) ft (distance below ba	C sin bottom at Stage	verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) Ou	n Area w/ Debris = Iculated Parameters utlet Orifice Area = : Orifice Centroid =	26.80 s for Outlet Pipe w/ Zone 3 Restrictor 3.93	N/A N/A / Flow Restriction Pla Not Selected N/A	ft ²
Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	0% e (Circular Orifice, R Zone 3 Restrictor 0.25 30.00	N/A N/A estrictor Plate, or R Not Selected N/A	% (ectangular Orifice) ft (distance below ba inches	C sin bottom at Stage	verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) Ou Outlet	n Area w/ Debris = Iculated Parameters utlet Orifice Area = : Orifice Centroid =	26.80 s for Outlet Pipe w/ Zone 3 Restrictor 3.93 1.03	N/A N/A / Flow Restriction Pla Not Selected N/A N/A	ft ² ate ft ² feet
Debris Clogging % = User Input: Outlet Pipe w/ Flow Restriction Plate Depth to Invert of Outlet Pipe = Outlet Pipe Diameter =	0% e (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 22.40	N/A N/A estrictor Plate, or R Not Selected N/A	% (ectangular Orifice) ft (distance below ba inches	C sin bottom at Stage	verflow Grate Open Overflow Grate Open <u>Ca</u> = 0 ft) Ou Outlet	n Area w/ Debris = Iculated Parameters utlet Orifice Area = : Orifice Centroid =	26.80 s for Outlet Pipe w/ Zone 3 Restrictor 3.93 1.03	N/A N/A / Flow Restriction Pla Not Selected N/A N/A N/A	ft ² ate ft ² feet
Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert =	0% 2 (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 22.40 Trapezoidal)	N/A N/A estrictor Plate, or R Not Selected N/A N/A	% (ectangular Orifice) ft (distance below ba inches	C sin bottom at Stage Half-Cent	verflow Grate Open Iverflow Grate Open <u>Ca</u> = 0 ft) Ot Outlet ral Angle of Restrict	n Area w/ Debris = Iculated Parameters utlet Orifice Area = : Orifice Centroid =	26.80 <u>5 for Outlet Pipe w/</u> Zone 3 Restrictor 3.93 1.03 2.09	N/A N/A / Flow Restriction Pla Not Selected N/A N/A N/A	ft ² ate ft ² feet
Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u>	0% 2 (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 22.40 Trapezoidal)	N/A N/A estrictor Plate, or R Not Selected N/A N/A	% (<u>tectangular Orifice)</u> ft (distance below ba jinches inches	C sin bottom at Stage Half-Cent	verflow Grate Open Iverflow Grate Open (<u>Ca</u> = 0 ft) Or Outlet ral Angle of Restrict Spillway Do	n Area w/ Debris = lculated Parameters utlet Orifice Area = : Orifice Centroid = tor Plate on Pipe =	26.80 5 for Outlet Pipe w/ Zone 3 Restrictor 3.93 1.03 2.09 Calculated Parame	N/A N/A / Flow Restriction Pla Not Selected N/A N/A N/A	ft ² ate ft ² feet
Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage=	0% <u>2 (Circular Orifice, R</u> <u>2 one 3 Restrictor</u> 0.25 <u>30.00</u> 22.40 <u>7 rapezoidal</u> <u>7.77</u> <u>300.00</u>	N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin	% (<u>tectangular Orifice)</u> ft (distance below ba jinches inches	C sin bottom at Stage Half-Cent	verflow Grate Open overflow Grate Open <u>Ca</u> = 0 ft) Or Outlet ral Angle of Restrict Spillway Dr Stage at T	h Area w/ Debris = <u>lculated Parameters</u> utlet Orifice Area = : Orifice Centroid = tor Plate on Pipe = esign Flow Depth=	26.80 <u>s for Outlet Pipe w/</u> Zone 3 Restrictor 3.93 1.03 2.09 <u>Calculated Parame</u> 0.37	N/A N/A / Flow Restriction Pla Not Selected N/A N/A N/A N/A eters for Spillway feet	ft ² ate ft ² feet
Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length =	0% <u>2 (Circular Orifice, R</u> <u>2 one 3 Restrictor</u> 0.25 <u>30.00</u> 22.40 <u>7 rapezoidal</u> <u>7.77</u> <u>300.00</u>	N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet	% (<u>tectangular Orifice)</u> ft (distance below ba jinches inches	C sin bottom at Stage Half-Cent	verflow Grate Open overflow Grate Open (<u>Ca</u> = 0 ft) Or Outlet ral Angle of Restrict Spillway Dr Stage at T Basin Area at T	h Area w/ Debris = <u>lculated Parameter</u> : utlet Orifice Area = Orifice Centroid = tor Plate on Pipe = esign Flow Depth= op of Freeboard =	26.80 <u>5 for Outlet Pipe w/</u> Zone 3 Restrictor 3.93 1.03 2.09 <u>Calculated Parame</u> 0.37 9.14 2.89	N/A N/A Not Selected N/A N/A N/A eters for Spillway feet feet	ft ² ate ft ² feet
Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes =	0% <u>2 (Circular Orifice, R</u> <u>2 one 3 Restrictor</u> 0.25 <u>30.00</u> 22.40 <u>Trapezoidal</u>) <u>7.77</u> <u>300.00</u> <u>4.00</u>	N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V	% (<u>tectangular Orifice)</u> ft (distance below ba jinches inches	C sin bottom at Stage Half-Cent	verflow Grate Open overflow Grate Open (<u>Ca</u> = 0 ft) Or Outlet ral Angle of Restrict Spillway Dr Stage at T Basin Area at T	h Area w/ Debris = <u>lculated Parameter</u> : utlet Orifice Area = Orifice Centroid = tor Plate on Pipe = esign Flow Depth = Top of Freeboard = Top of Freeboard =	26.80 <u>5 for Outlet Pipe w/</u> <u>Zone 3 Restrictor</u> <u>3.93</u> 1.03 2.09 <u>Calculated Parame</u> 0.37 <u>9.14</u> 2.89	N/A N/A N/A N/A N/A N/A N/A eters for Spillway feet feet acres	ft ² ate ft ² feet
Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface =	0% 2 (Circular Orifice, R 2 one 3 Restrictor 0.25 30.00 22.40 Trapezoidal) 7.77 300.00 4.00 1.00	N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basin feet H:V feet	% (<u>tectangular Orifice)</u> ft (distance below ba inches inches bottom at Stage =	c sin bottom at Stage Half-Cent 0 ft)	verflow Grate Open Iverflow Grate Open (Ca = 0 ft) Or Outlet ral Angle of Restrict Spillway D Stage at T Basin Area at T Basin Volume at T	h Area w/ Debris = <u>lculated Parameters</u> utlet Orifice Area = : Orifice Centroid = tor Plate on Pipe = esign Flow Depth = :op of Freeboard = :op of Freeboard = :op of Freeboard =	26.80 5 for Outlet Pipe w/ Zone 3 Restrictor 3.93 1.03 2.09 <u>Calculated Parame</u> 0.37 9.14 2.89 17.52	N/A N/A Not Selected N/A N/A N/A ters for Spillway feet feet acres acre-ft	ft ² ft ² feet radians
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Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = CUHP Runoff Volume (acre-ft) = CUHP Runoff Volume (acre-ft) = CUHP Redevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Inflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) =	0% (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 22.40 Trapezoidal) 7.77 300.00 4.00 1.00 7he user can oven WQCV N/A 2.457 N/A	N/A N/A N/A estrictor Plate, or R N/A N/A N/A ft (relative to basin feet H:V feet EURV EURV N/A 8.139 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	% (cectangular Orifice) (ft (distance below ba inches (inches) bottom at Stage = (HP hydrographs and 2 Year 0.86 4.248 4.248 0.0 0.00 37.0 1.3 N/A Plate N/A Plate N/A S56	Sin bottom at Stage Half-Cent 0 ft) 1 runoff volumes by 5 Year 1.14 5.786 5.786 0.4 0.4 0.00 48.9 0.4 0.00 48.9 1.7 4.5 Plate N/A 66	erflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open (2) (2) (2) (2) (2) (2) (2) (3) (4) (4) (4) (5) (4) (5) (5) (5) (5) (5) (5) (5) (5	n Area w/ Debris = lculated Parameters utlet Orifice Area = : Orifice Centroid = tor Plate on Pipe = esign Flow Depth = iop of Freeboard = iop of Freeboard = iop of Freeboard = es in the Inflow Hyy 25 Year 1.85 10.932 5.8 0.04 104.6 11.8 2.0 Overflow Weir 1 0.4 N/A 83	26.80 2000 3 Restrictor 3.93 1.03 2.09 <u>Calculated Parame</u> 0.37 9.14 2.89 17.52 <i>drographs table (Colored States)</i> 14.760 15.74 15.74 15.74 15.74 15.75 15.74 15.75 15.	N/A N/A N/A N/A N/A N/A N/A N/A N/A ters for Spillway feet feet acres acre-ft 00 Year 2.66 19.737 19.737 19.737 55.0 0.38 203.4 50.1 0.9 Spillway 1.8 N/A 78	ft ² ft ² feet radians 500 Year 3.83 33.551 33.551 33.551 138.2 0.95 346.7 272.0 2.0 Spillway 1.8 N/A 72
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Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = Inflow Hydrograph Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = OPTIONAL Override Predevelopment Peak Q (cfs) = Peak Inflow Q (cfs) = Peak Outflow to Predevelopment Q = Structure Controlling Flow = Max Velocity through Grate 1 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 99% of Inflow Volume (hours) = Maximum Ponding Depth (ft) =	0% 2 (Circular Orifice, R 2 one 3 Restrictor 0.25 3 0.00 22.40 Trapezoidal) 7.77 3 00.00 4.00 1.00 7 he user can oven WOCV N/A 2.457 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A 1.1 N/A N/A 1.1 N/A 1.1 N/A 1.2	N/A N/A N/A estrictor Plate, or R N/A N/A N/A ft (relative to basin feet H:V feet <i>ride the default CU/I</i> EURV N/A 8.139 N/A N/A N/A N/A N/A N/A N/A Overflow Weir 1 N/A N/A N/A N/A S N/A N/A N/A N/A N/A N/A N/A N/A N/A	% <pre> % % % % % % % % % % % % % % % % % % %</pre>	Sin bottom at Stage Half-Cent 0 ft) 1.14 5.786 5.786 0.4 0.4 0.0 1.7 4.5 Plate N/A N/A 66 70 4.34	erflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open () () () () () () () () () ()	h Area w/ Debris = lculated Parameter: utlet Orifice Area = Orifice Centroid = tor Plate on Pipe = tor Plate on Pipe = tor Plate on Pipe = tor of Freeboard = op of Freeboard = op of Freeboard = op of Freeboard = tor pof Freeboard = 1.85 10.932 5.8 0.04 104.6 11.8 2.0 Overflow Weir 1 0.4 N/A 83 89 6.16	26.80 20ne 3 Restrictor 3.93 1.03 2.09 Calculated Parame 0.37 9.14 2.89 17.52 drographs table (CC 50 Year 2.23 14.760 14.760 14.760 26.5 0.18 148.1 35.4 1.3 Overflow Weir 1 1.2 N/A 81 89 6.85	N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	ft ² <u>ate</u> ft ² feet radians <u>500 Year</u> <u>3.83</u> <u>33.551</u> <u>33.551</u> <u>33.551</u> <u>33.551</u> <u>33.551</u> <u>33.551</u> <u>33.551</u> <u>33.651</u> <u>346.7</u> <u>272.0</u> <u>2.0</u> <u>59illway</u> <u>1.8</u> <u>N/A</u> <u>72</u> <u>85</u> <u>8.16</u>
Debris Clogging % = <u>User Input: Outlet Pipe w/ Flow Restriction Plate</u> Depth to Invert of Outlet Pipe = Outlet Pipe Diameter = Restrictor Plate Height Above Pipe Invert = <u>User Input: Emergency Spillway (Rectangular or</u> Spillway Invert Stage= Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway Crest Length = Spillway End Slopes = Freeboard above Max Water Surface = <u>Routed Hydrograph Results</u> Design Storm Return Period = One-Hour Rainfall Depth (in) = CUHP Runoff Volume (acre-ft) = UHP Runoff Volume (acre-ft) = CUHP Predevelopment Peak Q (cfs) = Predevelopment Unit Peak Flow, q (cfs/acre) = Peak Inflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Peak Outflow Q (cfs) = Ratio Peak Outflow to Predevelopment Q (cfs) = Ratio Peak Outflow for the Q (cfs) = Max Velocity through Grate 1 (fps) = Max Velocity through Grate 2 (fps) = Time to Drain 97% of Inflow Volume (hours) = Time to Drain 97% of Inflow Volume (hours) =	0% (Circular Orifice, R Zone 3 Restrictor 0.25 30.00 22.40 Trapezoidal) 7.77 300.00 4.00 1.00 The user can overn WOCV N/A 2.457 N/A	N/A N/A estrictor Plate, or R Not Selected N/A N/A ft (relative to basir feet H:V feet H:V feet EURV N/A 8.139 N/A N/A N/A N/A N/A N/A N/A N/A N/A N/A	% <pre>% ft (distance below ba inches inches inches h bottom at Stage = </pre> HP hydrographs and 2 Year 0.86 4.248 0.0 0.00 37.0 1.3 N/A Plate N/A N/A N/A S6 56 59	Sin bottom at Stage Half-Cent 0 ft) 1.14 5.786 0.4 0.4 0.00 48.9 1.7 4.5 Plate N/A N/A N/A N/A 66 70	erflow Grate Open verflow Grate Open verflow Grate Open verflow Grate Open () () () () () () () () () ()	h Area w/ Debris = lculated Parameters utlet Orifice Area = Orifice Centroid = tor Plate on Pipe = bor Plate on Pipe = bor of Freeboard = op of Freeboard = op of Freeboard = op of Freeboard = cop of Freeboard = 10.932 5.8 0.04 10.932 10.932 5.8 0.04 10.932 10.932 5.8 0.04 10.932 10.94 10.9	26.80 20ne 3 Restrictor 3.93 1.03 2.09 <u>Calculated Parame</u> 0.37 9.14 2.89 17.52 <i>trographs table (Co</i> 50 Year 2.23 14.760 26.5 0.18 148.1 35.4 1.3 Overflow Weir 1 1.2 N/A 81 89	N/A N/A N/A Not Selected N/A deters for Spillway feet feet acres acre-ft 000 Year 2.66 19.737 55.0 0.38 203.4 50.1 0.9 Spillway 1.8 N/A 78 88	ft ² <u>ate</u> ft ² feet radians <u>500 Year</u> <u>3.83</u> <u>33.551</u> <u>33.551</u> <u>138.2</u> <u>0.95</u> <u>346.7</u> <u>272.0</u> <u>2.0</u> <u>5pillway</u> <u>1.8</u> N/A <u>72</u> <u>85</u>



Outflow Hydrograph Workbook Filename:

Inflow Hydrographs

								l in a separate pr		
	SOURCE	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP	CUHP
Time Interval	TIME	WQCV [cfs]	EURV [cfs]	2 Year [cfs]	5 Year [cfs]	10 Year [cfs]	25 Year [cfs]	50 Year [cfs]	100 Year [cfs]	500 Year [cfs]
5.00 min	0:00:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	0:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.20	0.18	1.53
	0:15:00	0.00	0.00	0.65	1.76	2.63	2.26	3.56	3.86	8.35
	0:20:00	0.00	0.00	5.20	8.62	11.53	9.03	12.31	14.00	23.58
	0:25:00	0.00	0.00	15.79	22.74	29.92	22.44	28.95	34.05	56.65
	0:30:00	0.00	0.00	27.44	37.70	49.67	49.39	67.25	83.96	144.60
	0:35:00	0.00	0.00	34.59 37.02	46.44 48.92	60.98 63.83	79.57 98.51	111.75 139.45	146.69 188.12	252.30 321.34
	0:45:00	0.00	0.00	36.35	47.86	62.20	104.64	148.09	203.39	346.75
	0:50:00	0.00	0.00	34.36	45.51	58.77	102.95	144.86	201.18	343.61
	0:55:00	0.00	0.00	32.40	43.26	55.59	97.36	135.82	189.81	325.86
	1:00:00	0.00	0.00	30.64	41.09	52.77	91.31	126.40	177.88	307.14
	1:05:00	0.00	0.00	29.19	39.19	50.37	85.45	117.33	166.82	289.51
	1:10:00	0.00	0.00	27.91	37.73	48.61	79.94	109.00	155.34	270.53
	1:15:00	0.00	0.00	26.47	36.27	47.04	74.97	101.61	143.73	250.00
	1:20:00	0.00	0.00	24.92	34.51	45.14	70.04	94.38	131.59	227.85
	1:25:00	0.00	0.00	23.33	32.51	42.57	64.83	86.85	118.97	204.84
ŀ	1:30:00 1:35:00	0.00	0.00	21.76	30.47	39.61	59.43	79.17	106.73	182.64
	1:40:00	0.00	0.00	20.38 19.35	28.65 27.09	36.79 34.57	54.12 49.23	71.64 64.68	95.34 84.99	162.03 143.60
	1:45:00	0.00	0.00	19.35	27.09	34.57	49.23	59.52	77.38	143.60
·	1:50:00	0.00	0.00	18.03	23.07	31.61	42.53	55.52	71.51	119.83
	1:55:00	0.00	0.00	17.27	23.05	30.28	40.07	52.13	66.40	110.47
	2:00:00	0.00	0.00	16.23	21.80	28.79	37.81	48.99	61.74	101.92
	2:05:00	0.00	0.00	14.86	20.15	26.61	34.99	45.17	56.44	92.59
	2:10:00	0.00	0.00	13.24	18.05	23.81	31.40	40.42	50.27	82.08
	2:15:00	0.00	0.00	11.59	15.83	20.85	27.57	35.39	43.92	71.45
	2:20:00	0.00	0.00	10.05	13.69	18.01	23.86	30.50	37.84	61.33
	2:25:00	0.00	0.00	8.61	11.71	15.40	20.38	25.89	32.04	51.64
	2:30:00 2:35:00	0.00	0.00	7.27	9.89	13.01	17.15	21.59	26.57	42.51
·	2:40:00	0.00	0.00	6.03 4.89	8.19 6.68	10.80 8.85	14.11 11.34	17.57 13.89	21.38 16.57	33.82 25.79
	2:45:00	0.00	0.00	3.98	5.48	7.26	8.92	10.67	12.33	19.03
	2:50:00	0.00	0.00	3.30	4.58	6.09	7.04	8.37	9.43	14.59
	2:55:00	0.00	0.00	2.77	3.87	5.14	5.69	6.74	7.44	11.39
	3:00:00	0.00	0.00	2.33	3.25	4.32	4.66	5.51	5.91	8.91
	3:05:00	0.00	0.00	1.97	2.72	3.63	3.82	4.50	4.71	6.97
	3:10:00	0.00	0.00	1.66	2.28	3.04	3.15	3.70	3.77	5.47
	3:15:00	0.00	0.00	1.39	1.90	2.55	2.61	3.07	3.04	4.33
	3:20:00	0.00	0.00	1.16	1.58	2.12	2.15	2.52	2.45	3.44
	3:25:00	0.00	0.00	0.96	1.29	1.73	1.76	2.06	2.00	2.80
	3:30:00 3:35:00	0.00	0.00	0.78	1.04	1.40	1.42	1.66	1.62	2.26
·	3:40:00	0.00	0.00	0.63	0.82	1.11	1.13	1.32	1.30	1.80
	3:45:00	0.00	0.00	0.48	0.64	0.87	0.89	1.02 0.77	1.01 0.76	1.39
·	3:50:00	0.00	0.00	0.30	0.48	0.48	0.49	0.56	0.55	0.74
	3:55:00	0.00	0.00	0.17	0.24	0.33	0.34	0.38	0.37	0.48
ľ	4:00:00	0.00	0.00	0.10	0.15	0.21	0.22	0.24	0.22	0.29
	4:05:00	0.00	0.00	0.05	0.09	0.12	0.12	0.13	0.11	0.14
ŀ	4:10:00	0.00	0.00	0.02	0.04	0.05	0.05	0.05	0.04	0.04
ŀ	4:15:00 4:20:00	0.00	0.00	0.01	0.01	0.01	0.01	0.01	0.00	0.00
	4:25:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
·	4:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	4:40:00 4:45:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	4:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ľ	5:00:00 5:05:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:10:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:15:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:20:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:25:00 5:30:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:35:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:40:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ŀ	5:45:00 5:50:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
	5:55:00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

MHFD-Detention, Version 4.04 (February 2021) Summary Stage-Area-Volume-Discharge Relationships

The user can create a summary S-A-V-D by entering the desired stage increments and the remainder of the table will populate automatically. The user should graphically compare the summary S-A-V-D table to the full S-A-V-D table in the chart to confirm it captures all key transition points.

Stage - Storage Description	Stage [ft]	Area [ft ²]	Area [acres]	Volume [ft ³]	Volume [ac-ft]	Total Outflow [cfs]	
							For best results, include the
							stages of all grade slope
							changes (e.g. ISV and Floor from the S-A-V table on
	1						from the S-A-V table on
	-						Sheet 'Basin'.
							Also include the inverts of a
							outlets (e.g. vertical orifice,
							overflow grate, and spillway
							overflow grate, and spillway where applicable).
							-
							-
							-
							4
							_
							1
							1
							1
							1
			1				1
			1				1
							1
							-
							-
							-
							4
							4
							-
							-
							1
							1
							1
							-
							-
							-
							-
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	_		L				4
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							-
							4
							4
			1				1
]
]
							1
							4
							4
							4
							4
				1			1
							1
			1				1
]
]

Pond C Forebay 1 Notch

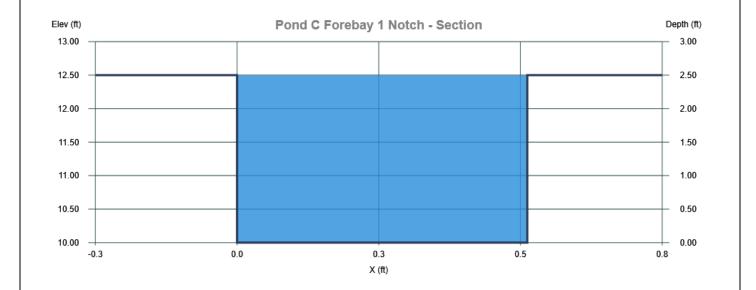
04-01-2021

Channel 1

Project Name: New Project

RECTANGULAR		DISCHARGE	
Bottom Width	= 0.51 ft	Method	= Known Q
Total Depth	= 2.50 ft	Known Q	= 3.01 cfs
Invert Elevation	= 10.00 ft		
Channel Slope	= 0.300 %		
Manning's n	= 0.013		

Flow	Depth	Area	Velocity	WP	n-value	Crit Depth	HGL	EGL	Max Shear	Top Width
(cfs)	(ft)	(sqft)	(ft/s)	(ft)		(ft)	(ft)	(ft)	(lb/sqft)	(ft)
3.01	2.49	1.27	2.36	5.49	0.013	1.03	12.49	12.58	0.47	0.51



Pond C Forebay 2 Notch

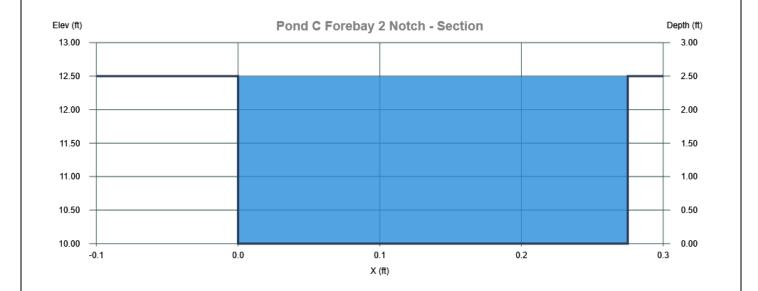
04-01-2021

Channel 1

Project Name: New Project

RECTANGULAR		DISCHARGE	
Bottom Width	= 0.28 ft	Method	= Known Q
Total Depth	= 2.50 ft	Known Q	= 1.10 cfs
Invert Elevation	= 10.00 ft		
Channel Slope	= 0.300 %		
Manning's n	= 0.013		

Flow	Depth	Area	Velocity	WP	n-value	Crit Depth	HGL	EGL	Max Shear	Top Width
(cfs)	(ft)	(sqft)	(ft/s)	(ft)		(ft)	(ft)	(ft)	(lb/sqft)	(ft)
1.10	2.49	0.68	1.61	5.25	0.013	0.80	12.49	12.53	0.47	0.28



Studio Express by Hydrology Studio v 1.0.0.9

Pond C Trickle Channel

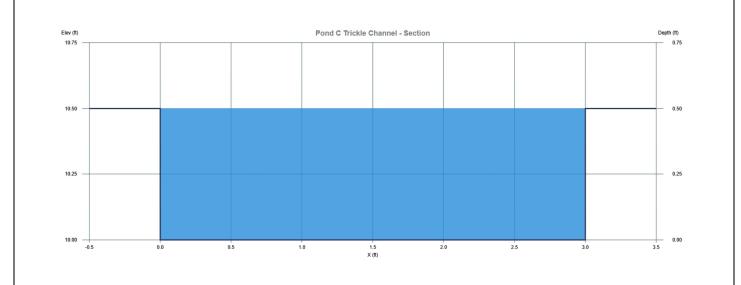
04-09-2021

Channel 3

RECTANGULAR		DISCHARGE	
Bottom Width	= 3.00 ft	Method	= Q vs Depth
Total Depth	= 0.50 ft	Q Min	= 0.12 cfs
Invert Elevation	= 10.00 ft	Q Max	= 4.88 cfs
Channel Slope	= 0.300 %	Increments	= 10
Manning's n	= 0.013		

CALCULATION SAMPLE

Flow	Depth	Area	Velocity	WP	n-value	Crit Depth	HGL	EGL	Max Shear	Top Width
(cfs)	(ft)	(sqft)	(ft/s)	(ft)		(ft)	(ft)	(ft)	(lb/sqft)	(ft)
4.88	0.50	1.50	3.25	4.00	0.013	0.44	10.50	10.66	0.09	3.00





NOTES TO USERS

This map is for use in administering the National Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

To obtain more detailed information in areas where **Base Flood Elevations** (BFEs) and/or **floodways** have been determined, users are encouraged to consult the Flood Profiles and Floodway Data and/or Summary of Stillwater Elevations tables contained within the Flood Insurance Study (FIS) Report that accompanies this FIRM. Users should be aware that BFEs shown on the FIRM represent rounded whole-foot elevations. These BFEs are intended for flood insurance rating purposes only and should not be used as the sole source of flood elevation information. Accordingly, flood elevation data presented in the FIS Report should be utilized in conjunction with the FIRM for purposes of construction and/or floodplain management.

Coastal Base Flood Elevations shown on this map apply only landward of 0.0' North American Vertical Datum of 1988 (NAVD 88). Users of this FIRM should be aware that coastal flood elevations are also provided in the Summary of Stillwater Elevations table in the Flood Insurance Study Report for this jurisdiction. Elevations shown in the Summary of Stillwater Elevations table should be used for construction and/or floodplain management purposes when they are higher than the elevations shown on this FIRM.

Boundaries of the floodways were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study Report for this jurisdiction.

Certain areas not in Special Flood Hazard Areas may be protected by flood control structures. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study Report for information on flood control structures for this jurisdiction.

The projection used in the preparation of this map was Universal Transverse Mercator (UTM) zone 13. The horizontal datum was NAD 83, GRS 1980 spheroid. Differences in datum, spheroid, projection or UTM zones used in the production of FIRMs for adjacent jurisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRM.

Flood elevations on this map are referenced to the North American Vertical Datum of 1988. These flood elevations must be compared to structure and ground elevations referenced to the same vertical datum. For information regarding conversion between the National Geodetic Vertical Datum of 1929 and the North American Vertical Datum of 1988, visit the National Geodetic Survey website at http://www.ngs.noaa.gov or contact the National Geodetic Survey at the following address:

NGS Information Services NOAA, N/NGS12 National Geodetic Survey SSMC-3, #9202 1315 East-West Highway Silver Spring, Maryland 20910-3282 (301) 713-3242

To obtain current elevation, description, and/or location information for bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 713- 3242, or visit its website at http://www.ngs.noaa.gov.

Base map information shown on this FIRM was derived from NAIP Orthophotography produced with a one meter ground resolution from photography dated 2013.

The **profile baselines** depicted on this map represent the hydraulic modeling baselines that match the flood profiles in the FIS report. As a result of improved topographic data, the profile baseline, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

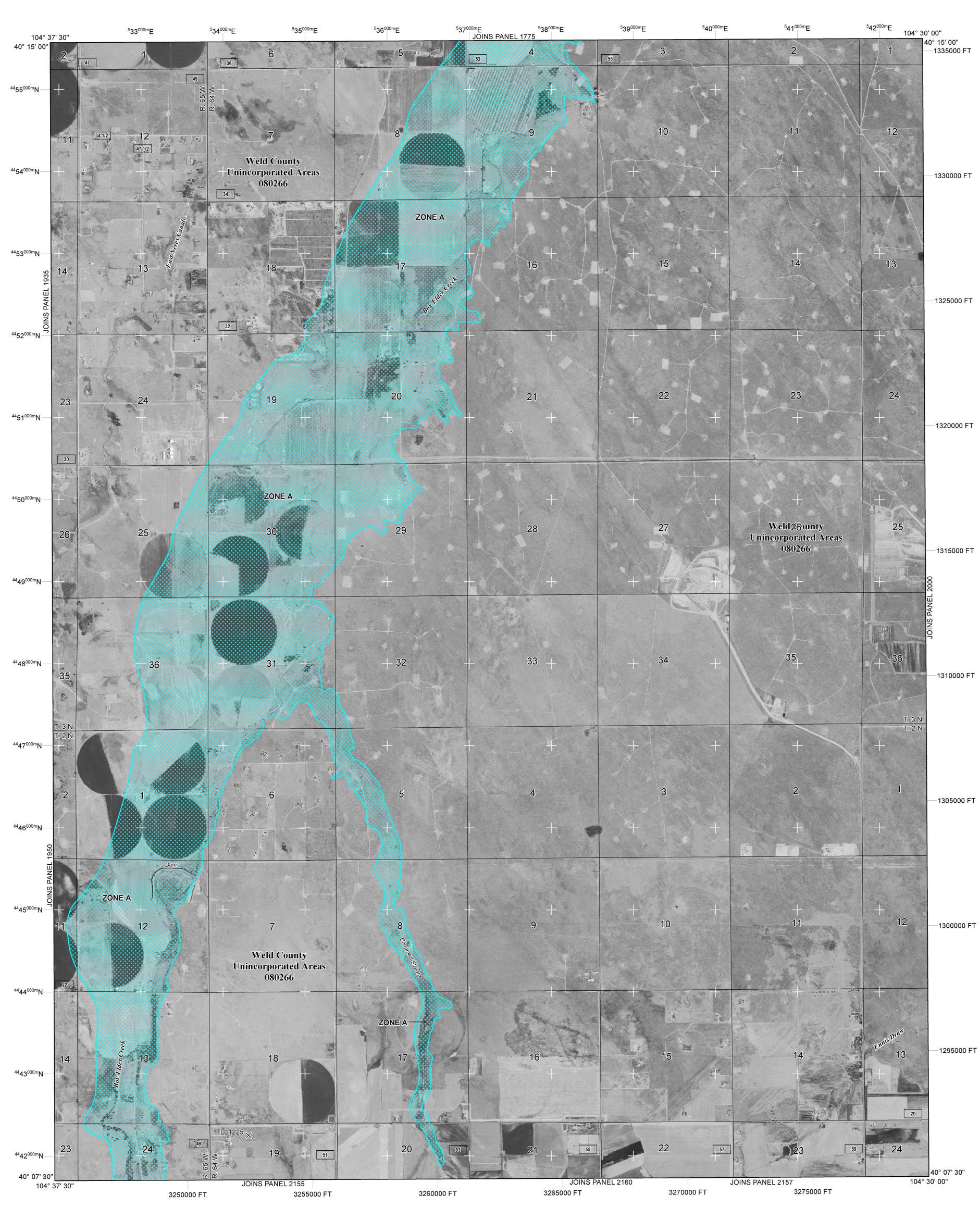
This map reflects more detailed and up-to-date stream channel configurations than those shown on the previous FIRM for this jurisdiction. The floodplains and podways that were transferred from the previous FIRM may have been adjusted to conform to these new stream channel configurations. As a result, the Flood Profiles and Floodway Data tables for multiple streams in the Flood Insurance Study Report (which contains authoritative hydraulic data) may reflect stream channel distances that differ from what is shown on this map.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this map was published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a Listing of Communities table containing National Flood Insurance Program dates for each community as well as a listing of the panels on which each community is located.

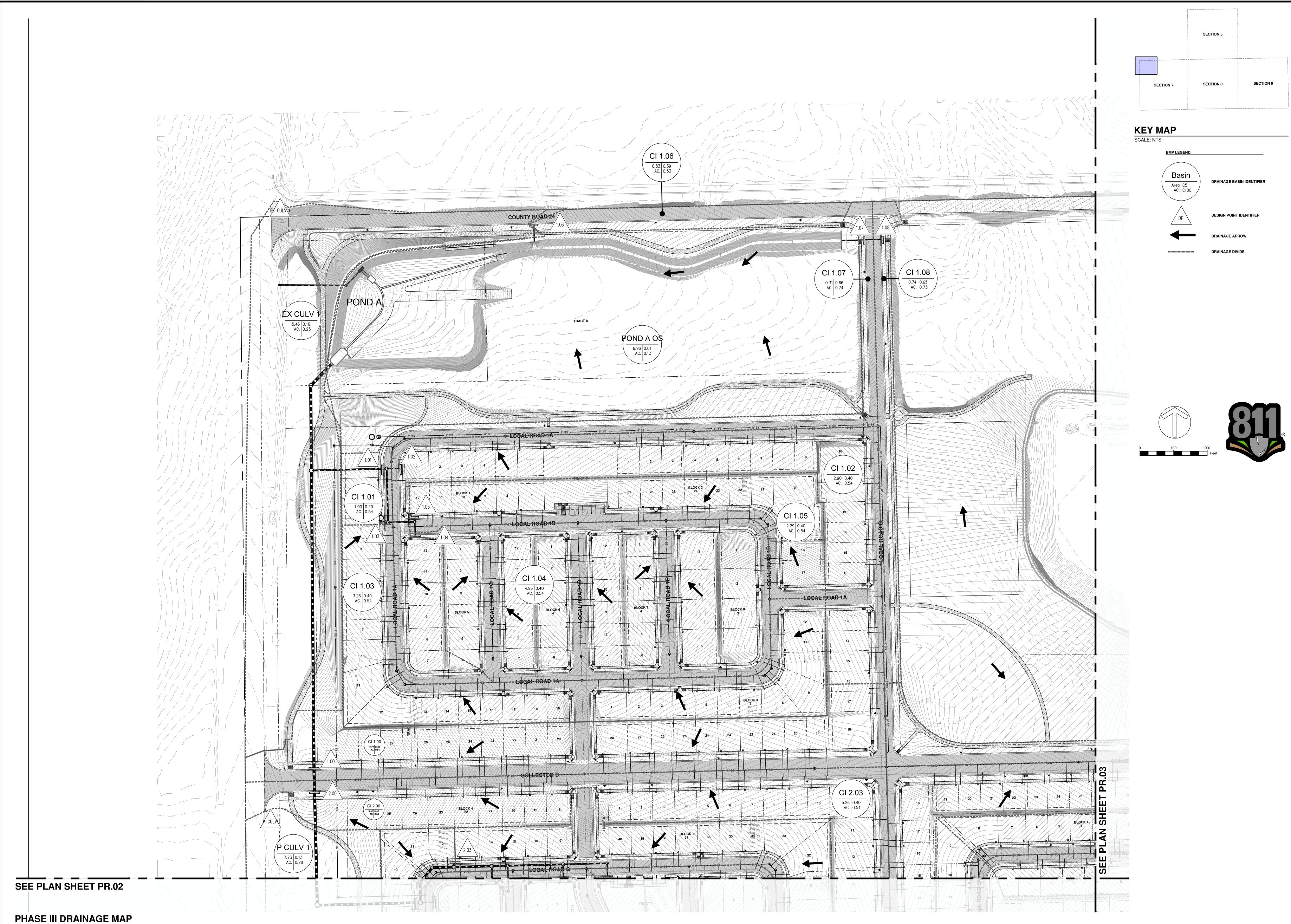
For information on available products associated with this FIRM visit the Map Service Center (MSC) website at http://msc.fema.gov. Available products may include previously issued Letters of Map Change, a Flood Insurance Study Report, and/or digital versions of this map. Many of these products can be ordered or obtained directly from the MSC website.

If you have questions about this map, how to order products, or the National Flood Insurance Program in general, please call the FEMA Map Information eXchange (FMIX) at 1-877-FEMA-MAP (1-877-336-2627) or visit the FEMA website at http://www.fema.gov/business/nfip.

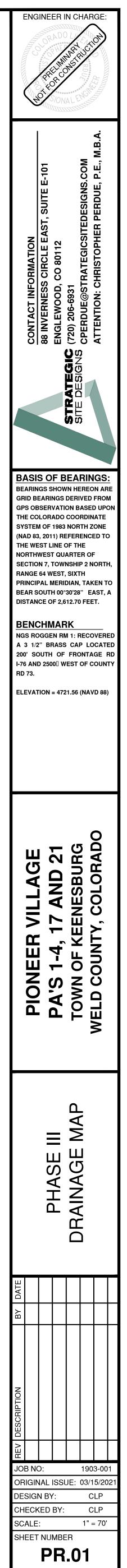


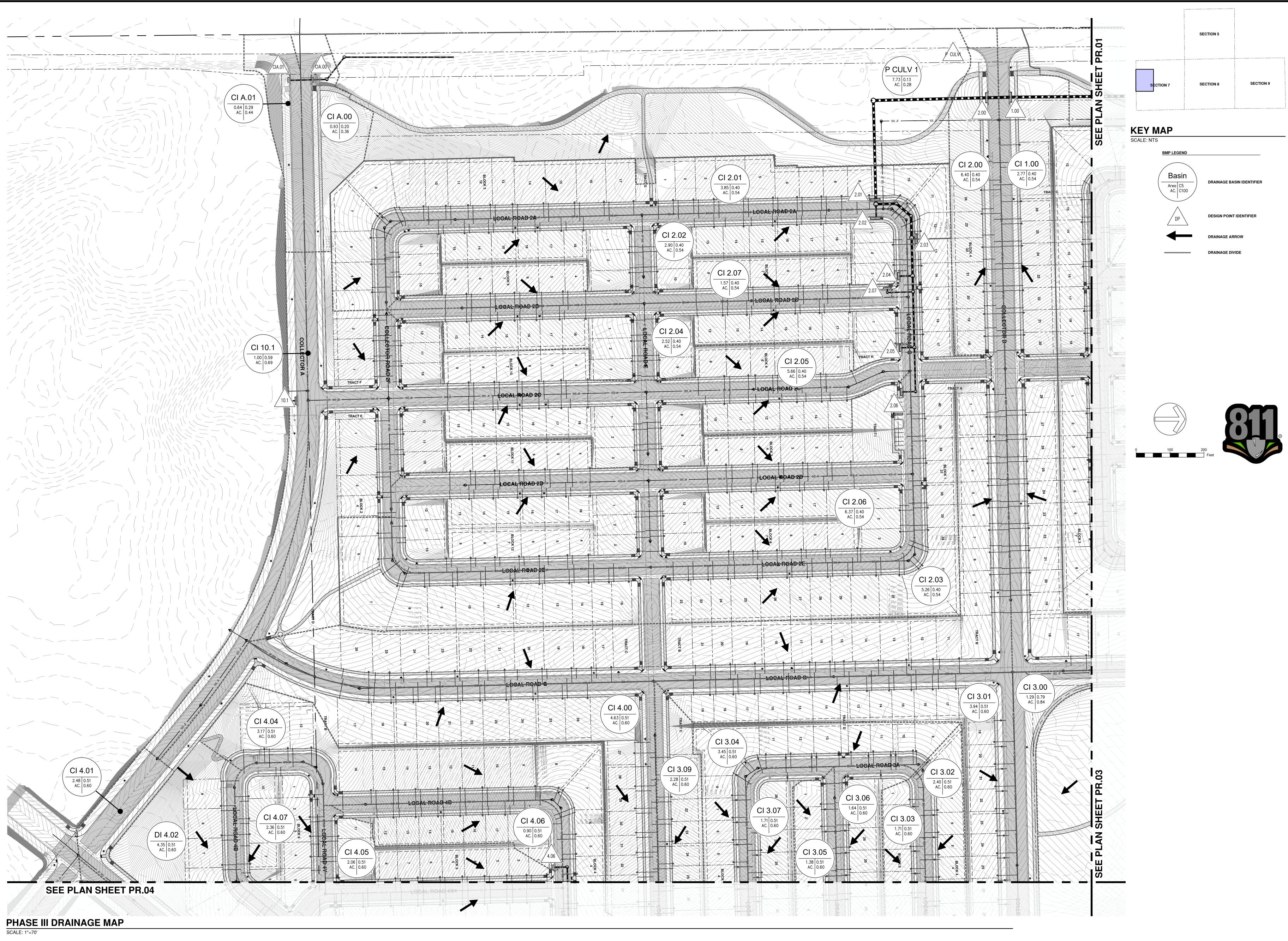
a 1% chance c		LEGEND	
the area cubic	INUNDATI	FLOOD HAZARD AREAS (SFHAs) SUBJECT TO ION BY THE 1% ANNUAL CHANCE FLOOD (100-year flood), also known as the base flood, is the flood that ed or exceeded in any given year. The Special Flood Hazard Area i	
include Zones elevation of the	ct to flooding b A, AE, AH, AO,	by the 1% annual chance flood. Areas of Special Flood Hazard , AR, A99, V, and VE. The Base Flood Elevation is the water-surfac	
ZONE A		Flood Elevations determined.	
ZONE AE ZONE AH	Flood dep	od Elevations determined. pths of 1 to 3 feet (usually areas of ponding); Base Flood Elevatio	ns
ZONE AO		pths of 1 to 3 feet (usually sheet flow on sloping terrain); average	
ZONE AR	Special F flood by	letermined. For areas of alluvial fan flooding, velocities also determ Flood Hazard Areas formerly protected from the 1% annual chance a flood control system that was subsequently decertified. Zone ates that the former flood control system is being restored to provi	
ZONE A99	protectio Area to b	on from the 1% annual chance or greater flood. be protected from 1% annual chance flood by a Federal flood	
ZONE V		on system under construction; no Base Flood Elevations determined flood zone with velocity hazard (wave action); no Base Flood Eleva	
ZONE VE		flood zone with velocity hazard (wave action); Base Flood Elevation	ns
		AY AREAS IN ZONE AE	
		of a stream plus any adjacent floodplain areas that must be kept fi 6 annual chance flood can be carried without substantial increases	
ZONE X		OOD AREAS % annual chance flood; areas of 1% annual chance flood with	
	average dept	oths of less than 1 foot or with drainage areas less than 1 square eas protected by levees from 1% annual chance flood.	
ZONE X ZONE D		nined to be outside the 0.2% annual chance floodplain. ich flood hazards are undetermined, but possible.	
\square	COASTAL	BARRIER RESOURCES SYSTEM (CBRS) AREAS	
	OTHERWI	ISE PROTECTED AREAS (OPAs)	
CBRS areas an	d OPAs are noi	rmally located within or adjacent to Special Flood Hazard Areas.	
		1% Annual Chance Floodplain Boundary 0.2% Annual Chance Floodplain Boundary	
		Floodway boundary	
		Zone D boundary CBRS and OPA boundary	
00000000		Boundary dividing Special Flood Hazard Area Zones and boundar dividing Special Flood Hazard Areas of different Base Flood Eleva	
~~ 540.	••••	flood depths, or flood velocities. Base Flood Elevation line and value; elevation in feet*	15
(EL 987))	Base Flood Elevation value where uniform within zone; elevation	n in
Referenced to	the North Am	feet nerican Vertical Datum of 1988	
A		Cross section line	
23		Transect line	
45° 02' 08", 9	93° 02' 12"	Geographic coordinates referenced to the North American Datun 1983 (NAD 83) Western Hemisphere	n of
3100000	FT	5000-foot ticks: Colorado State Plane Central Zone (FIPS Zone 0502), Lambert Conformal Conic projection	
⁴⁹ 89 ^{000m} ℕ	1	1000-meter Universal Transverse Mercator grid values, zone 13	-
DX5510 • M1.5	×	Bench mark (see explanation in Notes to Users section of this FI panel) River Mile	.RM
	EFFEC	FLOOD INSURANCE RATE MAP January 20, 2016 CTIVE DATE(S) OF REVISION(S) TO THIS PANEL	
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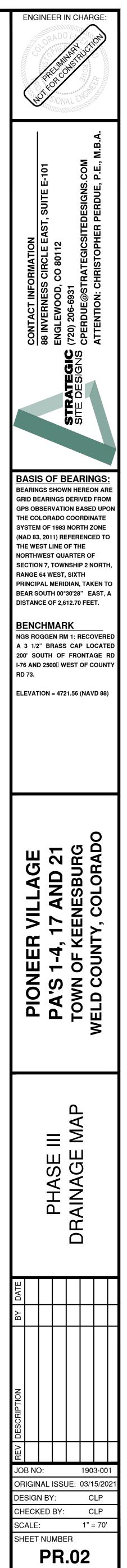


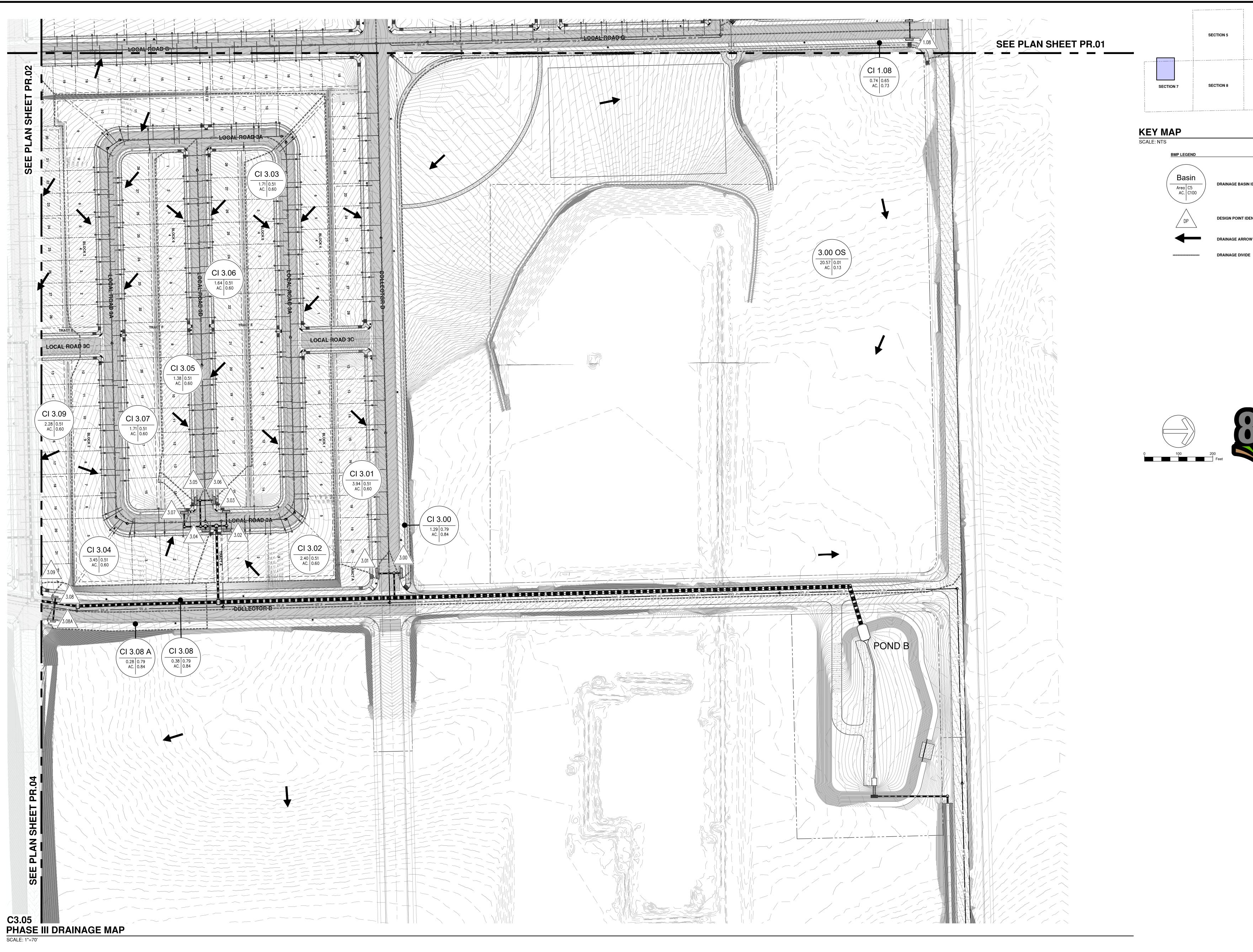


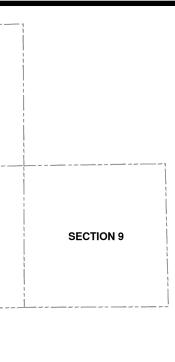
SCALE: 1"=70'







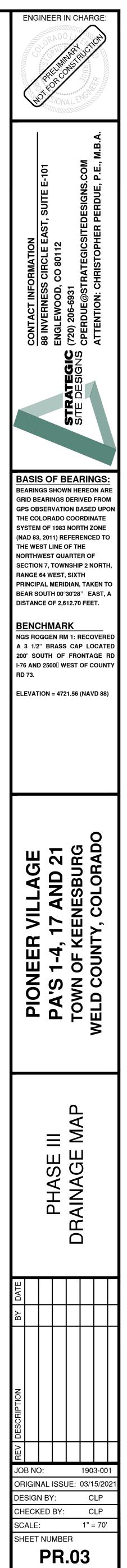


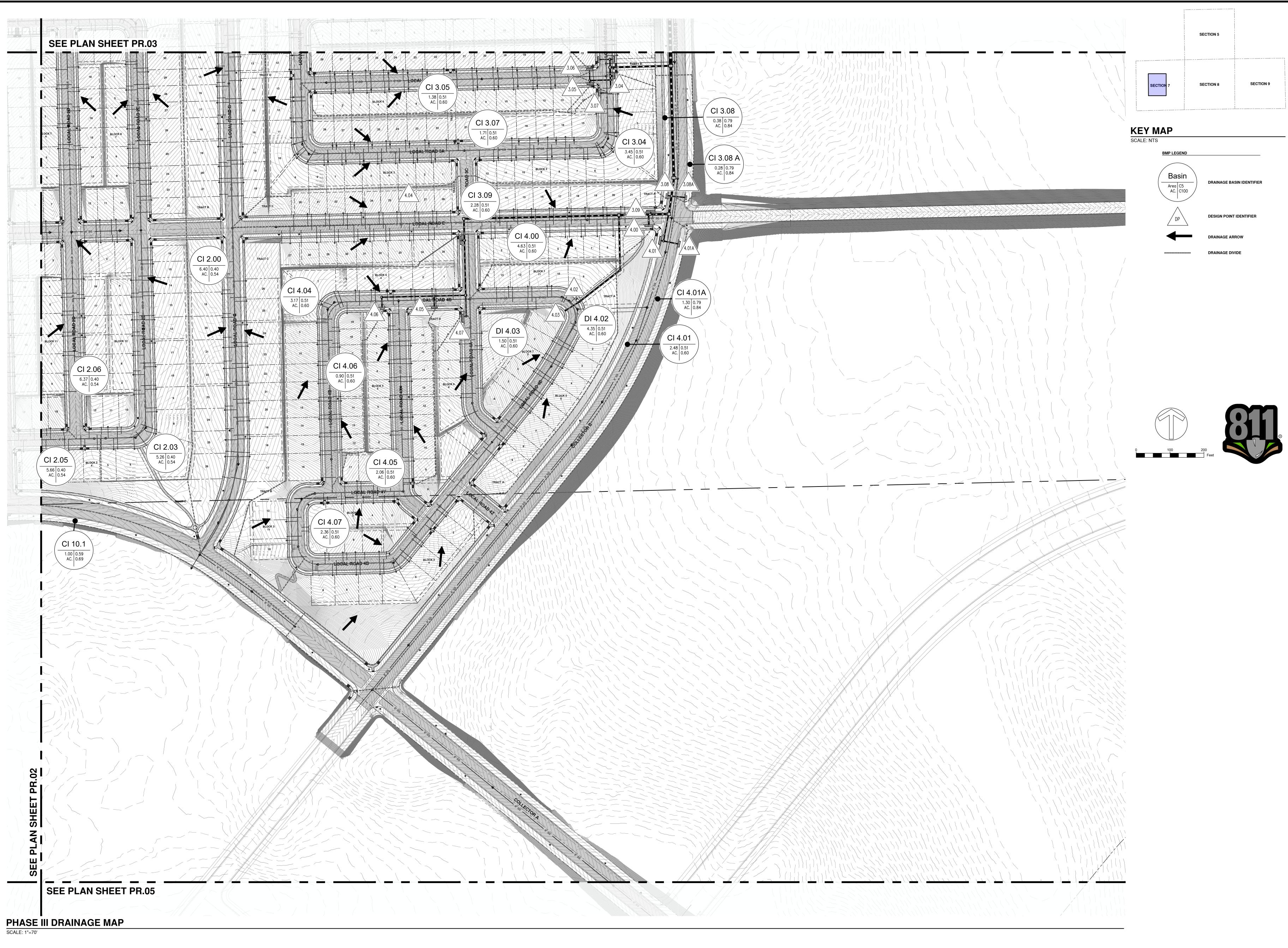


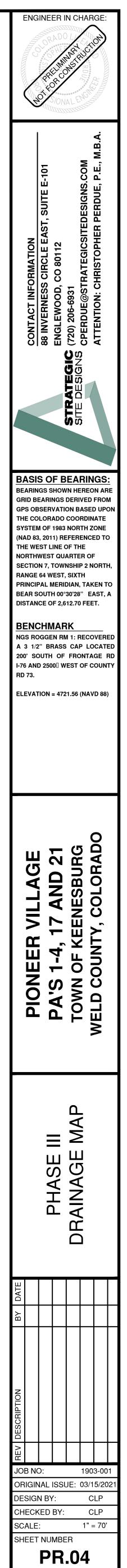
DRAINAGE BASIN IDENTIFIER

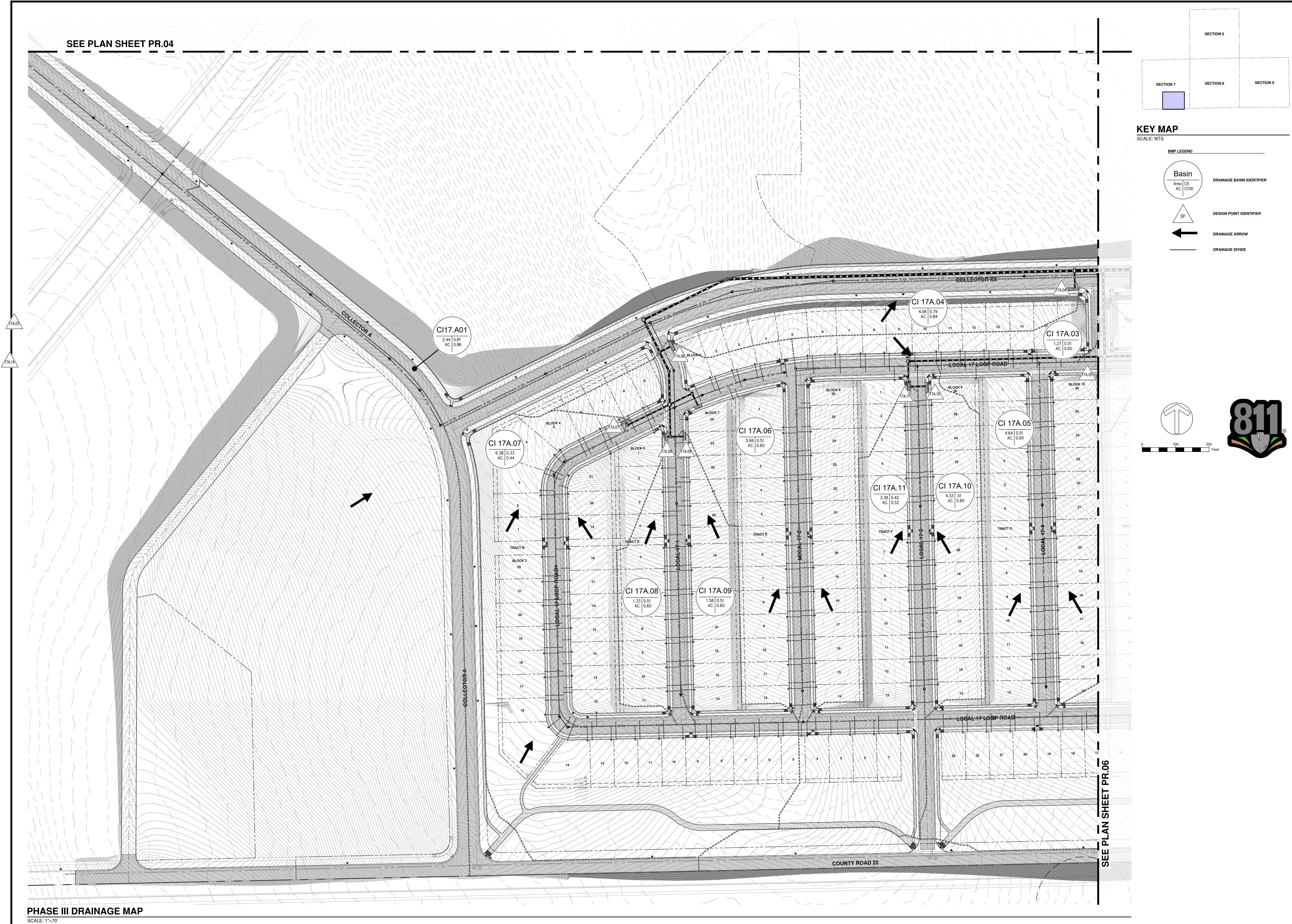
DESIGN POINT IDENTIFIER

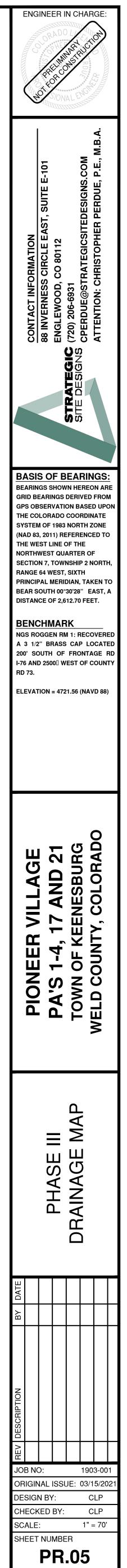


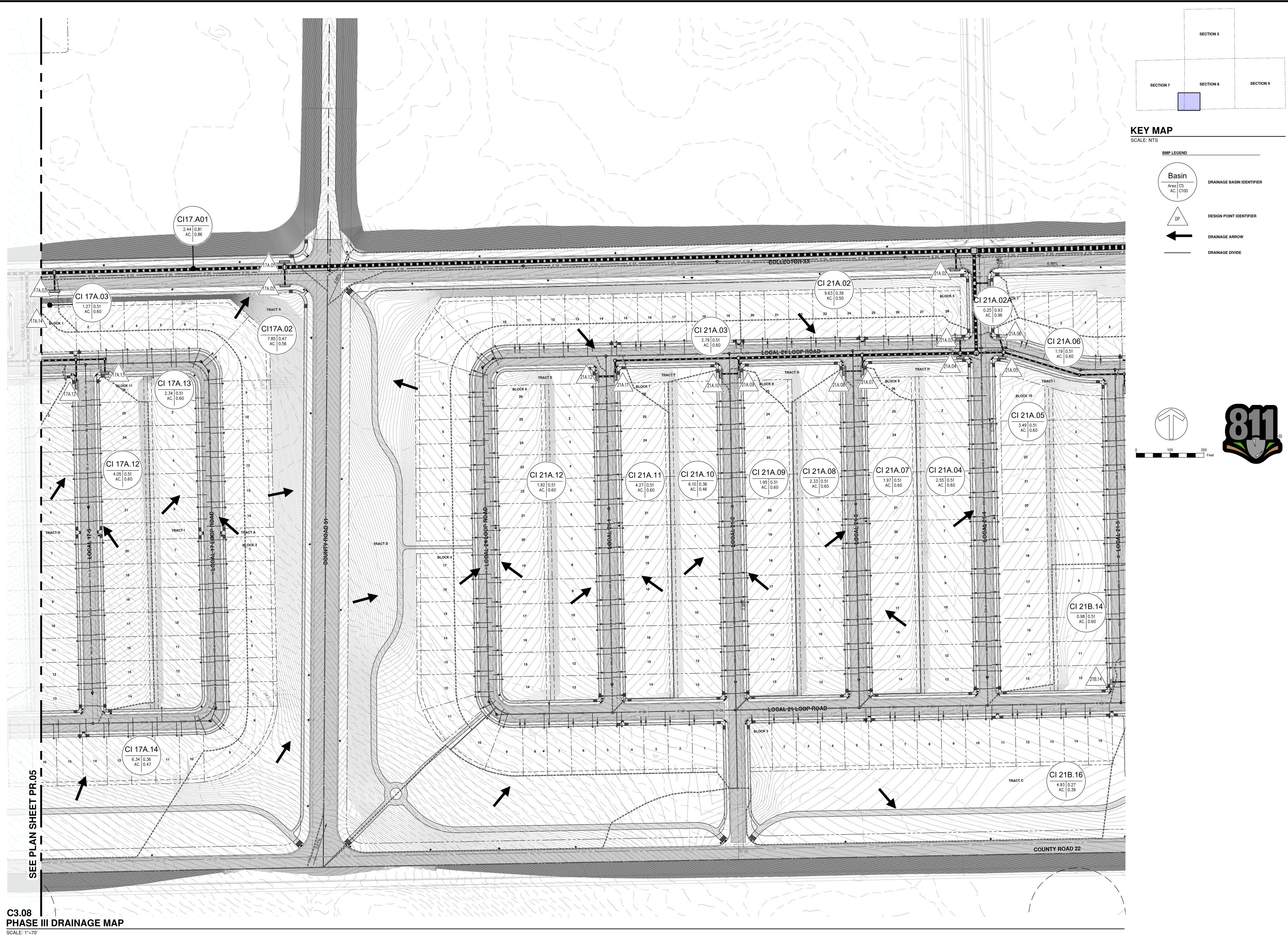


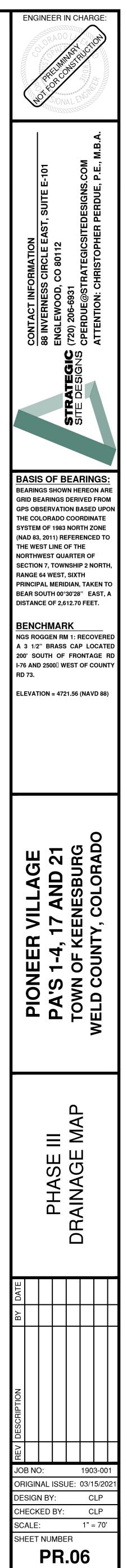


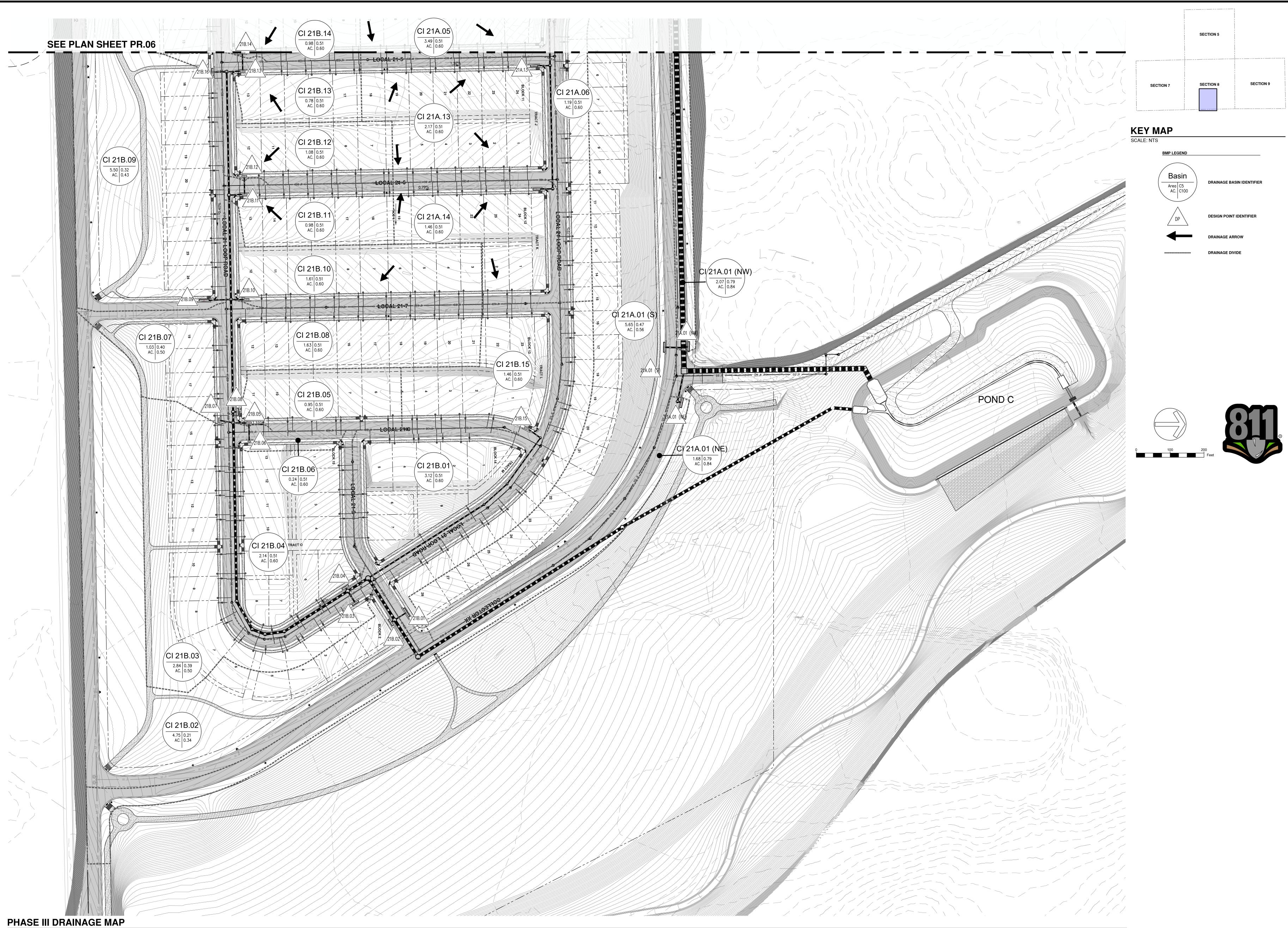


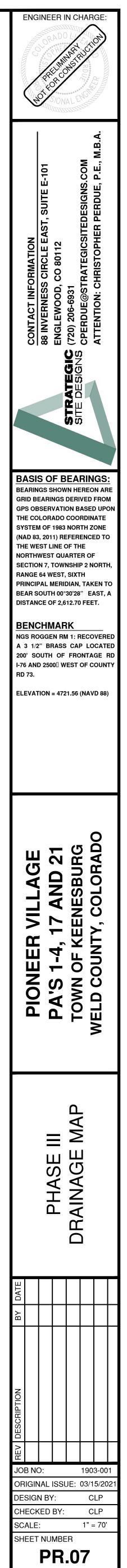
















United States Department of Agriculture

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Weld County, Colorado, Southern Part

Pioneer Village Section 7



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Contents

Preface	2
How Soil Surveys Are Made	
Soil Map	
Soil Map	9
Legend	10
Map Unit Legend	11
Map Unit Descriptions	11
Weld County, Colorado, Southern Part	
44—Olney loamy sand, 1 to 3 percent slopes	
49—Osgood sand, 0 to 3 percent slopes	14
70—Valent sand, 3 to 9 percent slopes	15
72—Vona loamy sand, 0 to 3 percent slopes	17
References	

How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP LEGEND			MAP INFORMATION		
	nterest (AOI) Area of Interest (AOI)	61	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.		
Soils	Area of Interest (AOI) Soil Map Unit Polygons Soil Map Unit Lines Soil Map Unit Lines Borrow Pit Clay Spot Closed Depression Gravel Pit Gravelly Spot Landfill Lava Flow Marsh or swamp	ا ک ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا ا	Very Stony Spot Wet Spot Other Special Line Features res Streams and Canals ion Rails Interstate Highways US Routes Major Roads Local Roads	1:24,000. Warning: Soil Map may not be valid at this scale. Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale. Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.		
	Mine or Quarry Miscellaneous Water Perennial Water Rock Outcrop Saline Spot Sandy Spot Severely Eroded Spot Sinkhole Slide or Slip Sodic Spot			 This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Weld County, Colorado, Southern Part Survey Area Data: Version 19, Jun 5, 2020 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Jul 19, 2018—Aug 10, 2018 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. 		

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
44	Olney loamy sand, 1 to 3 percent slopes	1.4	0.2%
49	Osgood sand, 0 to 3 percent slopes	88.0	14.4%
70	Valent sand, 3 to 9 percent slopes	467.2	76.7%
72	Vona loamy sand, 0 to 3 percent slopes	52.6	8.6%
Totals for Area of Interest		609.1	100.0%

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Weld County, Colorado, Southern Part

44—Olney loamy sand, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 362r Elevation: 4,600 to 5,200 feet Mean annual precipitation: 11 to 15 inches Mean annual air temperature: 46 to 54 degrees F Frost-free period: 125 to 175 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Olney and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Olney

Setting

Landform: Plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Mixed deposit outwash

Typical profile

H1 - 0 to 10 inches: loamy sand H2 - 10 to 20 inches: sandy clay loam H3 - 20 to 25 inches: sandy clay loam H4 - 25 to 60 inches: fine sandy loam

Properties and qualities

Slope: 1 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water capacity: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 4c Hydrologic Soil Group: B Ecological site: R067BY024CO - Sandy Plains Hydric soil rating: No

Minor Components

Vona

Percent of map unit: 8 percent

Hydric soil rating: No

Zigweid

Percent of map unit: 7 percent Hydric soil rating: No

49—Osgood sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 362x Elevation: 4,680 to 4,900 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 46 to 55 degrees F Frost-free period: 140 to 150 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Osgood and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Osgood

Setting

Landform: Plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Eolian sands

Typical profile

H1 - 0 to 22 inches: sand *H2 - 22 to 34 inches:* sandy loam *H3 - 34 to 60 inches:* sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water capacity: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A *Ecological site:* R067BY015CO - Deep Sand *Hydric soil rating:* No

Minor Components

Valent

Percent of map unit: 10 percent *Hydric soil rating:* No

Dailey

Percent of map unit: 5 percent Hydric soil rating: No

70-Valent sand, 3 to 9 percent slopes

Map Unit Setting

National map unit symbol: 2tczf Elevation: 3,050 to 5,150 feet Mean annual precipitation: 12 to 18 inches Mean annual air temperature: 48 to 55 degrees F Frost-free period: 130 to 180 days Farmland classification: Not prime farmland

Map Unit Composition

Valent and similar soils: 80 percent Minor components: 20 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Valent

Setting

Landform: Hills, dunes Landform position (two-dimensional): Backslope, shoulder, footslope, summit Landform position (three-dimensional): Side slope, head slope, nose slope, crest Down-slope shape: Linear, convex Across-slope shape: Linear, convex Parent material: Noncalcareous eolian sands

Typical profile

A - 0 to 5 inches: sand AC - 5 to 12 inches: sand C1 - 12 to 30 inches: sand C2 - 30 to 80 inches: sand

Properties and qualities

Slope: 3 to 9 percent Depth to restrictive feature: More than 80 inches Drainage class: Excessively drained Runoff class: Very low Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 39.96 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None Calcium carbonate, maximum content: 1 percent Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Very low (about 2.4 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R067BY015CO - Deep Sand, R072XY109KS - Rolling Sands Hydric soil rating: No

Minor Components

Dailey

Percent of map unit: 10 percent Landform: Interdunes Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Concave Ecological site: R067BY015CO - Deep Sand, R072XA021KS - Sands (North) (PE 16-20)

Hydric soil rating: No

Vona

Percent of map unit: 5 percent Landform: Hills Landform position (two-dimensional): Footslope, backslope, shoulder Landform position (three-dimensional): Side slope, head slope, nose slope, base slope Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY024CO - Sandy Plains, R072XA022KS - Sandy (North) Draft (April 2010) (PE 16-20) Hydric soil rating: No

Haxtun

Percent of map unit: 5 percent Landform: Interdunes Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Concave Ecological site: R067BY024CO - Sandy Plains, R072XY111KS - Sandy Plains Hydric soil rating: No

72—Vona loamy sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 363r Elevation: 4,600 to 5,200 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 48 to 55 degrees F Frost-free period: 130 to 160 days Farmland classification: Farmland of local importance

Map Unit Composition

Vona and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Vona

Setting

Landform: Plains, terraces Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium and/or eolian deposits

Typical profile

H1 - 0 to 6 inches: loamy sand H2 - 6 to 28 inches: fine sandy loam H3 - 28 to 60 inches: sandy loam

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Maximum salinity: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)
Available water capacity: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 4e Hydrologic Soil Group: A Ecological site: R067BY024CO - Sandy Plains Hydric soil rating: No

Minor Components

Remmit

Percent of map unit: 10 percent *Hydric soil rating:* No

Valent

Percent of map unit: 5 percent Hydric soil rating: No

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United States Department of Agriculture

Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Weld County, Colorado, Southern Part

Pioneer Village Section 8



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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Contents

Preface How Soil Surveys Are Made	
Soil Map	
Soil Map	9
Legend	10
Map Unit Legend	11
Map Unit Descriptions	11
Weld County, Colorado, Southern Part	
35—Loup-Boel loamy sands, 0 to 3 percent slopes	13
44—Olney loamy sand, 1 to 3 percent slopes	14
49—Osgood sand, 0 to 3 percent slopes	15
70—Valent sand, 3 to 9 percent slopes	17
72—Vona loamy sand, 0 to 3 percent slopes	18
85—Water	19
References	21

How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

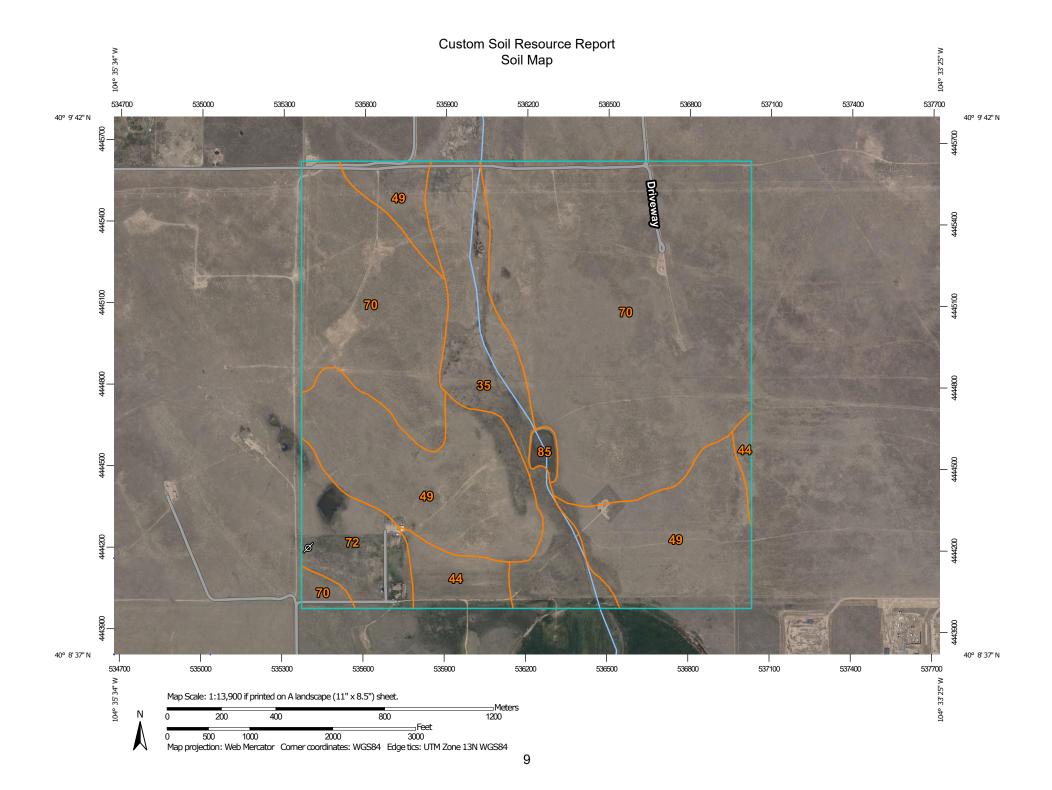
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND)	MAP INFORMATION	
Area of Int	erest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:24,000.	
Soils	Soil Map Unit Polygons Soil Map Unit Lines	00 V	Very Stony Spot Wet Spot	Please rely on the bar scale on each map sheet for map measurements.	
•	Soil Map Unit Points Point Features	△ Water Fea	Other Special Line Features	Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857)	
© ⊠ ×	Blowout Borrow Pit Clay Spot	~	Streams and Canals Transportation	Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.	
◇ ※	Closed Depression Gravel Pit Gravelly Spot	* *	Interstate Highways US Routes Major Roads	This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.	
© ۸.	Landfill Lava Flow Marsh or swamp	Backgrou	Local Roads Ind Aerial Photography	Soil Survey Area: Weld County, Colorado, Southern Part Survey Area Data: Version 19, Jun 5, 2020 Soil map units are labeled (as space allows) for map scales	
* 0 0	Mine or Quarry Miscellaneous Water Perennial Water			1:50,000 or larger. Date(s) aerial images were photographed: Jul 19, 2018—Aug 10, 2018	
× + ∷	Rock Outcrop Saline Spot Sandy Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.	
⊕ ♦ ∮	Severely Eroded Spot Sinkhole Slide or Slip Sodic Spot				
עצ					

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
35	Loup-Boel loamy sands, 0 to 3 percent slopes	78.9	11.6%
44	Olney loamy sand, 1 to 3 percent slopes	22.8	3.4%
49	Osgood sand, 0 to 3 percent slopes	176.6	26.0%
70	Valent sand, 3 to 9 percent slopes	359.5	53.0%
72	Vona loamy sand, 0 to 3 percent slopes	37.0	5.5%
85	Water	3.9	0.6%
Totals for Area of Interest		678.7	100.0%

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Weld County, Colorado, Southern Part

35—Loup-Boel loamy sands, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 362f Elevation: 4,550 to 4,750 feet Mean annual precipitation: 11 to 15 inches Mean annual air temperature: 46 to 52 degrees F Frost-free period: 130 to 180 days Farmland classification: Not prime farmland

Map Unit Composition

Loup and similar soils: 55 percent Boel and similar soils: 35 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Loup

Setting

Landform: Swales, drainageways, streams Down-slope shape: Linear Across-slope shape: Linear Parent material: Sandy alluvium

Typical profile

H1 - 0 to 16 inches: loamy sand H2 - 16 to 40 inches: loamy sand H3 - 40 to 60 inches: sandy loam

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: About 0 to 18 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water capacity: Low (about 5.2 inches)

Interpretive groups

Land capability classification (irrigated): 4w Land capability classification (nonirrigated): 6w Hydrologic Soil Group: A/D Ecological site: R067BY029CO - Sandy Meadow Hydric soil rating: Yes

Description of Boel

Setting

Landform: Swales, drainageways, streams Down-slope shape: Linear Across-slope shape: Linear Parent material: Stratified sandy alluvium

Typical profile

H1 - 0 to 14 inches: loamy sand *H2 - 14 to 60 inches:* loamy sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Somewhat poorly drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (5.95 to 19.98 in/hr)
Depth to water table: About 18 to 36 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 5 percent
Available water capacity: Low (about 4.2 inches)

Interpretive groups

Land capability classification (irrigated): 4w Land capability classification (nonirrigated): 6w Hydrologic Soil Group: A Ecological site: R067BY029CO - Sandy Meadow Hydric soil rating: No

Minor Components

Osgood

Percent of map unit: 5 percent Hydric soil rating: No

Valent

Percent of map unit: 5 percent Hydric soil rating: No

44—Olney loamy sand, 1 to 3 percent slopes

Map Unit Setting

National map unit symbol: 362r Elevation: 4,600 to 5,200 feet Mean annual precipitation: 11 to 15 inches Mean annual air temperature: 46 to 54 degrees F Frost-free period: 125 to 175 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Olney and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Olney

Setting

Landform: Plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Mixed deposit outwash

Typical profile

H1 - 0 to 10 inches: loamy sand
H2 - 10 to 20 inches: sandy clay loam
H3 - 20 to 25 inches: sandy clay loam
H4 - 25 to 60 inches: fine sandy loam

Properties and qualities

Slope: 1 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.60 to 2.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water capacity: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 4c Hydrologic Soil Group: B Ecological site: R067BY024CO - Sandy Plains Hydric soil rating: No

Minor Components

Vona

Percent of map unit: 8 percent Hydric soil rating: No

Zigweid

Percent of map unit: 7 percent Hydric soil rating: No

49—Osgood sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 362x Elevation: 4,680 to 4,900 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 46 to 55 degrees F Frost-free period: 140 to 150 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Osgood and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Osgood

Setting

Landform: Plains Down-slope shape: Linear Across-slope shape: Linear Parent material: Eolian sands

Typical profile

H1 - 0 to 22 inches: sand *H2 - 22 to 34 inches:* sandy loam *H3 - 34 to 60 inches:* sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)
Available water capacity: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R067BY015CO - Deep Sand Hydric soil rating: No

Minor Components

Valent

Percent of map unit: 10 percent *Hydric soil rating:* No

Dailey

Percent of map unit: 5 percent Hydric soil rating: No

70-Valent sand, 3 to 9 percent slopes

Map Unit Setting

National map unit symbol: 2tczf Elevation: 3,050 to 5,150 feet Mean annual precipitation: 12 to 18 inches Mean annual air temperature: 48 to 55 degrees F Frost-free period: 130 to 180 days Farmland classification: Not prime farmland

Map Unit Composition

Valent and similar soils: 80 percent Minor components: 20 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Valent

Setting

Landform: Hills, dunes Landform position (two-dimensional): Backslope, shoulder, footslope, summit Landform position (three-dimensional): Side slope, head slope, nose slope, crest Down-slope shape: Linear, convex Across-slope shape: Linear, convex Parent material: Noncalcareous eolian sands

Typical profile

A - 0 to 5 inches: sand AC - 5 to 12 inches: sand C1 - 12 to 30 inches: sand C2 - 30 to 80 inches: sand

Properties and qualities

Slope: 3 to 9 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00 to 39.96 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 1 percent
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water capacity: Very low (about 2.4 inches)

Interpretive groups

Land capability classification (irrigated): 4e Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Ecological site: R067BY015CO - Deep Sand, R072XY109KS - Rolling Sands Hydric soil rating: No

Minor Components

Dailey

Percent of map unit: 10 percent Landform: Interdunes Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Concave Ecological site: R067BY015CO - Deep Sand, R072XA021KS - Sands (North) (PE 16-20) Hydric soil rating: No

Vona

Percent of map unit: 5 percent Landform: Hills Landform position (two-dimensional): Footslope, backslope, shoulder Landform position (three-dimensional): Side slope, head slope, nose slope, base slope Down-slope shape: Linear Across-slope shape: Linear Ecological site: R067BY024CO - Sandy Plains, R072XA022KS - Sandy (North) Draft (April 2010) (PE 16-20) Hydric soil rating: No

Haxtun

Percent of map unit: 5 percent Landform: Interdunes Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope Down-slope shape: Linear Across-slope shape: Concave Ecological site: R067BY024CO - Sandy Plains, R072XY111KS - Sandy Plains Hydric soil rating: No

72—Vona loamy sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 363r Elevation: 4,600 to 5,200 feet Mean annual precipitation: 13 to 15 inches Mean annual air temperature: 48 to 55 degrees F Frost-free period: 130 to 160 days Farmland classification: Farmland of local importance

Map Unit Composition

Vona and similar soils: 85 percent *Minor components:* 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Vona

Setting

Landform: Plains, terraces Down-slope shape: Linear Across-slope shape: Linear Parent material: Alluvium and/or eolian deposits

Typical profile

H1 - 0 to 6 inches: loamy sand H2 - 6 to 28 inches: fine sandy loam H3 - 28 to 60 inches: sandy loam

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): High (1.98 to 6.00 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Calcium carbonate, maximum content: 15 percent
Maximum salinity: Nonsaline to slightly saline (0.0 to 4.0 mmhos/cm)
Available water capacity: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): 3e Land capability classification (nonirrigated): 4e Hydrologic Soil Group: A Ecological site: R067BY024CO - Sandy Plains Hydric soil rating: No

Minor Components

Remmit

Percent of map unit: 10 percent *Hydric soil rating:* No

Valent

Percent of map unit: 5 percent Hydric soil rating: No

85—Water

Map Unit Composition Water: 95 percent Minor components: 5 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Minor Components

Aquolls

Percent of map unit: 5 percent Landform: Marshes Hydric soil rating: Yes

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